



# Preliminary Drainage Report

For

## Arizona Farms

### Pinal County, Arizona

#### Owner/Developer

El Dorado Arizona Farms, LLC, an  
Arizona Limited Liability Company

8501 N. Scottsdale Road Suite 120

Tel: 602-955-2424

Contact: Brad Hinton

#### Civil Engineer

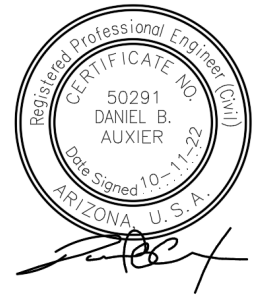
EPS Group Inc.

1130 N. Alma School Road, Ste. 120

Mesa, AZ 85201

Tel: 480-503-2250

Contact: Daniel Auxier



Project No. 21-0483

Date: October 2022

1130 N. Alma School Road, Suite 120

Mesa, AZ 85201

o: 480.503.2250

f: 480.503.2258

## Table of Contents

1.0	Introduction .....	2
1.1	National Flood Insurance Program .....	2
2.0	Existing Site Conditions.....	2
3.0	Offsite Drainage Characteristics and Hydrology.....	2
4.0	Onsite Drainage Characteristics and Hydrology.....	3
5.0	Methodology and Criteria.....	4
5.1	Rational Method .....	4
5.2	Time of Concentration .....	4
6.0	Drainage Infrastructure .....	4
6.1	Onsite Retention Requirements.....	4
6.1.1	Required Retention Volume .....	5
6.1.2	Provided Retention Volume.....	5
7.0	Ultimate Outfall.....	5
8.0	Conclusions.....	5
9.0	References .....	6

## List of Figures

Figure 1: FIRM Map.....	Appendix A
Figure 2: NOAA Atlas.....	Appendix A
Figure 3: Preliminary Drainage Exhibit.....	Appendix A

## Appendix List

- Appendix A: Figures
- Appendix B: Preliminary Drainage Calculations
- Appendix C: Offsite Drainage Report
- Appendix D: Offsite Drainage Analysis

## 1.0 Introduction

Arizona Farms, the Project, is a proposed residential development of 3,126 lots on approximately 760 acres. The site is bounded by E Arizona Farms Road to the north, N Felix Road to the East, E Heritage Road to the South, and the Copper Basin Railway to the West. By legal description, the property is located in a portion of land located in both Section 1, Township 4 South, Range 8 East, and Section 6, Township 4 South, Range 9 East of the Gila and Salt River Base Meridian, Pinal County, Arizona, Assessor Parcel Numbers (APN) 200-31-007B,D,E,F,G,K,L, 200-24-001R, and W.

This preliminary report evaluates the drainage characteristics within the Arizona Farms master planned community. Design parameters from Pinal County will be applied to the Project to ensure adherence to regulations.

### 1.1 National Flood Insurance Program

The Project is located within FEMA Flood Zone Shaded X as shown on FEMA Flood Insurance Rate (FIRM) Map 04021C0875E for Pinal County dated December 4, 2007. See Figure 1: FIRM Map.

Flood Zone Shaded X is defined as:

Areas of the 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

## 2.0 Existing Site Conditions

The Project site is currently used for agricultural purposes. Existing grades historically slope from the northeast of the site to the southwest.

## 3.0 Offsite Drainage Characteristics and Hydrology

The Magma Dam/FRS is approximately three miles to the east of the site, which exists to provide flood protection from residents and infrastructure in Florence, Arizona.

Offsite flows impacting the development are generated by the area whose outline is called the Magma Flood Control District, by the governing Pinal County Flood Control District (PCFCD).

There are 3 main offsite flows impacting the site. The first enters the site from the north at the intersection of Attaway Rd and Arizona Farms Road. The overtop of Arizona Farms Rd totals 95 cfs entering the site. In the existing condition, this flow is routed toward the west.

## Arizona Farms Drainage Report

The second flow enters the site at the northwest corner of the site, at the intersection of the Copper Basin Railway and Arizona Farms Road. The Copper Basin Railway acts as a berm that directs a flow of 101 cfs through the site along the railway.

The third enters the site near the northeast corner of the site, where irrigation fields overtop Felix Road at a rate of 55 cfs. The 55 cfs combines with a flow of 35 cfs which originates from rainfall in HEC-1 sub-basin 3. These two flows combine for a total of 90 cfs which flows through a swale then south-southeast through agricultural fields in the existing condition.

The flow rates used for the hydrology were obtained from the approved Master Drainage Report for Arizona Farms found in Appendix D.

In order to accommodate the offsite flows impacting the site, it is recommended to reserve space that can be used to construct swales, basins, and minor channels as part of the proposed development. See the Offsite Drainage Report in Appendix C for more information.

### **4.0 Onsite Drainage Characteristics and Hydrology**

The drainage exhibit for the Project is located in Appendix A. The exhibit highlights sub-drainage areas, flow directions, inlet locations, and retention basin locations and capacities. Runoff generated onsite will be routed to the retention basins located within the parcel.

All retention basins have been designed to pond three (3) feet deep with one (1) foot of freeboard, unless noted otherwise, with side slopes of 4:1 and/or 6:1. All retention basins have been adequately sized to retain the 100-year, 2-hour storm event per Pinal County design requirements.

Pinal County design standards require all retention basins to drain within a 36-hour period. Drywells have been used to facilitate percolation of the runoff for any basins deeper than one foot in ponding depth. A percolation test will be required as part of the Final Drainage clearance for the site. Drywell will be installed according to Arizona Department of Environmental Quality (ADEQ) guidelines of installation and will be designed and maintained in accordance with the Town of Queen Creek's Drywell Policy. All drywells will be registered with ADEQ. See section 602.3 & 602.4 of the Drainage Ordinance and sections 3.10.4.2 & 3.10.4.3 in volume I of the Pinal County Drainage Manual.

## Arizona Farms Drainage Report

Onsite basins will retain 100% of the 100-year, 2-hour storm event per Pinal County requirements. All retention basins were designed with a maximum of 4:1 side slopes and ponding depths not to exceed 3 feet with 1 foot of freeboard to the low gutter elevation, making a total depth not to exceed 4 feet.

### 5.0 Methodology and Criteria

The following section provides an overview of the rational method and time of concentration to be used during final design for sizing of drainage structures.

#### 5.1 Rational Method

The rational method will be used for storm drain peak flows:

$$Q_p = C \times i \times A_d$$

where:

$Q_p$  = Peak flow (cfs)

$C$  = Composite runoff coefficient

$i$  = Intensity corresponding to  $T_c$

$A_d$  = Area in acres

#### 5.2 Time of Concentration

Inlet time estimated, system time established based on summation of travel time in system and initial time of concentration based upon the following equation, with the initial lot  $T_c$  being 5 minutes:

$$T_c = 11.4L^{0.5} \times K_b^{0.52} \times S^{-0.31} \times i^{-0.38}$$

where:

$T_c$  = Time of concentration (hrs): minimum of 5 minutes

$L$  = Length of the longest flow path (miles)

$K_b$  = Watershed resistance coefficient – (See Maricopa County Drainage Manual, Hydrology)

$S$  = Watercourse slope (ft/mi)

$i$  = Rainfall intensity (in/hr)

### 6.0 Drainage Infrastructure

The following section provides an overview of the storm water drainage system that will be designed to collect and dispose of runoff generated during the 100-year, 2-hour storm event.

#### 6.1 Onsite Retention Requirements

The following section outlines the design requirements governing onsite retention basins as outlined in the Pinal County drainage standards.

### 6.1.1 Required Retention Volume

$$V_{required} = (C \times P \times A)/12$$

where:

$$V_{required} = \text{Volume Required (cf)}$$

C = Average per FCDMC Hydrology Manual

P = 2.27-inches (100-year, 2-hour design storm)

A = Area (sf)

### 6.1.2 Provided Retention Volume

Volume provided is calculated using the Conic Approximation Method:

$$V_{provided} = d/3 (A_{top} + A_{bot} + \sqrt{A_{top}A_{bot}})$$

where:

$$V_{provided} = \text{Volume Provided (cf)}$$

d = Depth of basin (ft)

A<sub>top</sub> = Area of top contour (sf)

A<sub>bot</sub> = Area of bottom contour (sf)

## 7.0 Ultimate Outfall

The ultimate outfall for of the site is at the culvert along the southern boundary at an approximate elevation of 980.00 feet. Building finished floors will be designed to be a minimum of 14” above the sub-basin and ultimate outfalls, as well as the lot low outfall.

## 8.0 Conclusions

This report concluded that:

- This site has sufficient retention capacity to retain, at a minimum, the 100-year, 2-hour event per Pinal County design standards.
- There are 3 areas where offsite flows enter the site. Space has been reserved to construct swales, basins, and minor channels as part of the proposed development to alleviate any adverse drainage impacts or increased drainage problems of offsite flows to the project or adjacent upstream or downstream, properties .
- The project has all weather access per Drainage Ordinance requirements.
- The site will be designed to comply with the Pinal County Drainage Ordinance, the Pinal County Drainage Manual, and the Pina County Floodplain Ordinance.

## 9.0 References

Pinal County Drainage Manual Volumes 1 & 2: Design Criteria

Flood Control District of Maricopa County, 2013 Drainage Design Manual for Maricopa County, AZ. Volume 1, Hydrology & Volume 2, Hydraulics

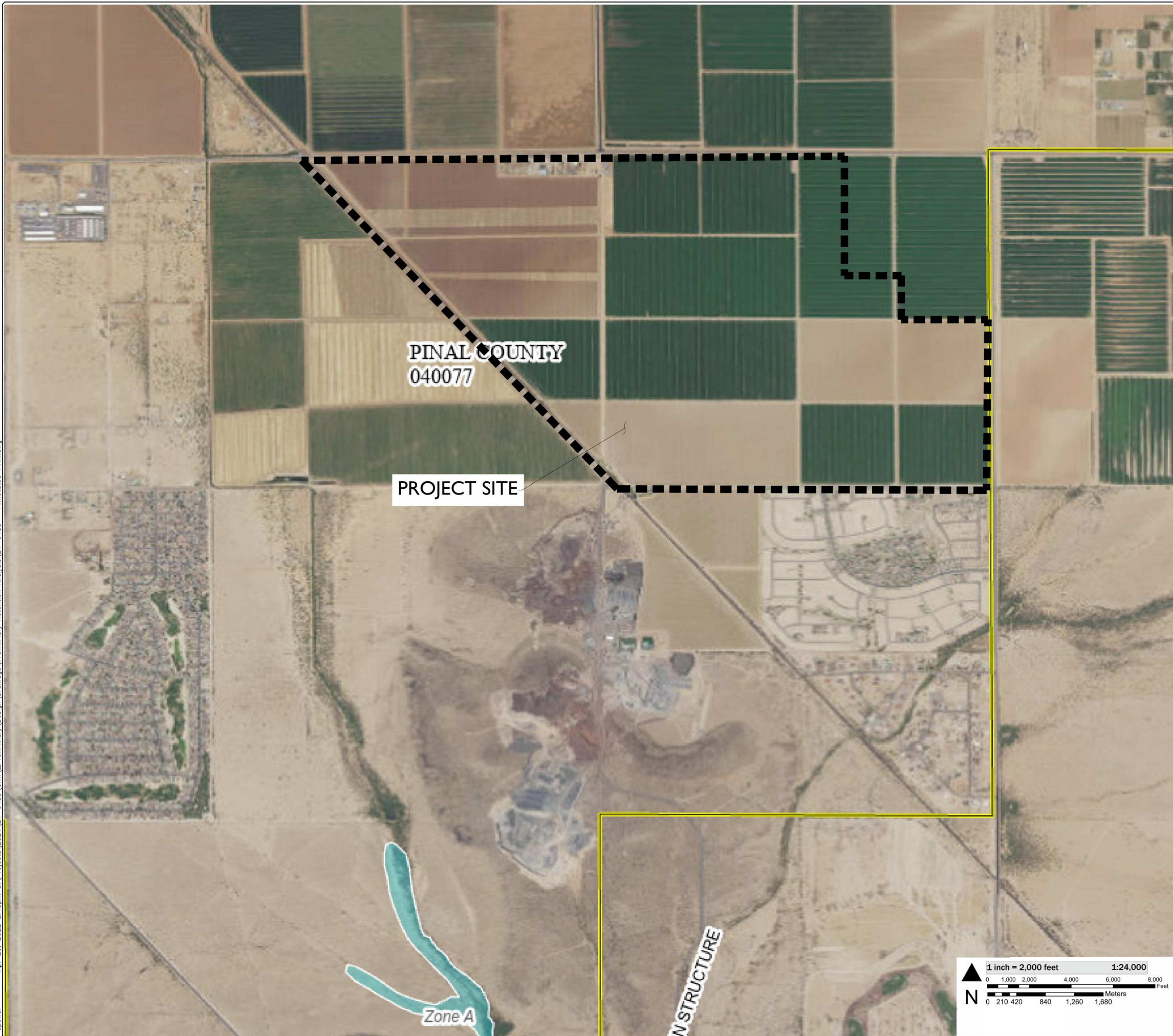
Flood Control District of Maricopa County, 2016 Drainage Policies and Standards for Maricopa County, AZ.

# **Appendix A**

## **Figures**

# 21-0483 - Arizona Farms

Apr 20, 2022 2:48pm S:\Projects\2021\21-0483\Civil\Pre\Design\Drainage\Pre\Design\Analysis\21-0483 - Associated FIRM.dwg



## FLOOD HAZARD INFORMATION

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP  
FOR DRAFT FIRM PANEL LAYOUT

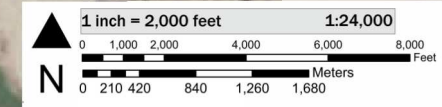
- SPECIAL FLOOD HAZARD AREAS**
  - Without Base Flood Elevation (BFE) Zone A, V, A99
  - With BFE or Depth Zone AE, AO, AH, VE, AR
  - Regulatory Floodway
- OTHER AREAS OF FLOOD HAZARD**
  - 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
  - Future Conditions 1% Annual Chance Flood Hazard Zone X
  - Area with Reduced Flood Risk due to Levee See Notes Zone X
  - Area with Flood Risk due to Levee Zone D
- OTHER AREAS**
  - NO SCREEN Area of Minimal Flood Hazard Zone X
  - Effective LOMRs
  - Area of Undetermined Flood Hazard Zone D
- GENERAL STRUCTURES**
  - Channel, Culvert, or Storm Sewer
  - Levee, Dike, or Floodwall
- OTHER FEATURES**
  - 20.2 Cross Sections with 1% Annual Chance
  - 17.5 Water Surface Elevation
  - Coastal Transect
  - Coastal Transect Baseline
  - Profile Baseline
  - Hydrographic Feature
  - Base Flood Elevation Line (BFE)
  - Limit of Study
  - Jurisdiction Boundary

PINAL COUNTY  
040077

PROJECT SITE

Zone A

N STRUCTURE



NATIONAL FLOOD INSURANCE PROGRAM  
FLOOD INSURANCE RATE MAP

PANEL 875 OF 2575

Panel Contains:

COMMUNITY	NUMBER	PANEL
PINAL COUNTY	040077	0875
FLORENCE MILITARY RESERVATION	040084	0875
TOWN OF FLORENCE	040082	0875
CITY OF COOLIDGE	040082	0875

MAP NUMBER  
04021C0875E  
EFFECTIVE DATE  
December 04, 2007

1130 N Alma School Road  
Suite 400  
Mesa, AZ 85201  
T: 480.503.2250 | F: 480.503.2258  
www.epsgroupinc.com

Project: Arizona Farms  
Pinal County, AZ

**FIGURE I - FEMA FIRM MAP**

Revisions:

NO.	DATE	DESCRIPTION

Arizona  
DRAWN BY: EPS  
DESIGNED BY: EPS

Job No.  
**21-0483**

Sheet No.  
**EX01**

Sheet No.  
**1 of 1**



**NOAA Atlas 14, Volume 1, Version 5**  
**Location name: Florence, Arizona, USA\***  
**Latitude: 33.1117°, Longitude: -111.4601°**  
**Elevation: 1532.03 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Tryppaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps\\_&\\_aerials](#)

**PF tabular**

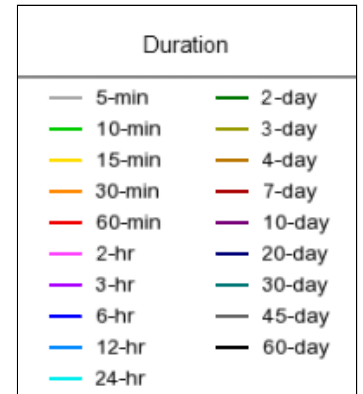
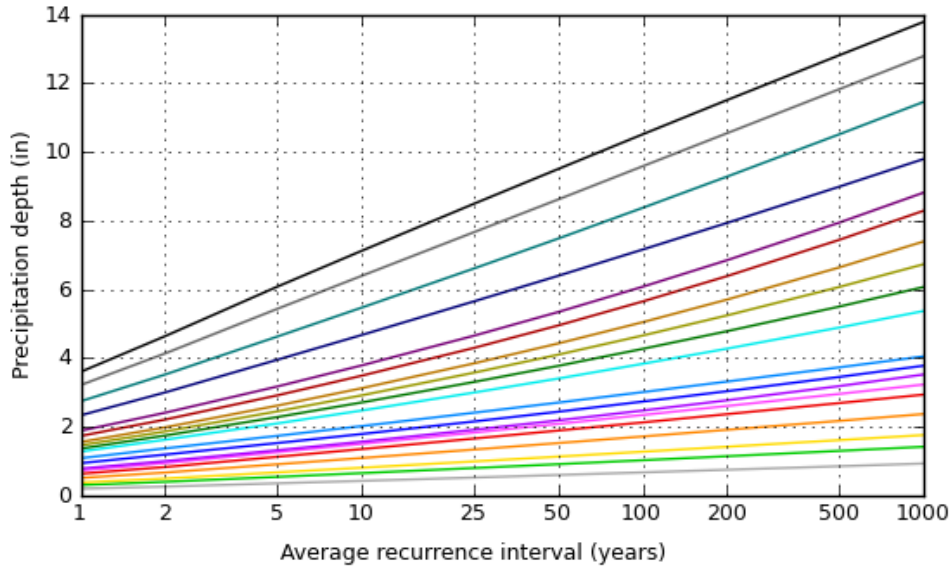
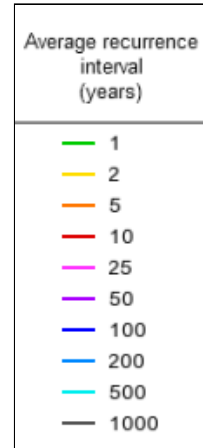
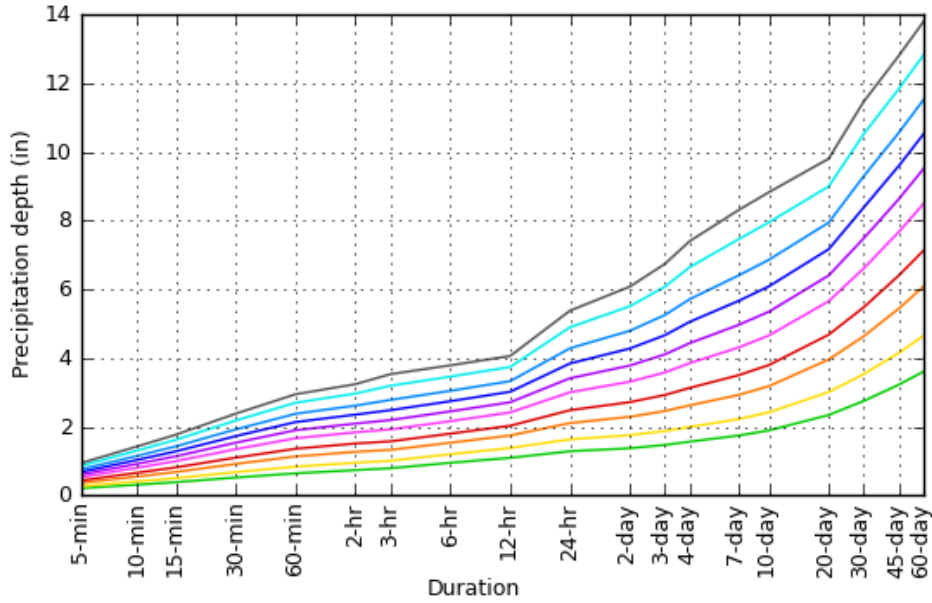
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.204 (0.172-0.245)	0.265 (0.227-0.321)	0.360 (0.304-0.432)	0.431 (0.362-0.516)	0.528 (0.438-0.629)	0.603 (0.493-0.715)	0.678 (0.545-0.803)	0.755 (0.596-0.894)	0.857 (0.659-1.02)	0.936 (0.705-1.12)
10-min	0.310 (0.262-0.373)	0.404 (0.345-0.488)	0.547 (0.462-0.658)	0.657 (0.552-0.785)	0.804 (0.666-0.957)	0.917 (0.749-1.09)	1.03 (0.829-1.22)	1.15 (0.908-1.36)	1.30 (1.00-1.55)	1.42 (1.07-1.70)
15-min	0.384 (0.325-0.462)	0.500 (0.428-0.605)	0.679 (0.573-0.815)	0.814 (0.684-0.973)	0.996 (0.825-1.19)	1.14 (0.929-1.35)	1.28 (1.03-1.52)	1.43 (1.13-1.69)	1.62 (1.24-1.92)	1.77 (1.33-2.10)
30-min	0.517 (0.438-0.623)	0.674 (0.575-0.814)	0.914 (0.772-1.10)	1.10 (0.921-1.31)	1.34 (1.11-1.60)	1.53 (1.25-1.82)	1.72 (1.38-2.04)	1.92 (1.52-2.27)	2.18 (1.68-2.58)	2.38 (1.79-2.83)
60-min	0.640 (0.542-0.771)	0.834 (0.712-1.01)	1.13 (0.955-1.36)	1.36 (1.14-1.62)	1.66 (1.38-1.98)	1.90 (1.55-2.25)	2.13 (1.71-2.53)	2.37 (1.88-2.81)	2.70 (2.07-3.20)	2.94 (2.22-3.51)
2-hr	0.733 (0.626-0.872)	0.950 (0.814-1.13)	1.27 (1.08-1.51)	1.51 (1.27-1.79)	1.83 (1.53-2.16)	2.09 (1.72-2.46)	2.35 (1.90-2.76)	2.61 (2.08-3.07)	2.96 (2.30-3.49)	3.24 (2.45-3.83)
3-hr	0.788 (0.671-0.942)	1.01 (0.861-1.21)	1.32 (1.13-1.59)	1.57 (1.33-1.88)	1.92 (1.59-2.28)	2.19 (1.79-2.59)	2.48 (1.99-2.93)	2.78 (2.19-3.28)	3.19 (2.44-3.77)	3.53 (2.64-4.18)
6-hr	0.947 (0.824-1.11)	1.20 (1.04-1.40)	1.53 (1.33-1.79)	1.80 (1.55-2.09)	2.16 (1.83-2.50)	2.44 (2.05-2.82)	2.74 (2.25-3.16)	3.04 (2.46-3.52)	3.46 (2.72-3.99)	3.78 (2.90-4.38)
12-hr	1.09 (0.961-1.25)	1.38 (1.21-1.58)	1.74 (1.53-1.99)	2.03 (1.77-2.31)	2.41 (2.08-2.74)	2.71 (2.31-3.07)	3.01 (2.53-3.42)	3.32 (2.75-3.77)	3.73 (3.02-4.26)	4.06 (3.21-4.66)
24-hr	1.28 (1.17-1.42)	1.63 (1.48-1.81)	2.10 (1.90-2.33)	2.48 (2.24-2.74)	3.00 (2.69-3.30)	3.41 (3.03-3.75)	3.84 (3.38-4.22)	4.28 (3.74-4.71)	4.89 (4.21-5.40)	5.38 (4.57-5.95)
2-day	1.37 (1.24-1.52)	1.75 (1.59-1.94)	2.29 (2.07-2.53)	2.71 (2.45-3.00)	3.31 (2.96-3.65)	3.78 (3.36-4.16)	4.27 (3.77-4.71)	4.79 (4.18-5.30)	5.50 (4.74-6.11)	6.07 (5.16-6.77)
3-day	1.47 (1.33-1.62)	1.87 (1.70-2.07)	2.45 (2.23-2.71)	2.92 (2.64-3.22)	3.58 (3.22-3.93)	4.10 (3.67-4.51)	4.66 (4.13-5.13)	5.25 (4.61-5.78)	6.07 (5.26-6.71)	6.74 (5.77-7.48)
4-day	1.56 (1.43-1.72)	1.99 (1.82-2.19)	2.62 (2.39-2.88)	3.13 (2.84-3.43)	3.85 (3.47-4.22)	4.43 (3.97-4.86)	5.05 (4.50-5.54)	5.71 (5.04-6.27)	6.64 (5.78-7.32)	7.40 (6.37-8.18)
7-day	1.74 (1.59-1.92)	2.22 (2.02-2.44)	2.92 (2.66-3.22)	3.49 (3.17-3.85)	4.30 (3.87-4.72)	4.95 (4.43-5.45)	5.65 (5.02-6.22)	6.39 (5.62-7.04)	7.44 (6.46-8.23)	8.29 (7.12-9.21)
10-day	1.89 (1.73-2.08)	2.42 (2.20-2.66)	3.18 (2.89-3.50)	3.79 (3.44-4.17)	4.65 (4.20-5.11)	5.34 (4.79-5.87)	6.08 (5.41-6.68)	6.86 (6.05-7.55)	7.95 (6.92-8.78)	8.82 (7.61-9.77)
20-day	2.34 (2.13-2.57)	3.01 (2.74-3.30)	3.95 (3.59-4.34)	4.68 (4.24-5.13)	5.65 (5.10-6.19)	6.40 (5.75-7.01)	7.16 (6.41-7.86)	7.94 (7.06-8.73)	8.99 (7.92-9.92)	9.80 (8.57-10.8)
30-day	2.75 (2.52-3.00)	3.53 (3.24-3.84)	4.63 (4.24-5.05)	5.47 (5.00-5.96)	6.61 (6.00-7.19)	7.48 (6.77-8.15)	8.38 (7.54-9.13)	9.29 (8.31-10.2)	10.5 (9.31-11.5)	11.5 (10.1-12.6)
45-day	3.22 (2.94-3.52)	4.14 (3.78-4.53)	5.44 (4.96-5.94)	6.40 (5.83-6.99)	7.66 (6.95-8.36)	8.62 (7.78-9.41)	9.59 (8.62-10.5)	10.6 (9.43-11.6)	11.8 (10.5-13.0)	12.8 (11.3-14.1)
60-day	3.60 (3.30-3.93)	4.64 (4.25-5.07)	6.08 (5.56-6.64)	7.13 (6.50-7.77)	8.49 (7.72-9.25)	9.51 (8.60-10.4)	10.5 (9.47-11.5)	11.5 (10.3-12.6)	12.8 (11.4-14.1)	13.8 (12.2-15.2)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

**PF graphical**

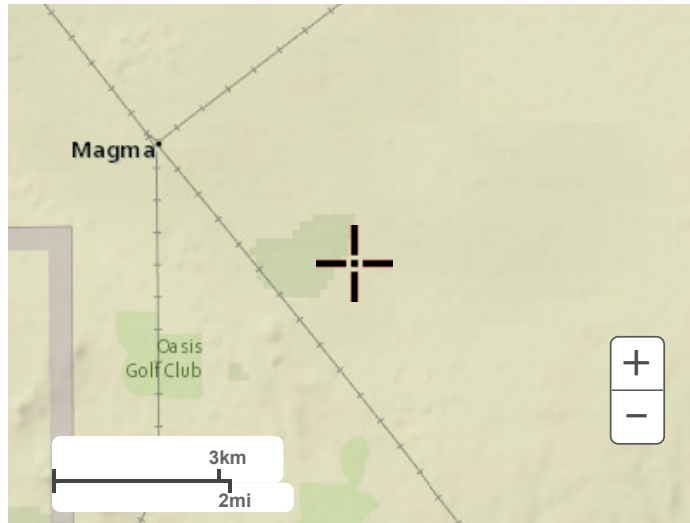
PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 33.1117°, Longitude: -111.4601°



[Back to Top](#)

**Maps & aerials**

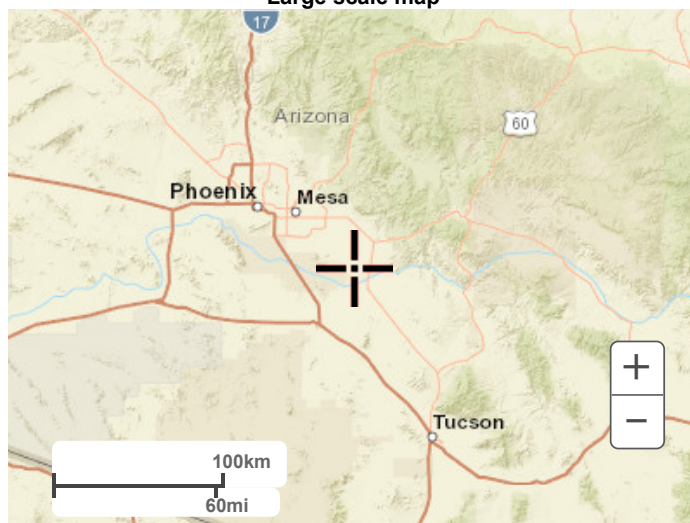
**Small scale terrain**



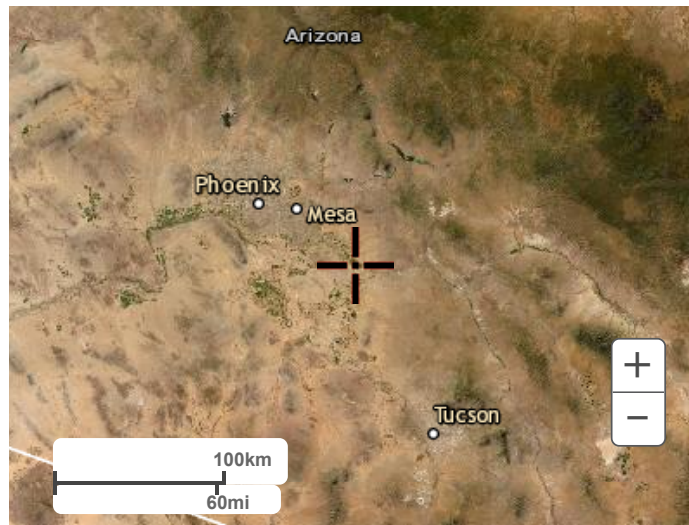
Large scale terrain



Large scale map



Large scale aerial



[Back to Top](#)

---

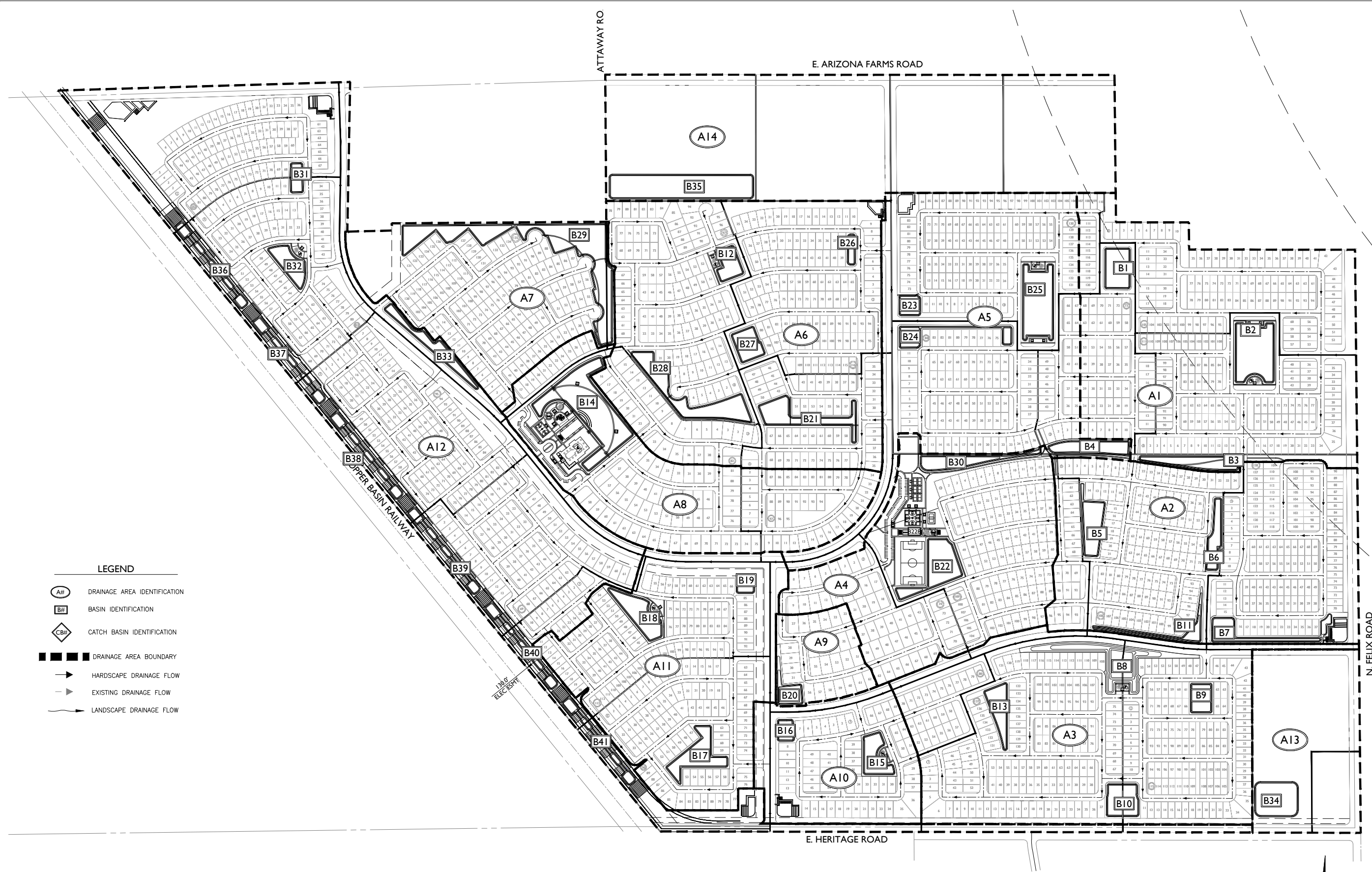
[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

[Disclaimer](#)

# 21-0483 - Arizona Farms

Apr. 20, 2022 2:42pm S:\Projects\2021\21-0483\Civil\Preliminary\Design\Drainage\Preliminary\_Retention\_Analysis\21-0483 - Prelim\_Retention.dwg

- LEGEND**
- A# DRAINAGE AREA IDENTIFICATION
  - B# BASIN IDENTIFICATION
  - CATCH BASIN IDENTIFICATION
  - DRAINAGE AREA BOUNDARY
  - HARDSCAPE DRAINAGE FLOW
  - EXISTING DRAINAGE FLOW
  - LANDSCAPE DRAINAGE FLOW



Revisions:

No.	Description

Designer: EPS  
Drawn by: AJP

## **Appendix B**

### **Preliminary Drainage Calculations**

# Retention Calculations

**Project:** Arizona Farms

**Storm Event:** 100-yr 2-hr

**Prepared by:** Alexis Power

**Date:** 4/20/2022

$$V = C * A * P / 12^{(1)}$$

Where:

V = Runoff Volume

C = Runoff Coefficient

A = Drainage Area

P = 2.35 in

## Surface Retention Basin Volume Calculations

Basin ID	Elevation	Area (ft <sup>2</sup> )	Incremental Volume (ft <sup>3</sup> )	Volume Provided, V <sub>p</sub> (ft <sup>3</sup> )
B1	1530	41,462		
	1531	44,854	43,158	
	1532	48,347	46,600	
	1533	51,940	50,143	139,902
B2	0	89,066		
	1	94,757	91,912	
	2	100,548	97,652	
	3	106,424	103,486	293,050
B3	1528	38,596		
	1529	44,395	41,495	
	1530	50,294	47,344	
	1531	56,293	53,293	142,133
B4	0	36,457		
	1	41,328	38,892	
	2	46,300	43,814	
	3	51,382	48,841	131,548
B5	0	41,280		
	1	45,124	43,202	
	2	50,564	47,844	
	3	55,689	53,126	144,172
B6	0	24,842		
	1	29,294	27,068	
	2	33,844	31,569	
	3	38,478	36,161	94,799
B7	1525	29,336		
	1526	36,509	32,923	
	1527	50,367	43,438	
	1528	59,684	55,025	131,386

# Retention Calculations

**Project:** Arizona Farms

**Storm Event:** 100-yr 2-hr

**Prepared by:** Alexis Power

**Date:** 4/20/2022

B8	0	27,439		
	1	34,831	31,135	
	2	61,549	48,190	
	3	90,203	75,876	155,202

B9	0	23,874		
	1	26,455	25,164	
	2	29,163	27,809	
	3	31,931	30,547	83,521

B10	0	41,766		
	1	45,056	43,411	
	2	48,447	46,752	
	3	51,939	50,193	140,356

B11	0	10,416		
	1	18,330	14,373	
	2	26,977	22,653	
	3	35,949	31,463	68,489

B12	0	24,284		
	1	27,115	25,700	
	2	30,046	28,581	
	3	33,078	31,562	85,843

B13	0	32,365		
	1	36,557	34,461	
	2	40,849	38,703	
	3	45,244	43,047	116,211

B14	0	156,309		
	1	167,108	161,708	
	2	178,007	172,557	
	3	189,009	183,508	517,774

B15	0	31,298		
	1	35,126	33,212	
	2	39,054	37,090	
	3	43,083	41,068	111,370

B16	0	12,221		
	1	14,041	13,131	
	2	15,961	15,001	
	3	17,982	16,972	45,103

B17	0	49,347		
	1	55,383	52,365	
	2	61,530	58,457	
	3	67,762	64,646	175,468

# Retention Calculations

**Project:** Arizona Farms

**Storm Event:** 100-yr 2-hr

**Prepared by:** Alexis Power

**Date:** 4/20/2022

B18	0	45,314		
	1	49,834	47,574	
	2	54,458	52,146	
	3	59,187	56,822	156,542

B19	0	9,552		
	1	11,145	10,349	
	2	12,839	11,992	
	3	14,634	13,737	36,078

B20	0	18,076		
	1	20,266	19,171	
	2	24,847	22,556	
	3	29,939	27,393	69,121

B21	0	49,338		
	1	57,646	53,492	
	2	66,065	61,855	
	3	74,575	70,320	185,667

B22	0	61,558		
	1	67,508	64,533	
	2	73,607	70,557	
	3	79,805	76,706	211,796

B23	0	16,113		
	1	18,154	17,134	
	2	20,293	19,224	
	3	22,533	21,413	57,771

B24	0	17,053		
	1	19,155	18,104	
	2	32,212	25,684	
	3	40,578	36,395	80,183

B25	0	88,575		
	1	94,955	91,765	
	2	101,435	98,195	
	3	107,968	104,702	294,662

B26	0	6,795		
	1	8,638	7,717	
	2	10,582	9,610	
	3	12,627	11,605	28,932

## Retention Calculations

**Project:** Arizona Farms

**Storm Event:** 100-yr 2-hr

**Prepared by:** Alexis Power

**Date:** 4/20/2022

B27	0	30,182		
	1	33,050	31,616	
	2	36,018	34,534	
	3	39,088	37,553	103,703

B28	0	79,274		
	1	88,802	84,038	
	2	98,429	93,615	
	3	108,158	103,294	280,947

B29	0	137,892		
	1	219,453	178,672	
	2	240,005	229,729	
	3	260,545	250,275	658,676

B30	0	31,825		
	1	39,228	35,526	
	2	46,325	42,776	
	3	53,522	49,924	128,226

B31	0	13,121		
	1	15,224	14,172	
	2	17,428	16,326	
	3	19,732	18,580	49,078

B32	0	31,935		
	1	35,336	33,635	
	2	38,837	37,086	
	3	42,439	40,638	111,359

B33	0	32,736		
	1	39,919	36,328	
	2	47,204	43,561	
	3	54,588	50,896	130,785

B34	0	63,285		
	1	67,184	65,234	
	2	71,184	69,184	
	3	75,285	73,235	207,653

B35	0	149,548		
	1	158,632	154,090	
	2	167,817	163,225	
	3	177,102	172,460	489,775

B36	0	14,555		
	1	22,783	18,669	
	2	29,699	26,241	
	3	36,769	33,234	78,144

## Retention Calculations

**Project:** Arizona Farms

**Storm Event:** 100-yr 2-hr

**Prepared by:** Alexis Power

**Date:** 4/20/2022

B37	0	12,740		
	1	22,780	17,760	
	2	29,694	26,237	
	3	36,762	33,228	77,225

B38	0	12,750		
	1	22,808	17,779	
	2	29,737	26,273	
	3	36,824	33,281	77,332

B39	0	12,750		
	1	22,783	17,767	
	2	29,699	26,241	
	3	36,769	33,234	77,241

B40	0	14,555		
	1	22,786	18,670	
	2	29,703	26,244	
	3	36,774	33,239	78,153

B41	0	14,555		
	1	22,855	18,705	
	2	29,821	26,338	
	3	36,941	33,381	78,424

## Volume Required and Summary

Basin ID	Sub-Basin ID	Sub Basin Area Description	Contributing Area (ft <sup>2</sup> )	C =	Volume Required, V <sub>R</sub> (ft <sup>3</sup> )	Volume Provided, V <sub>P</sub> (ft <sup>3</sup> )	Estimated Water Depth (ft)
B1 - B3	A1	Single-Family Residential	3,051,534	0.80	478,074		
		Total	3,051,534	0.80	478,074	575,084	2.49
B5 - B7, B11	A2	Single-Family Residential	2,622,442	0.80	410,849		
		Total	2,622,442	0.80	410,849	438,846	2.81
B8-10, B13,	A3	Single-Family Residential	3,104,943	0.80	486,441		
		Total	3,104,943	0.80	486,441	495,290	2.95
B22, B30	A4	Single-Family Residential	1,967,471	0.80	308,237		
		Total	1,967,471	0.80	308,237	340,023	2.72
B4, B23-B25	A5	Single-Family Residential	2,691,698	0.80	421,699		
		Total	2,691,698	0.80	421,699	564,164	2.24
B12, B21, B26-B28	A6	Single-Family Residential	3,466,649	0.80	543,108		
		Total	3,466,649	0.80	543,108	685,092	1211.33
B29	A7	Single-Family Residential	1,561,231	0.80	244,593		
		Total	1,561,231	0.80	244,593	658,676	1.11
B14	A8	Single-Family Residential	1,714,978	0.80	268,680		
		Total	1,714,978	0.80	268,680	517,774	1.56

## Retention Calculations

**Project:** Arizona Farms

**Storm Event:** 100-yr 2-hr

**Prepared by:** Alexis Power

**Date:** 4/20/2022

B20	A9	Single-Family Residential	381,836	0.80	59,821		
		Total	381,836	0.80	59,821	69,121	1.73
B15-B16	A10	Single-Family Residential	971,548	0.80	152,209		
		Total	971,548	0.80	152,209	156,473	1.95
B17-B19	A11	Single-Family Residential	2,096,852	0.80	328,507		
		Total	2,096,852	0.80	328,507	368,088	2.68
B31-B33, B36-B41	A13	Single-Family Residential	5,545,281	0.80	868,761		
		Total	5,545,281	0.80	868,761	870,964	2.99
B34	A14	Commercial	964,994	0.80	151,182		
		Total	964,994	0.80	151,182	207,653	1.46
B35	A15	Commercial	3,113,369	0.80	487,761		
		Total	3,113,369	0.80	487,761	489,775	1.99

# **Appendix C**

## **Offsite Drainage Report**

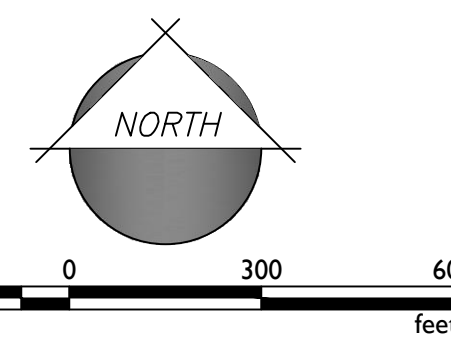
# ARIZONA FARMS CONCEPTUAL SITE PLAN with CHANNEL LOCATIONS

E. ARIZONA FARMS ROAD



Parcel	Proposed Land Use	Net Acreage	Min. Lot Size	Density (du/ac)	Lot Yield
1	MDR	29.3	48x115		85
2	MLDR	27.1	53x120		88
3	MDR	21.1	48x115		72
4	MLDR	25.3	58x120		82
5	MDR	30.9	48x115		130
6	MLDR	26.8	53x120		90
7	MR	23.0	48x115		345
8	MLDR	35.4	53x120		133
9	MLDR	24.4	58x120		106
10	MLDR	31.9	53x120		124
11	MLDR	22.7	70x120		38
12	MLDR	27.1	70x130		74
13/14	MLDR	27.2	58x120		92
15	MLDR	24.6	58x130		70
16	MLDR	14.2	53x120		56
17	MLDR	27.5	53x120		97
18	MDR	25.1	48x115		110
19	MR	17.5	-	15+	262.5
20	MLDR	24.1	70x130		64
21	MLDR	28.7	58x130		100
22	MDR	16.5	48x115		76
23	MLDR	15.1	53x120		45
24	MR	28.2	53x120	15+	108
25	MLDR	28.7	53x120		117
26	MLDR	23.5	58x120		93
27A	MDR	32.0	48x115		139
27B	MLDR	16.3	53x120		73
27C	COM	4.2	-	-	-
28	MDR	22.7	48x115		111
29	COM	19.7	-	-	-
30*	COM	15.0	-	-	-
31	MR	14.8	-	15+	222
<b>Total</b>					<b>3203</b>

**Notes**  
 10\* Land Use Plan shows a second Parcel 10 located at the SEC of the project  
 NSC\* North-South Corridor  
 30\* Parcel 30 was split in half resulting in a 10-acre COM parcel and 10-acre MR parcel



**Existing Condition 100-year, 6-hour  
HEC-1 Output**

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 07JUN17 TIME 10:41:04
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Flood Control District of Pinal County
2 ID AZ FARMS EX 100YR6HR - Arizona Farms MDR Existing Condition 100YR, 6HR
3 ID 100 YEAR
4 ID 6 Hour Storm
5 ID Unit Hydrograph: Clark
6 ID Storm: Multiple
7 ID FILE NAME: EX100YR6HR.DAT
8 ID BY: WOOD/PATEL JCD
9 ID 11/03/2016
*DIAGRAM
10 IT 2 1JAN99 0 2000
11 IO 5
12 IN 15
*
13 JD 2.74 0.0001
14 PC 0.000 0.008 0.016 0.025 0.033 0.041 0.050 0.058 0.066 0.074
15 PC 0.087 0.099 0.118 0.138 0.216 0.377 0.834 0.911 0.931 0.950
16 PC 0.962 0.972 0.983 0.991 1.000
17 JD 2.72 0.5000
18 PC 0.000 0.008 0.016 0.025 0.033 0.041 0.050 0.058 0.066 0.074
19 PC 0.087 0.099 0.118 0.138 0.216 0.377 0.834 0.911 0.931 0.950
20 PC 0.962 0.972 0.983 0.991 1.000
21 JD 2.67 2.8
22 PC 0.000 0.009 0.016 0.025 0.034 0.042 0.051 0.059 0.067 0.076
23 PC 0.087 0.100 0.120 0.163 0.252 0.451 0.694 0.837 0.900 0.938
24 PC 0.950 0.963 0.975 0.988 1.000
25 JD 2.53 16.0
26 PC 0.000 0.015 0.020 0.030 0.048 0.063 0.076 0.090 0.105 0.119
27 PC 0.135 0.152 0.175 0.222 0.304 0.472 0.670 0.796 0.868 0.912
28 PC 0.946 0.960 0.973 0.987 1.000
*
29 KK OFF A BASIN
30 BA 0.553
31 LG 0.50 0.00 7.58 0.15 0
32 UC 3.302 1.934
33 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
34 UA 100
*
35 KK DA9 DIVERT
36 DT DTA9 0.0 0.0
37 DI 0.0 66.0 206.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
38 DQ 0.0 9.0 55.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
*
39 KK RAB ROUTE
40 RS 7 FLOW
41 RC 0.016 0.025 0.025 5100 0.0025 0.00
42 RX 0.00 0.00 3.00 15.00 30.00 35.00 39.00 54.00
43 RY 1538.0 1538.00 1537.00 1536.00 1536.00 1537.00 1538.00 1539.00
*
*

```

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
44 KK OFF B BASIN
45 BA 0.584
46 LG 0.50 0.00 4.87 0.46 0
47 UC 4.401 3.738
48 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
49 UA 100
*

```

```

50      KK      CBAB COMBINE
51      HC          2
      *

52      KK      ON 1  BASIN
53      BA      0.023
54      LG      0.50      0.00      5.05      0.42      3
55      UC      1.045      1.146
56      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
57      UA      100
      *

58      KK      OFF C  BASIN
59      BA      0.481
60      LG      0.50      0.00      7.58      0.15      0
61      UC      3.874      3.202
62      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
63      UA      100
      *

64      KK      RCF  ROUTE
65      RS      6          FLOW
66      RC      0.016      0.025      0.025      2290      0.0022      0.00
67      RX      0.00      0.00      11.00      15.00      42.00      54.00      65.00      69.00
68      RY      1536.0      1536.00      1535.00      1534.00      1534.00      1535.00      1535.00      1536.00
      *
      *

69      KK      OFF D  BASIN
70      KO
71      BA      0.887
72      LG      0.35      0.34      7.00      0.10      0
73      UC      2.221      1.995
74      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
75      UA      100
      *

76      KK      DD STORAGE
77      KO
78      RS      1          STOR
79      SV      12.00      45.00
80      SQ      0.00      70.00
81      SE      1559.6      1561.60      1563.60
      *
      *

```

1

HEC-1 INPUT

PAGE 3

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

82      KK      RED  ROUTE
83      RS      4          FLOW
84      RC      0.025      0.025      0.025      2210      0.0027      0.00
85      RX      0.00      0.00      0.00      6.00      10.00      16.00      16.00      16.00
86      RY      1557.0      1557.00      1557.00      1554.00      1554.00      1557.00      1557.00      1557.00
      *
      *

87      KK      OFF E  BASIN
88      BA      0.124
89      LG      0.35      0.36      5.05      0.23      0
90      UC      0.659      0.432
91      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
92      UA      100
      *

93      KK      CBDE COMBINE
94      *          1          2
      HC          2
      *

95      KK      REF  ROUTE
96      *          40          2
      RS      169          FLOW
97      RC      0.025      0.016      0.025      10410      0.0019      0.00
98      RX      0.00      2.00      35.00      49.00      63.00      80.00      88.00      90.00
99      RY      1542.0      1540.00      1540.00      1540.28      1540.28      1540.00      1540.00      1542.00
      *
      *

100     KK      OFF F  BASIN
101     BA      1.187
102     LG      0.50      0.00      8.36      0.12      0
103     UC      5.749      4.831
104     UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
105     UA      100
      *

106     KK      CBEF COMBINE
107     HC          2
      *

108     KK      CPF COMBINE
109     HC          2
      *

110     KK      DF  DIVERT
111     DT      DTF      0.0          0.0
112     DI      0.0      120.0      328.0      0.0          0.0          0.0          0.0          0.0          0.0          0.0
113     DQ      0.0          0.0          79.0      0.0          0.0          0.0          0.0          0.0          0.0          0.0
      *
      *

```

1

HEC-1 INPUT

PAGE 4

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```



180 KK R67 ROUTE  
 181 KO  
 182 RS 16 FLOW  
 183 RC 0.050 0.035 0.050 1500 0.0010 0.00  
 184 RX 0.00 3.00 1261.00 1267.00 1273.00 1278.00 1311.00 1410.00  
 185 RY 1511.0 1510.00 1510.00 1508.00 1508.00 1510.00 1510.00 1511.00  
 \*  
 \*

1

HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

186 KK ON 7 BASIN  
 187 BA 0.193  
 188 LG 0.50 0.01 5.71 0.31 0  
 189 UC 3.014 2.840  
 190 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0  
 191 UA 100  
 \*

192 KK CB67 COMBINE  
 193 HC 2  
 \*

194 KK R78 ROUTE  
 195 KO  
 196 RS 11 FLOW  
 197 RC 0.050 0.035 0.050 1350 0.0015 0.00  
 198 RX 0.00 2.00 230.00 1296.00 1305.00 1307.00 1310.00 1315.00  
 199 RY 1510.0 1509.00 1508.00 1509.00 1507.00 1507.00 1509.00 1510.00  
 \*

200 KK MR BASIN  
 201 KM MAGIC RANCH HYDROGRAPH FROM HEC-HMS DRAINAGE REPORT OUTPUT  
 202 BA 1.369  
 203 QI 0 0 0 0 0 0 0 0 0 0  
 204 QI 0 0 0 0 0 0 0 0 0 0  
 205 QI 0 0 0 0 0 0 0 0 0 0  
 206 QI 0 0 0 0 0 0 0 0 0 0  
 207 QI 0 0 0 0 0 0 0 0 0 0  
 208 QI 0 20 22 24 27 30 33 34 35 36  
 209 QI 36 36 36 36 36 36 36 36 36 36  
 210 QI 36 36 36 36 36 36 36 36 36 36  
 211 QI 36 36 36 36 36 36 36 36 36 36  
 212 QI 36 36 36 36 36 36 36 36 36 36  
 213 QI 36 36 36 36 36 36 36 36 36 36  
 214 QI 36 36 36 36 36 36 36 36 36 36  
 215 QI 36 36 36 36 36 36 36 36 36 36  
 216 QI 36 36 36 36 36 36 36 36 36 36  
 217 QI 36 36 36 36 36 36 36 36 36 36  
 218 QI 36 36 36 36 36 36 36 36 36 36  
 219 QI 36 36 36 36 36 36 36 36 36 36  
 220 QI 36 36 36 36 36 36 36 36 36 36  
 221 QI 36 36 36 36 36 36 36 36 36 36  
 222 QI 36 36 36 36 36 36 36 36 36 36  
 223 QI 36 36 36 36 36 36 36 36 36 36  
 224 QI 36 36 36 36 36 36 36 36 36 36  
 225 QI 36 36 36 36 36 36 36 36 36 36  
 226 QI 36 36 36 36 36 36 36 36 36 36  
 227 QI 36 36 36 36 36 36 36 36 36 36  
 228 QI 36 36 36 36 36 36 36 36 36 36  
 229 QI 36 36 36 36 36 36 36 36 36 36  
 230 QI 36 36 36 36 36 36 36 36 36 36  
 231 QI 36 36 36 36 36 36 36 36 36 36  
 232 QI 36 36 36 36 36 36 36 36 36 36  
 233 QI 36 36 36 36 36 36 36 36 36 36  
 \*

1

HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

234 QI 36 36 36 36 36 36 36 36 36 36  
 235 QI 36 36 36 36 36 36 36 36 36 36  
 236 QI 36 36 36 36 36 36 36 36 36 36  
 237 QI 36 36 36 36 36 36 36 36 36 36  
 238 QI 36 36 36 36 36 36 36 36 36 36  
 239 QI 36 36 36 36 36 36 36 36 36 36  
 240 QI 36 36 36 36 36 36 36 36 36 36  
 241 QI 36 36 36 36 36 36 36 36 36 36  
 242 QI 36 36 36 36 36 36 36 36 36 36  
 243 QI 36 36 36 36 36 36 36 36 36 36  
 \*

244 KK RMR ROUTE  
 245 KO  
 246 RS 71 FLOW  
 247 RC 0.050 0.050 0.050 7240 0.0014 0.00  
 248 RX 0.00 0.00 0.00 6.00 106.00 112.00 112.00 112.00  
 249 RY 1510.0 1510.00 1510.00 1509.00 1509.00 1510.00 1510.00 1510.00  
 \*  
 \*

250 KK OFF K BASIN  
 251 BA 0.505  
 252 LG 0.30 0.23 6.16 0.17 5  
 253 UC 1.543 1.047  
 254 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0  
 255 UA 100  
 \*

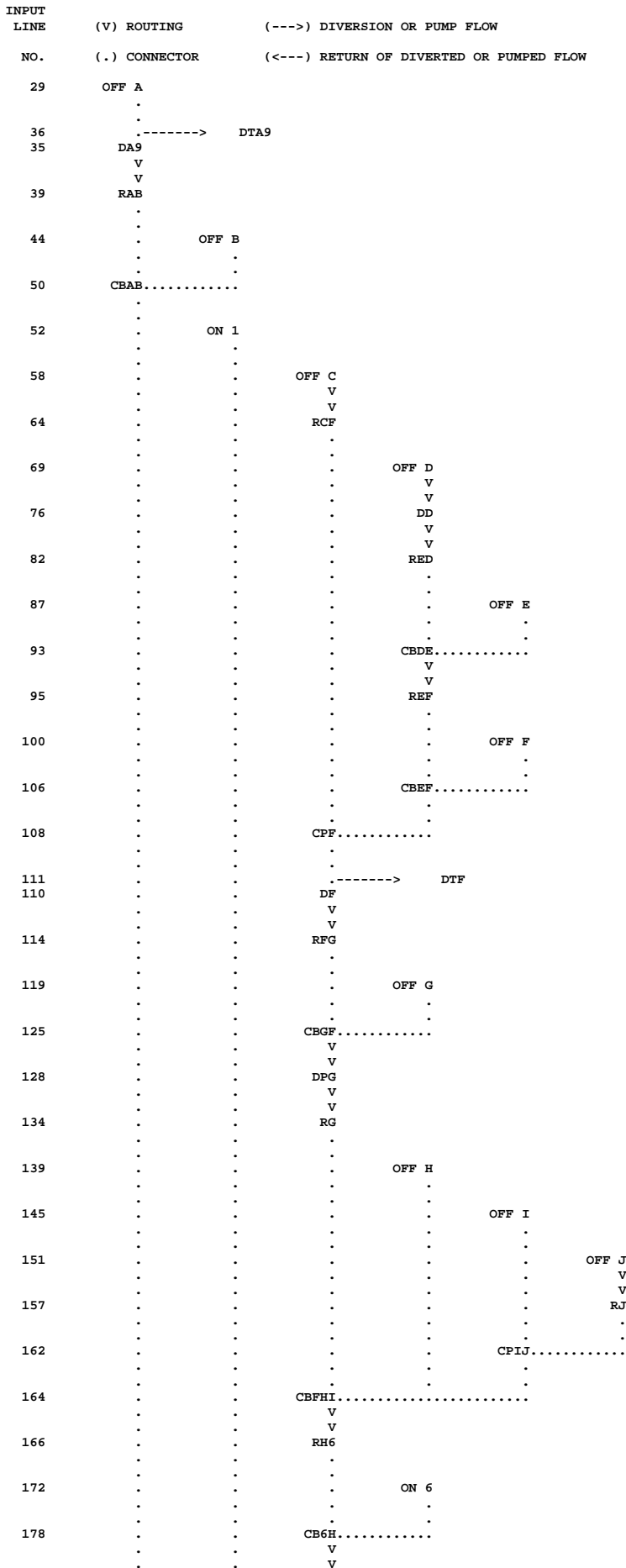
256 KK CB7K COMBINE  
 257 HC 3  
 \*

258 KK OFF L BASIN





SCHEMATIC DIAGRAM OF STREAM NETWORK



```

180      .      .      R67
      .      .      .
186      .      .      .      ON 7
      .      .      .      .
192      .      .      CB67.....
      .      .      V
      .      .      V
194      .      .      R78
      .      .      .
200      .      .      .      MR
      .      .      .      V
      .      .      .      V
244      .      .      .      RMR
      .      .      .      .
250      .      .      .      .      OFF K
      .      .      .      .      .
256      .      .      .      CB7K.....
      .      .      .      .
258      .      .      .      .      OFF L
      .      .      .      .      V
      .      .      .      .      V
264      .      .      .      .      RL8
      .      .      .      .      .
269      .      .      .      .      .      ON 8
      .      .      .      .      .
275      .      .      .      .      CB8L.....
      .      .      .      .
277      .      .      .      .      CP8.....
      .      .      .      .      V
      .      .      .      .      V
279      .      .      .      .      DET8
      .      .      .      .
286      .      .      .      .      .      <----- DTF
285      .      .      .      .      DF
      .      .      .      .      V
      .      .      .      .      V
287      .      .      .      .      RF
      .      .      .      .      .
292      .      .      .      .      .      OFF M
      .      .      .      .      .
298      .      .      .      .      .      CFPM.....
      .      .      .      .      V
      .      .      .      .      V
300      .      .      .      .      RFM
      .      .      .      .      .
305      .      .      .      .      .      ON 3
      .      .      .      .      .
311      .      .      .      .      .      CFM3.....
      .      .      .      .      V
      .      .      .      .      V
313      .      .      .      .      D23
      .      .      .      .      V
319      .      .      .      .      R24
      .      .      .      .
325      .      .      .      .      .      <----- DTA9
324      .      .      .      .      DA9
      .      .      .      .      V
      .      .      .      .      V
326      .      .      .      .      RA4
      .      .      .      .      .
331      .      .      .      .      .      .      OFF N
      .      .      .      .      .      V
      .      .      .      .      .      V
337      .      .      .      .      .      .      RN
      .      .      .      .      .
342      .      .      .      .      .      CP4N.....
      .      .      .      .      V
      .      .      .      .      V
344      .      .      .      .      .      RA4N
      .      .      .      .      .
349      .      .      .      .      .      .      ON 4
      .      .      .      .      .
355      .      .      .      .      .      CP24.....
      .      .      .      .      .
357      .      .      .      .      .      .      ON 5
      .      .      .      .      .
363      .      .      .      .      .      CB45.....
      .      .      .      .      V
      .      .      .      .      V
365      .      .      .      .      .      RET4

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 07JUN17 TIME 10:41:04 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

```

Flood Control District of Pinal County
AZ FARMS EX 100YR6HR - Arizona Farms MDR Existing Condition 100YR, 6HR
100 YEAR
6 Hour Storm
Unit Hydrograph: Clark
Storm: Multiple
FILE NAME: EX100YR6HR.DAT
BY: WOOD/PATEL JCD
11/03/2016

```

```

11 IO      OUTPUT CONTROL VARIABLES
          IPRT      5  PRINT CONTROL
          IPLOT     0  PLOT CONTROL
          QSCAL    0.  HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN      2  MINUTES IN COMPUTATION INTERVAL
          IDATE     1JAN99  STARTING DATE
          ITIME     0000  STARTING TIME
          NQ        2000  NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    3JAN99  ENDING DATE
          NDTIME    1838  ENDING TIME
          ICENT     19  CENTURY MARK

          COMPUTATION INTERVAL .03 HOURS
          TOTAL TIME BASE     66.63 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH  INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-Feet
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

```

13 JD      INDEX STORM NO. 1
          STRM      2.74  PRECIPITATION DEPTH
          TRDA      .00  TRANSPOSITION DRAINAGE AREA

```

```

14 PI      PRECIPITATION PATTERN
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .01 .01 .01 .01 .01 .02 .02 .02 .02 .02
          .02 .02 .04 .06 .06 .06 .06 .06 .06 .06
          .01 .01 .01 .01 .01 .01 .01 .01 .01 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

```

```

17 JD      INDEX STORM NO. 2
          STRM      2.72  PRECIPITATION DEPTH
          TRDA      .50  TRANSPOSITION DRAINAGE AREA

```

```

18 PI      PRECIPITATION PATTERN
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .01 .01 .01 .01 .01 .02 .02 .02 .02 .02
          .02 .02 .04 .06 .06 .06 .06 .06 .06 .06
          .01 .01 .01 .01 .01 .01 .01 .01 .01 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

```

```

21 JD      INDEX STORM NO. 3
          STRM      2.67  PRECIPITATION DEPTH
          TRDA      2.80  TRANSPOSITION DRAINAGE AREA

```

```

22 PI      PRECIPITATION PATTERN
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

```

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

25 JD INDEX STORM NO. 4  
 STRM 2.53 PRECIPITATION DEPTH  
 TRDA 16.00 TRANSPOSITION DRAINAGE AREA

26 PI PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.02	.02	.02	.02	.02
.02	.02	.02	.03	.03	.03	.03	.03	.03	.03	.03
.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 69 KK \* OFF D \* BASIN  
 \* \*  
 \*\*\*\*\*

70 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 76 KK \* DD \* STORAGE  
 \* \*  
 \*\*\*\*\*

77 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 125 KK \* CBGF \* COMBINE  
 \* \*  
 \*\*\*\*\*

126 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 128 KK \* DPG \* STORAGE  
 \* \*  
 \*\*\*\*\*

129 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
166 KK \* RH6 \* ROUTE  
\* \*  
\*\*\*\*\*

167 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
180 KK \* R67 \* ROUTE  
\* \*  
\*\*\*\*\*

181 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
194 KK \* R78 \* ROUTE  
\* \*  
\*\*\*\*\*

195 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
244 KK \* RMR \* ROUTE  
\* \*  
\*\*\*\*\*

245 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
279 KK \* DET8 \* STORAGE  
\* \*  
\*\*\*\*\*

280 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
313 KK \* D23 \* STORAGE  
\* \*  
\*\*\*\*\*

314 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
365 KK \* RET4 \* STORAGE  
\* \*  
\*\*\*\*\*

\*\*\*\*\*

366 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	OFF A	208.	6.53	101.	27.	10.	.55		
DIVERSION TO	DTA9	56.	6.53	22.	6.	2.	.55		
HYDROGRAPH AT	DA9	152.	6.53	79.	22.	8.	.55		
ROUTED TO	RAB	151.	6.77	78.	22.	8.	.55		
HYDROGRAPH AT	OFF B	108.	7.47	72.	21.	8.	.58		
2 COMBINED AT	CBAB	238.	7.10	144.	41.	15.	1.14		
HYDROGRAPH AT	ON 1	15.	4.80	4.	1.	0.	.02		
HYDROGRAPH AT	OFF C	123.	7.03	76.	22.	8.	.48		
ROUTED TO	RCF	123.	7.23	76.	22.	8.	.48		
HYDROGRAPH AT	OFF D	265.	5.77	119.	32.	12.	.89		
ROUTED TO	DD	63.	8.87	56.	25.	9.	.89		
ROUTED TO	RED	63.	9.00	56.	25.	9.	.89		
HYDROGRAPH AT	OFF E	124.	4.43	16.	4.	1.	.12		
2 COMBINED AT	CBDE	108.	4.43	56.	29.	11.	1.01		
ROUTED TO	REF	72.	5.73	55.	28.	10.	1.01		
HYDROGRAPH AT	OFF F	203.	8.63	153.	44.	16.	1.19		
2 COMBINED AT	CBEF	250.	8.93	196.	69.	25.	2.20		
2 COMBINED AT	CPF	335.	8.50	258.	89.	33.	2.68		
DIVERSION TO	DTF	82.	8.50	53.	14.	5.	2.68		
HYDROGRAPH AT	DF	253.	8.50	206.	75.	28.	2.68		
ROUTED TO	RFG	253.	8.80	206.	75.	28.	2.68		
HYDROGRAPH AT	OFF G	284.	9.43	220.	62.	22.	1.90		
2 COMBINED AT	CBGF	510.	9.30	409.	132.	48.	4.57		
ROUTED TO	DPG	188.	13.90	178.	123.	48.	4.57		
ROUTED TO	RG	188.	14.00	178.	123.	48.	4.57		
HYDROGRAPH AT	OFF H	11.	6.53	8.	3.	1.	.06		
HYDROGRAPH AT	OFF I	82.	7.07	53.	16.	6.	.31		
HYDROGRAPH AT	OFF J	230.	6.67	115.	31.	11.	.68		
ROUTED TO	RJ	230.	6.70	115.	31.	11.	.68		
2 COMBINED AT	CPIJ	301.	6.80	165.	46.	17.	.99		
3 COMBINED AT	CBFHI	311.	7.03	253.	163.	64.	5.63		
ROUTED TO	RH6	308.	7.83	251.	163.	64.	5.63		

+	HYDROGRAPH AT	ON 6	83.	6.07	38.	10.	4.	.22
+	2 COMBINED AT	CB6H	343.	7.77	265.	171.	67.	5.85
+	ROUTED TO	R67	340.	8.30	264.	171.	67.	5.85
+	HYDROGRAPH AT	ON 7	49.	6.37	28.	8.	3.	.19
+	2 COMBINED AT	CB67	362.	8.30	276.	176.	69.	6.04
+	ROUTED TO	R78	360.	8.67	275.	176.	69.	6.04
+	HYDROGRAPH AT	MR	36.	14.77	36.	36.	29.	1.37
+	ROUTED TO	RMR	36.	17.17	36.	36.	27.	1.37
+	HYDROGRAPH AT	OFF K	278.	5.13	79.	20.	7.	.50
+	3 COMBINED AT	CB7K	364.	8.67	275.	204.	101.	7.91
+	HYDROGRAPH AT	OFF L	89.	4.17	7.	2.	1.	.05
+	ROUTED TO	RL8	78.	4.30	7.	2.	1.	.05
+	HYDROGRAPH AT	ON 8	76.	5.90	33.	9.	3.	.23
+	2 COMBINED AT	CB8L	83.	4.30	40.	11.	4.	.28
+	2 COMBINED AT	CP8	374.	8.67	280.	209.	103.	8.19
+	ROUTED TO	DET8	364.	8.90	280.	205.	102.	8.19
+	HYDROGRAPH AT	DF	82.	8.50	53.	14.	5.	2.68
+	ROUTED TO	RF	81.	9.17	52.	14.	5.	2.68
+	HYDROGRAPH AT	OFF M	25.	5.37	9.	2.	1.	.07
+	2 COMBINED AT	CPFM	95.	8.93	61.	19.	7.	.07
+	ROUTED TO	RFM	94.	9.17	61.	19.	7.	.07
+	HYDROGRAPH AT	ON 3	35.	5.67	16.	4.	2.	.10
+	2 COMBINED AT	CPM3	101.	9.10	64.	23.	8.	.16
+	ROUTED TO	D23	52.	11.97	42.	15.	6.	.16
+	ROUTED TO	R24	52.	12.30	42.	15.	6.	.16
+	HYDROGRAPH AT	DA9	56.	6.53	22.	6.	2.	.55
+	ROUTED TO	RA4	55.	7.20	22.	6.	2.	.55
+	HYDROGRAPH AT	OFF N	47.	5.00	12.	3.	1.	.07
+	ROUTED TO	RN	45.	5.53	12.	3.	1.	.07
+	2 COMBINED AT	CP4N	65.	7.07	34.	9.	3.	.07
+	ROUTED TO	RA4N	65.	7.50	34.	9.	3.	.07
+	HYDROGRAPH AT	ON 4	141.	7.97	98.	29.	10.	.85
+	3 COMBINED AT	CP24	196.	7.83	137.	50.	18.	1.08
+	HYDROGRAPH AT	ON 5	52.	6.70	32.	10.	3.	.24
+	2 COMBINED AT	CB45	232.	7.77	162.	58.	21.	1.32

+           ROUTED TO           RET4       232.   7.87           161.       56.       20.       1.32

\*\*\* NORMAL END OF HEC-1 \*\*\*

**Existing Condition 100-year, 24-hour  
HEC-1 Output**

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 07JUN17 TIME 10:41:12
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Flood Control District of Pinal County
2 ID AZ FARMS EX 100YR24HR - Arizona Farms MDR Existing Condition 100YR, 24HR
3 ID 100 YEAR
4 ID 24 Hour Storm
5 ID Unit Hydrograph: Clark
6 ID Storm: Multiple
7 ID FILE NAME: EX100YR24HR.DAT
8 ID BY: WOOD/PATEL JCD
9 ID 11/03/2016
*DIAGRAM
10 IT 2 1JAN99 0 2000
11 IO 5
12 IN 15
*
13 JD 3.84 0.0001
14 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
15 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
16 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
17 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
18 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
19 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
20 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
21 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
22 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
23 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
24 JD 3.648 10.0
*
25 KK OFF A BASIN
26 BA 0.553
27 LG 0.50 0.00 7.58 0.15 0
28 UC 3.302 1.934
29 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
30 UA 100
*
31 KK DA9 DIVERT
32 DT DTA9 0.0 0.0
33 DI 0.0 66.0 206.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
34 DQ 0.0 9.0 55.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
*
35 KK RAB ROUTE
36 RS 9 FLOW
37 RC 0.016 0.025 0.025 5100 0.0025 0.00
38 RX 0.00 0.00 3.00 15.00 30.00 35.00 39.00 54.00
39 RY 1538.0 1538.00 1537.00 1536.00 1536.00 1537.00 1538.00 1539.00
*
*

```

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 KK OFF B BASIN
41 BA 0.584
42 LG 0.50 0.00 4.87 0.46 0
43 UC 4.401 3.738
44 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
45 UA 100
*
46 KK CBAB COMBINE
47 HC 2
*

```

48	KK	ON 1	BASIN								
49	BA	0.023									
50	LG	0.50	0.00	5.05	0.42	3					
51	UC	1.045	1.146								
52	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
53	UA	100									
	*										
54	KK	OFF C	BASIN								
55	BA	0.481									
56	LG	0.50	0.00	7.58	0.15	0					
57	UC	3.874	3.202								
58	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
59	UA	100									
	*										
60	KK	RCF	ROUTE								
61	RS	6	FLOW								
62	RC	0.016	0.025	0.025	2290	0.0022	0.00				
63	RX	0.00	0.00	11.00	15.00	42.00	54.00	65.00	69.00		
64	RY	1536.0	1536.00	1535.00	1534.00	1534.00	1535.00	1535.00	1536.00		
	*										
	*										
65	KK	OFF D	BASIN								
66	KO										
67	BA	0.887									
68	LG	0.35	0.34	7.00	0.10	0					
69	UC	2.221	1.995								
70	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
71	UA	100									
	*										
72	KK	DD	STORAGE								
73	KO										
74	RS	1	STOR								
75	SV		12.00	45.00							
76	SQ		0.00	70.00							
77	SE	1559.6	1561.60	1563.60							
	*										
	*										

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

78	KK	RED	ROUTE								
79	RS	4	FLOW								
80	RC	0.025	0.025	0.025	2210	0.0027	0.00				
81	RX	0.00	0.00	0.00	6.00	10.00	16.00	16.00	16.00		
82	RY	1557.0	1557.00	1557.00	1554.00	1554.00	1557.00	1557.00	1557.00		
	*										
	*										
83	KK	OFF E	BASIN								
84	BA	0.124									
85	LG	0.35	0.36	5.05	0.23	0					
86	UC	0.659	0.432								
87	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
88	UA	100									
	*										
89	KK	CBDE	COMBINE								
	*	1	2								
90	HC	2									
	*										
91	KK	REF	ROUTE								
	*	40	2								
92	RS	36	FLOW								
93	RC	0.025	0.016	0.025	10410	0.0019	0.00				
94	RX	0.00	2.00	35.00	49.00	63.00	80.00	88.00	90.00		
95	RY	1542.0	1540.00	1540.00	1540.28	1540.28	1540.00	1540.00	1542.00		
	*										
	*										
96	KK	OFF F	BASIN								
97	BA	1.187									
98	LG	0.50	0.00	8.36	0.12	0					
99	UC	5.749	4.831								
100	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
101	UA	100									
	*										
102	KK	CBEF	COMBINE								
103	HC	2									
	*										
104	KK	CPF	COMBINE								
105	HC	2									
	*										
106	KK	DF	DIVERT								
107	DT	DTF	0.0	0.0							
108	DI	0.0	120.0	328.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
109	DQ	0.0	0.0	79.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	*										

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

110	KK	RFG	ROUTE								
111	RS	7	FLOW								
112	RC	0.030	0.025	0.050	3665	0.0022	0.00				

113	RX	0.00	13.00	18.00	40.00	78.00	100.00	110.00	115.00		
114	RY	1523.0	1522.00	1521.00	1520.00	1520.00	1520.00	1520.00	1521.00		
	*										
	*										
115	KK	OFF G	BASIN								
116	BA	1.896									
117	LG	0.50	0.00	7.27	0.16	0					
118	UC	6.830	5.088								
119	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
120	UA	100									
	*										
121	KK	CBGF	COMBINE								
122	KO										
123	HC	2									
	*										
124	KK	DPG	STORAGE								
125	KO	0									
126	RS	1	STOR								
127	SV	0	9.1	62.5	204.8	331.8					
128	SQ	0	31.0	122.2	223.4	256.4					
129	SE	1514	1516	1518	1520	1521					
	*										
	*										
130	KK	RG	ROUTE								
131	RS	4	FLOW								
132	RC	0.050	0.050	0.050	1100	0.0045	0.00				
133	RX	0.00	28.00	33.00	35.00	40.00	44.00	195.00	200.00		
134	RY	1517.0	1516.00	1515.00	1514.00	1514.00	1515.00	1516.00	1517.00		
	*										
	*										
135	KK	OFF H	BASIN								
136	BA	0.064									
137	LG	0.50	0.00	12.49	0.03	0					
138	UC	2.699	6.406								
139	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
140	UA	100									
	*										
141	KK	OFF I	BASIN								
142	BA	0.310									
143	LG	0.50	0.00	10.22	0.05	0					
144	UC	3.800	3.404								
145	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
146	UA	100									
	*										

1

HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10										
147	KK	OFF J	BASIN								
148	BA	0.680									
149	LG	0.50	0.00	6.34	0.24	0					
150	UC	3.518	2.001								
151	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
152	UA	100									
	*										
	*										
153	KK	RJ	ROUTE								
154	RS	1	FLOW								
155	RC	0.030	0.030	2.720	2720	0.3900	0.00				
156	RX	0.00	2.00	5.00	8.00	12.00	15.00	18.00	20.00		
157	RY	1518.0	1518.00	1517.00	1516.00	1516.00	1517.00	1518.00	1518.00		
	*										
	*										
158	KK	CPIJ	COMBINE								
159	HC	2									
	*										
	*										
160	KK	CBFHI	COMBINE								
161	HC	3									
	*										
162	KK	RH6	ROUTE								
163	KO										
164	RS	25	FLOW								
165	RC	0.050	0.035	0.050	2550	0.0010	0.00				
166	RX	0.00	50.00	950.00	957.00	963.00	967.00	970.00	1040.00		
167	RY	1513.0	1512.50	1512.00	1509.00	1509.00	1511.00	1512.00	1513.00		
	*										
	*										
168	KK	ON 6	BASIN								
169	BA	0.218									
170	LG	0.50	0.00	6.16	0.25	0					
171	UC	2.706	1.911								
172	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
173	UA	100									
	*										
174	KK	CB6H	COMBINE								
175	HC	2									
	*										
176	KK	R67	ROUTE								
177	KO										
178	RS	16	FLOW								
179	RC	0.050	0.035	0.050	1500	0.0010	0.00				

180 RX 0.00 3.00 1261.00 1267.00 1273.00 1278.00 1311.00 1410.00  
 181 RY 1511.0 1510.00 1510.00 1508.00 1508.00 1510.00 1510.00 1511.00

\*  
\*

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

182 KK ON 7 BASIN  
 183 BA 0.193  
 184 LG 0.50 0.01 5.71 0.31 0  
 185 UC 3.014 2.840  
 186 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0  
 187 UA 100  
 \*

188 KK CB67 COMBINE  
 189 HC 2  
 \*

190 KK R78 ROUTE  
 191 KO  
 192 RS 11 FLOW  
 193 RC 0.050 0.035 0.050 1350 0.0015 0.00  
 194 RX 0.00 2.00 230.00 1296.00 1305.00 1307.00 1310.00 1315.00  
 195 RY 1510.0 1509.00 1508.00 1509.00 1507.00 1507.00 1509.00 1510.00  
 \*

196 KK MR BASIN  
 197 KM MAGIC RANCH HYDROGRAPH FROM HEC-HMS DRAINAGE REPORT OUTPUT  
 198 BA 1.369  
 199 QI 0 0 0 0 0 0 0 0 0 0  
 200 QI 0 0 0 0 0 0 0 0 0 0  
 201 QI 0 0 0 0 0 0 0 0 0 0  
 202 QI 0 0 0 0 0 0 0 0 0 0  
 203 QI 0 0 0 0 0 0 0 0 0 0  
 204 QI 0 20 22 24 27 30 33 34 35 36  
 205 QI 36 36 36 36 36 36 36 36 36 36  
 206 QI 36 36 36 36 36 36 36 36 36 36  
 207 QI 36 36 36 36 36 36 36 36 36 36  
 208 QI 36 36 36 36 36 36 36 36 36 36  
 209 QI 36 36 36 36 36 36 36 36 36 36  
 210 QI 36 36 36 36 36 36 36 36 36 36  
 211 QI 36 36 36 36 36 36 36 36 36 36  
 212 QI 36 36 36 36 36 36 36 36 36 36  
 213 QI 36 36 36 36 36 36 36 36 36 36  
 214 QI 36 36 36 36 36 36 36 36 36 36  
 215 QI 36 36 36 36 36 36 36 36 36 36  
 216 QI 36 36 36 36 36 36 36 36 36 36  
 217 QI 36 36 36 36 36 36 36 36 36 36  
 218 QI 36 36 36 36 36 36 36 36 36 36  
 219 QI 36 36 36 36 36 36 36 36 36 36  
 220 QI 36 36 36 36 36 36 36 36 36 36  
 221 QI 36 36 36 36 36 36 36 36 36 36  
 222 QI 36 36 36 36 36 36 36 36 36 36  
 223 QI 36 36 36 36 36 36 36 36 36 36  
 224 QI 36 36 36 36 36 36 36 36 36 36  
 225 QI 36 36 36 36 36 36 36 36 36 36  
 226 QI 36 36 36 36 36 36 36 36 36 36  
 227 QI 36 36 36 36 36 36 36 36 36 36  
 228 QI 36 36 36 36 36 36 36 36 36 36  
 229 QI 36 36 36 36 36 36 36 36 36 36

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

230 QI 36 36 36 36 36 36 36 36 36 36  
 231 QI 36 36 36 36 36 36 36 36 36 36  
 232 QI 36 36 36 36 36 36 36 36 36 36  
 233 QI 36 36 36 36 36 36 36 36 36 36  
 234 QI 36 36 36 36 36 36 36 36 36 36  
 235 QI 36 36 36 36 36 36 36 36 36 36  
 236 QI 36 36 36 36 36 36 36 36 36 36  
 237 QI 36 36 36 36 36 36 36 36 36 36  
 238 QI 36 36 36 36 36 36 36 36 36 36  
 239 QI 36 36 36 36 36 36 36 36 36 36  
 \*

240 KK RMR ROUTE  
 241 KO  
 242 RS 71 FLOW  
 243 RC 0.050 0.050 0.050 7240 0.0014 0.00  
 244 RX 0.00 0.00 0.00 6.00 106.00 112.00 112.00 112.00  
 245 RY 1510.0 1510.00 1510.00 1509.00 1509.00 1510.00 1510.00 1510.00  
 \*

246 KK OFF K BASIN  
 247 BA 0.505  
 248 LG 0.30 0.23 6.16 0.17 5  
 249 UC 1.543 1.047  
 250 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0  
 251 UA 100  
 \*

252 KK CB7K COMBINE  
 253 HC 3  
 \*

254 KK OFF L BASIN  
 255 BA 0.052  
 256 LG 0.10 0.25 4.03 0.56 13  
 257 UC 0.283 0.194  
 258 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0



```

*
320 KK DA9RETRIEVE
321 DR DTA9
*

322 KK RA4 ROUTE
323 RS 21 FLOW
324 RC 0.025 0.025 0.050 5193 0.0027 0.00
325 RX 0.00 3.00 10.00 22.00 29.00 36.00 62.00 71.00
326 RY 1522.0 1521.00 1521.00 1520.00 1520.00 1521.00 1521.00 1522.00
*

327 KK OFF N BASIN
328 BA 0.071
329 LG 0.50 0.00 5.05 0.42 0
330 UC 1.362 0.957
331 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
332 UA 100
*

333 KK RN ROUTE
334 RS 15 FLOW
335 RC 0.025 0.025 0.050 3922 0.0025 0.00
336 RX 0.00 3.00 10.00 22.00 29.00 36.00 62.00 71.00
337 RY 1522.0 1521.00 1521.00 1520.00 1520.00 1521.00 1521.00 1522.00
*

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

338 KK CP4N COMBINE
339 HC 2
*

340 KK RA4N ROUTE
341 RS 19 FLOW
342 RC 0.025 0.025 0.050 4912 0.0022 0.00
343 RX 0.00 3.00 10.00 22.00 29.00 36.00 62.00 71.00
344 RY 1522.0 1521.00 1521.00 1520.00 1520.00 1521.00 1521.00 1522.00
*

345 KK ON 4 BASIN
346 BA 0.847
347 LG 0.50 0.00 5.05 0.42 0
348 UC 5.048 4.081
349 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
350 UA 100
*

351 KK CP24 COMBINE
352 HC 3
*

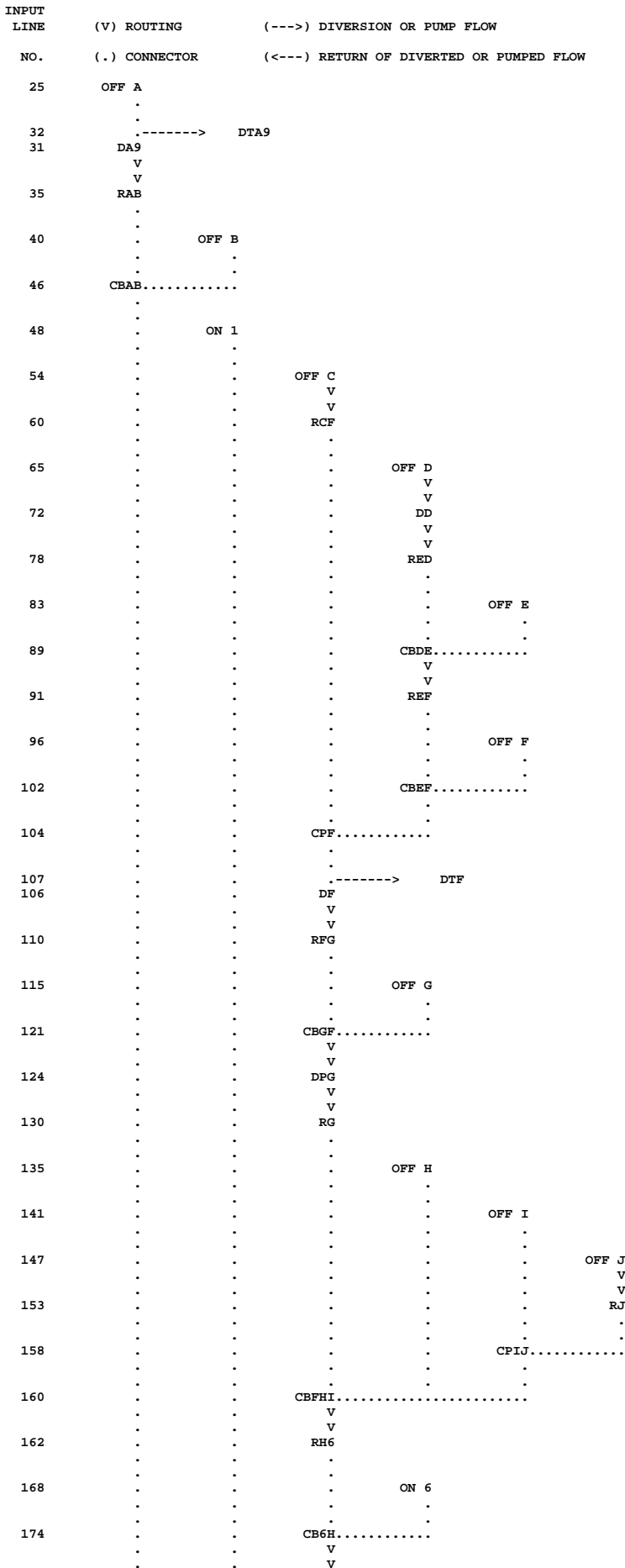
353 KK ON 5 BASIN
354 BA 0.240
355 LG 0.50 0.00 5.05 0.42 3
356 UC 3.407 3.553
357 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
358 UA 100
*

359 KK CB45 COMBINE
360 HC 2
*

361 KK RET4 STORAGE
362 KO
363 RS 1 STOR
364 SA 0.2 0.3 0.4 0.5 0.6 1.1 3.6 25.4
365 SE 1511.0 1512.00 1513.00 1514.00 1515.00 1516.00 1517.00 1518.00
366 SS 1517.0 475.00 2.60 1.50
*
*
367 ZZ

```

SCHEMATIC DIAGRAM OF STREAM NETWORK



```

176      .      .      R67
      .      .      .
182      .      .      ON 7
      .      .      .
188      .      .      CB67.....
      .      .      V
      .      .      V
190      .      .      R78
      .      .      .
196      .      .      MR
      .      .      V
      .      .      V
240      .      .      RMR
      .      .      .
246      .      .      OFF K
      .      .      .
252      .      .      CB7K.....
      .      .      .
254      .      .      OFF L
      .      .      V
      .      .      V
260      .      .      RL8
      .      .      .
265      .      .      ON 8
      .      .      .
271      .      .      CB8L.....
      .      .      .
273      .      .      CP8.....
      .      .      V
      .      .      V
275      .      .      DET8
      .      .      .
282      .      .      .<----- DTF
281      .      .      DF
      .      .      V
      .      .      V
283      .      .      RF
      .      .      .
288      .      .      OFF M
      .      .      .
294      .      .      CPM.....
      .      .      V
      .      .      V
296      .      .      RFM
      .      .      .
301      .      .      ON 3
      .      .      .
307      .      .      CPM3.....
      .      .      V
      .      .      V
309      .      .      D23
      .      .      V
      .      .      V
315      .      .      R24
      .      .      .
321      .      .      .<----- DTA9
320      .      .      DA9
      .      .      V
      .      .      V
322      .      .      RA4
      .      .      .
327      .      .      OFF N
      .      .      V
      .      .      V
333      .      .      RN
      .      .      .
338      .      .      CP4N.....
      .      .      V
      .      .      V
340      .      .      RA4N
      .      .      .
345      .      .      ON 4
      .      .      .
351      .      .      CP24.....
      .      .      .
353      .      .      ON 5
      .      .      .
359      .      .      CB45.....
      .      .      V
      .      .      V
361      .      .      RET4

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION





```
*****
*           *
65 KK      *   OFF D *   BASIN
*           *
*****
```

```
66 KO      OUTPUT CONTROL VARIABLES
           IPRNT      5 PRINT CONTROL
           IPLOT      0 PLOT CONTROL
           QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\* \*\*

```
*****
*           *
72 KK      *   DD *   STORAGE
*           *
*****
```

```
73 KO      OUTPUT CONTROL VARIABLES
           IPRNT      5 PRINT CONTROL
           IPLOT      0 PLOT CONTROL
           QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*           *
121 KK     *   CBGF *   COMBINE
*           *
*****
```

```
122 KO     OUTPUT CONTROL VARIABLES
           IPRNT      5 PRINT CONTROL
           IPLOT      0 PLOT CONTROL
           QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*           *
124 KK     *   DPG *   STORAGE
*           *
*****
```

```
125 KO     OUTPUT CONTROL VARIABLES
           IPRNT      5 PRINT CONTROL
           IPLOT      0 PLOT CONTROL
           QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*           *
162 KK     *   RH6 *   ROUTE
*           *
*****
```

```
163 KO     OUTPUT CONTROL VARIABLES
           IPRNT      5 PRINT CONTROL
           IPLOT      0 PLOT CONTROL
           QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*           *
176 KK     *   R67 *   ROUTE
*           *
*****
```

```
177 KO     OUTPUT CONTROL VARIABLES
           IPRNT      5 PRINT CONTROL
           IPLOT      0 PLOT CONTROL
           QSCAL      0. HYDROGRAPH PLOT SCALE
```

\*\*\* \*\* \*\* \*\*~

```
*****
*           *
190 KK     *   R78 *   ROUTE
*           *
*****
```

```
191 KO     OUTPUT CONTROL VARIABLES
           IPRNT      5 PRINT CONTROL
```

IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

```
*****  
* *  
240 KK * RMR * ROUTE  
* *  
*****
```

241 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\* \*\*

```
*****  
* *  
275 KK * DET8 * STORAGE  
* *  
*****
```

276 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

```
*****  
* *  
309 KK * D23 * STORAGE  
* *  
*****
```

310 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\* \*\* \*\*~

```
*****  
* *  
361 KK * RET4 * STORAGE  
* *  
*****
```

362 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

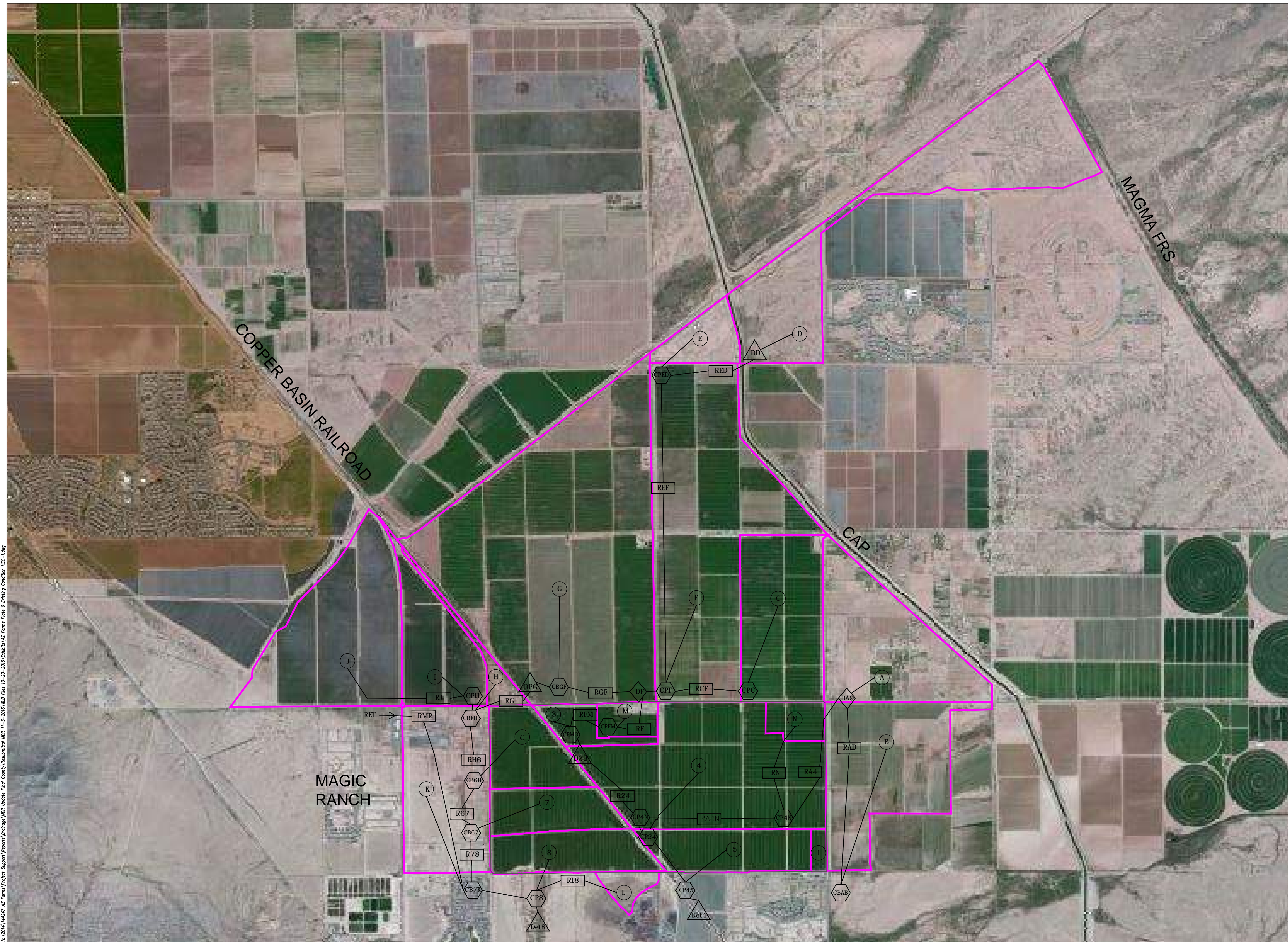
RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+	DIVERSION TO								
	OFF A	187.	14.53	95.	26.	9.	.55		
+	HYDROGRAPH AT								
+	DA9	49.	14.53	20.	5.	2.	.55		
+	HYDROGRAPH AT								
+	DA9	138.	14.53	75.	21.	7.	.55		
+	ROUTED TO								
+	RAB	137.	14.83	75.	21.	7.	.55		
+	HYDROGRAPH AT								
+	OFF B	85.	15.47	56.	16.	6.	.58		
+	2 COMBINED AT								
+	CBAB	213.	15.10	129.	37.	13.	1.14		
+	HYDROGRAPH AT								
+	ON 1	12.	12.80	3.	1.	0.	.02		
+	HYDROGRAPH AT								
+	OFF C	112.	15.10	72.	21.	8.	.48		
+	ROUTED TO								
+	RCF	112.	15.30	72.	21.	8.	.48		
+	HYDROGRAPH AT								
+	OFF D	254.	13.73	114.	31.	11.	.89		
+	ROUTED TO								
+	DD	60.	16.87	53.	24.	9.	.89		
+	ROUTED TO								
+	RED	60.	17.00	53.	24.	9.	.89		
+	HYDROGRAPH AT								
+	OFF E	111.	12.43	14.	4.	1.	.12		
+	2 COMBINED AT								
+	CBDE	109.	12.43	53.	27.	10.	1.01		
+	ROUTED TO								
+	REF	67.	13.63	53.	27.	10.	1.01		
+	HYDROGRAPH AT								
+	OFF F	199.	16.70	152.	45.	16.	1.19		
+	2 COMBINED AT								
+	CBEF	252.	17.00	200.	71.	26.	2.20		
+	2 COMBINED AT								
+	CPF	337.	16.53	263.	92.	33.	2.68		
+	DIVERSION TO								
+	DTF	82.	16.53	54.	14.	5.	2.68		
+	HYDROGRAPH AT								
+	DF	254.	16.53	208.	77.	28.	2.68		
+	ROUTED TO								
+	RFG	254.	16.77	208.	77.	28.	2.68		
+	HYDROGRAPH AT								
+	OFF G	273.	17.43	212.	60.	22.	1.90		
+	2 COMBINED AT								
+	CBGF	518.	17.30	416.	136.	50.	4.57		
+	ROUTED TO								
+	DPG	191.	21.87	181.	127.	50.	4.57		
+	ROUTED TO								
+	RG	191.	22.00	181.	127.	50.	4.57		
+	HYDROGRAPH AT								
+	OFF H	12.	14.63	10.	3.	1.	.06		
+	HYDROGRAPH AT								
+	OFF I	83.	15.20	58.	18.	7.	.31		
+	HYDROGRAPH AT								
+	OFF J	197.	14.70	99.	27.	10.	.68		
+	ROUTED TO								
+	RJ	197.	14.70	99.	27.	10.	.68		
+	2 COMBINED AT								
+	CPIJ	275.	14.80	156.	45.	16.	.99		
+	3 COMBINED AT								
+	CBFHI	316.	14.90	262.	170.	67.	5.63		
+	ROUTED TO								
+	RH6	314.	15.73	260.	170.	67.	5.63		

+	HYDROGRAPH AT	ON 6	70.	14.10	32.	9.	3.	.22
+	2 COMBINED AT	CB6H	350.	15.63	274.	178.	70.	5.85
+	ROUTED TO	R67	348.	16.17	273.	178.	70.	5.85
+	HYDROGRAPH AT	ON 7	41.	14.37	23.	7.	2.	.19
+	2 COMBINED AT	CB67	372.	16.13	285.	183.	72.	6.04
+	ROUTED TO	R78	370.	16.53	284.	183.	72.	6.04
+	HYDROGRAPH AT	MR	36.	14.77	36.	36.	29.	1.37
+	ROUTED TO	RMR	36.	17.17	36.	36.	27.	1.37
+	HYDROGRAPH AT	OFF K	244.	13.13	71.	19.	7.	.50
+	3 COMBINED AT	CB7K	418.	16.50	324.	227.	106.	7.91
+	HYDROGRAPH AT	OFF L	74.	12.17	6.	2.	1.	.05
+	ROUTED TO	RL8	63.	12.30	6.	2.	1.	.05
+	HYDROGRAPH AT	ON 8	63.	13.90	28.	7.	3.	.23
+	2 COMBINED AT	CB8L	67.	12.30	34.	9.	3.	.28
+	2 COMBINED AT	CP8	436.	16.50	331.	235.	109.	8.19
+	ROUTED TO	DET8	423.	16.77	331.	232.	109.	8.19
+	HYDROGRAPH AT	DF	82.	16.53	54.	14.	5.	2.68
+	ROUTED TO	RF	82.	17.13	53.	14.	5.	2.68
+	HYDROGRAPH AT	OFF M	22.	13.33	8.	2.	1.	.07
+	2 COMBINED AT	CPFM	87.	17.07	57.	17.	6.	.07
+	ROUTED TO	RFM	87.	17.33	57.	17.	6.	.07
+	HYDROGRAPH AT	ON 3	28.	13.67	12.	3.	1.	.10
+	2 COMBINED AT	CPM3	91.	17.27	59.	20.	7.	.16
+	ROUTED TO	D23	44.	20.40	35.	13.	5.	.16
+	ROUTED TO	R24	44.	20.80	35.	13.	5.	.16
+	HYDROGRAPH AT	DA9	49.	14.53	20.	5.	2.	.55
+	ROUTED TO	RA4	48.	15.23	20.	5.	2.	.55
+	HYDROGRAPH AT	OFF N	37.	13.00	10.	2.	1.	.07
+	ROUTED TO	RN	36.	13.50	10.	2.	1.	.07
+	2 COMBINED AT	CP4N	57.	15.10	30.	8.	3.	.07
+	ROUTED TO	RA4N	56.	15.73	29.	8.	3.	.07
+	HYDROGRAPH AT	ON 4	114.	15.97	79.	23.	8.	.85
+	3 COMBINED AT	CP24	168.	15.87	115.	43.	16.	1.08
+	HYDROGRAPH AT	ON 5	40.	14.70	26.	8.	3.	.24
+	2 COMBINED AT	CB45	200.	15.80	137.	50.	18.	1.32

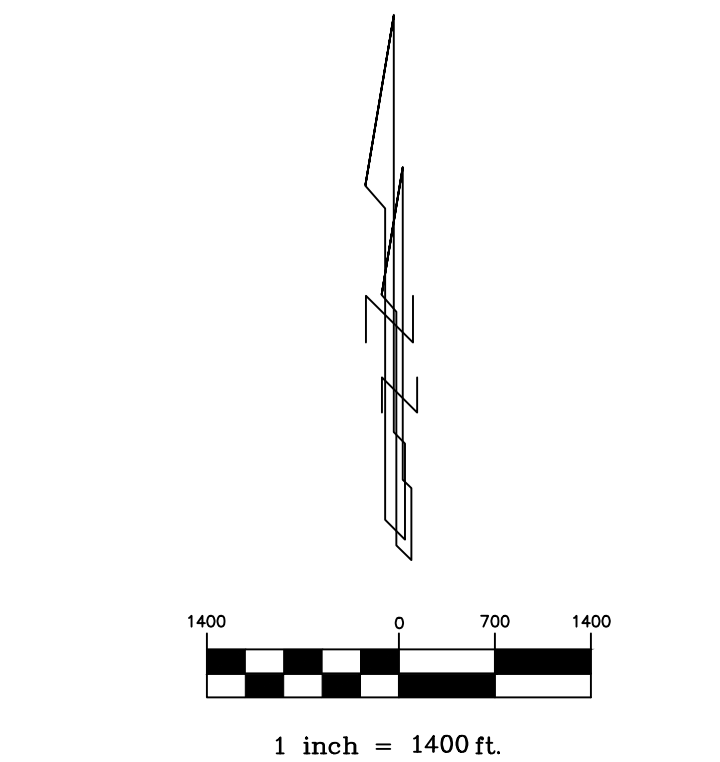
+           ROUTED TO           RET4       199.   15.90           137.       48.       18.       1.32

\*\*\* NORMAL END OF HEC-1 \*\*\*



**LEGEND**

- A HEC-1 SUB BASIN
- RAB HEC-1 ROUTING PATH
- CPG1 HEC-1 COMBINATION POINT
- DPG HEC-1 STORAGE
- DF HEC-1 DIVERSION
- DRAINAGE AREAS



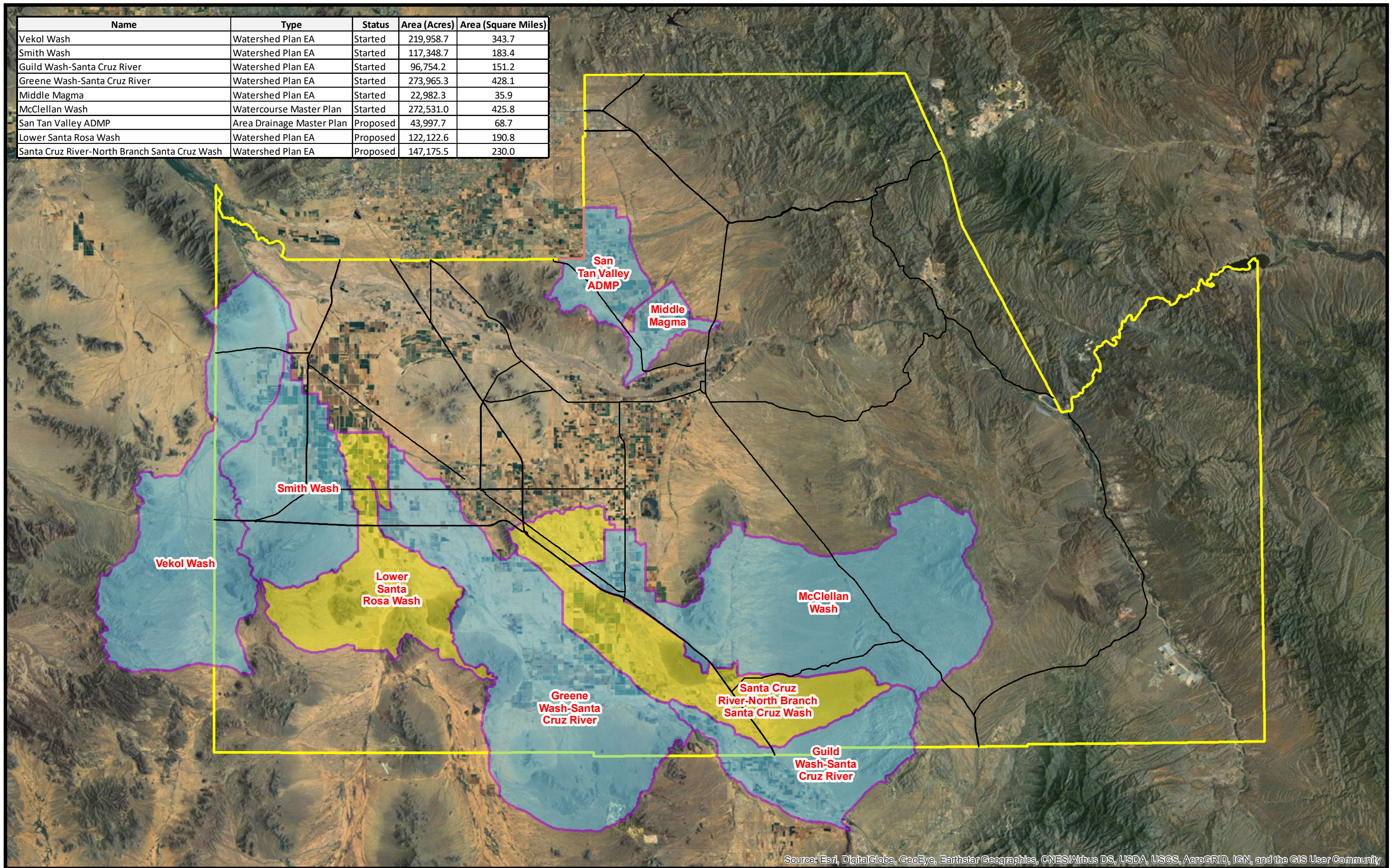
**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA

**PLATE 9 ARIZONA FARMS  
 EXISTING CONDITION  
 HEC-1 SCHEMATIC MAP**

DATE 11/03/2016	SCALE 1" = 1400'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 9

W:\2014\144247 AZ Farms\Project\_Support\Reports\Drainage\Map\_11-3-2016\WB\_Plate\_9\_Existing\_Condition\_HEC-1.dwg  
 11/3/2016 10:20:20 AM

Name	Type	Status	Area (Acres)	Area (Square Miles)
Vekol Wash	Watershed Plan EA	Started	219,958.7	343.7
Smith Wash	Watershed Plan EA	Started	117,348.7	183.4
Guild Wash-Santa Cruz River	Watershed Plan EA	Started	96,754.2	151.2
Greene Wash-Santa Cruz River	Watershed Plan EA	Started	273,965.3	428.1
Middle Magma	Watershed Plan EA	Started	22,982.3	35.9
McClellan Wash	Watercourse Master Plan	Started	272,531.0	425.8
San Tan Valley ADMP	Area Drainage Master Plan	Proposed	43,997.7	68.7
Lower Santa Rosa Wash	Watershed Plan EA	Proposed	122,122.6	190.8
Santa Cruz River-North Branch Santa Cruz Wash	Watershed Plan EA	Proposed	147,175.5	230.0



# **Appendix D**

## **Offsite Drainage Analysis**

**Appendix D.1**  
**Master Drainage Report for Arizona Farms**

**MASTER DRAINAGE REPORT  
FOR  
ARIZONA FARMS**

Revised June 7, 2017  
December 22, 2016  
WP# 144247

DRAINAGE  
CLEARANCE  
1998 DRAINAGE ORDINANCE  
*Scott E. [Signature]* 7/17/2017  
COUNTY ENGINEER DATE

*Prepared for:*

**El Dorado Holdings**  
426 North 44<sup>th</sup> Street  
Suite 100  
Phoenix, Arizona 85008  
Phone: (602) 955-2424  
Contact: Linda Cheney

*Submitted to:*

**Pinal County Flood Control District**  
31 N. Pinal Street  
Building F,  
Florence, Arizona 85132  
Phone: (520) 509-3555  
Fax: (520) 866-6511

*Prepared By:*

**Wood, Patel & Associates, Inc.**  
2051 West Northern Avenue  
Suite 100  
Phoenix, Arizona 85021  
Phone: (602) 335-8500



**WOOD/PATEL**  
MISSION: CLIENT SERVICE®

**TABLE OF CONTENTS**

**1.0 EXECUTIVE SUMMARY & INTRODUCTION ..... 1**

    1.1 Executive Summary ..... 1

    1.2 Introduction..... 2

**2.0 DESCRIPTION OF STUDY AREA ..... 4**

    2.1 Existing Site Conditions ..... 4

    2.2 Watershed Soils ..... 4

    2.3 Rainfall Seasons..... 5

    2.4 Flood Insurance Rate Map (FIRM)..... 5

    2.5 Major Drainage Courses ..... 5

    2.6 Section 404 Jurisdictional Washes..... 6

**3.0 EXISTING DRAINAGE CONDITIONS..... 7**

    3.1 Off-Site Watershed Impacts..... 7

    3.2 Adjacent Properties’ Existing Drainage Studies & Plans ..... 10

    3.3 Existing On-site Drainage..... 12

    3.4 Existing Condition Hydrology..... 14

    3.5 Existing Condition Hydraulics..... 14

**4.0 POST-DEVELOPMENT DRAINAGE CONDITIONS..... 15**

    4.1 Drainage Design Criteria ..... 15

    4.2 Post-Development On-Site Drainage..... 17

    4.3 Post-Development Hydrology ..... 17

    4.4 Erosion and Sediment Control ..... 18

    4.5 Post-Development Hydraulics ..... 18

        4.5.1 Drainage Swale/Channel Hydraulics ..... 18

        4.5.2 Culvert Hydraulics..... 19

        4.5.3 Street Conveyance ..... 19

        4.5.4 Storm Drain Design ..... 20

    4.6 Retention Basin Storage..... 20

    4.7 First Flush Volume ..... 22

    4.8 Post-Development Drainage Along Heritage Road..... 22

    4.9 Development Phasing East & West of the Copper Basin Railroad ..... 23

**5.0 DATA ANALYSIS METHODS..... 25**

    5.1 Hydrologic Procedures, Parameter Selection and Assumptions ..... 25

    5.2 Hydraulic Procedures, Methods, Parameter Selection, and Assumptions ..... 27

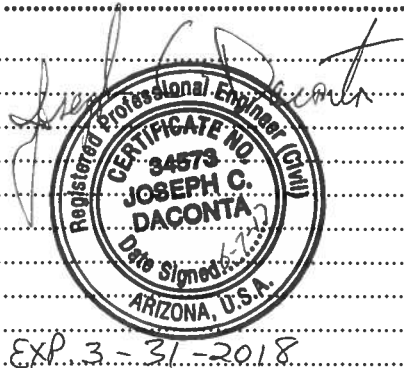
    5.3 Stormwater Storage Calculation Methods and Assumptions..... 27

**6.0 PRE VERSUS POST-DEVELOPMENT PEAK FLOW ANALYSIS ..... 29**

**7.0 OPERATION, MAINTENANCE & LIABILITY ..... 30**

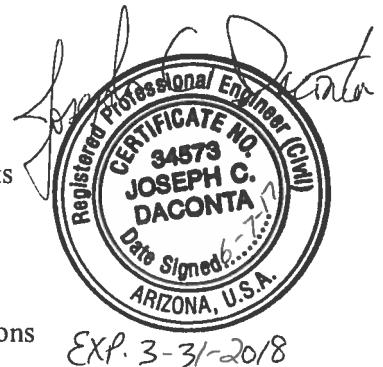
**8.0 CONCLUSIONS ..... 31**

**9.0 REFERENCES..... 33**



## APPENDICES

- APPENDIX A Existing Condition Data and Hydrology
- NOAA Atlas 14 Precipitation Values, Soil, Sub Basin, and Land Use Data
  - Existing Tc and Clark Variables
  - Routing Data
  - Railroad Detention Basin
  - Existing Condition HEC-1 Output
    - 100-year, 25-year, 10-year and 2-year, 6hr and 24hr storm events
- APPENDIX B Post-Development Condition Data and Hydrology
- NOAA Atlas 14 Precipitation Values, Soil, Sub Basin, and Land Use Data
  - Proposed Tc and Clark Variables
  - Routing Data
  - Post-Development Condition HEC-1 Output Historical Locations
    - 100-year, 25-year, 10-year and 2-year, 6hr and 24hr storm events
  - Post-Development Condition HEC-1 Output with Promontory Downstream
    - 100-year, 25-year, 10-year and 2-year, 6hr and 24hr storm events
  - Pre- versus Post-Development Flow Summary
  - Post-Development Required Retention Volume & Drywell Calculations
- APPENDIX C Hydraulics
- Railroad Embankment Analysis
  - Split Flow Calculations
  - Post-Development Condition Channel Hydraulic Outputs
  - Culvert Hydraulic Calculations
  - Retention Basin Drywell Calculations for RET4
  - Quail Run Lane Existing Condition Hydraulic Calculations
- APPENDIX D Supporting Documentation
- Letter from the Magma Flood Control District dated March 4, 2014
  - Salt-Gila Aqueduct Reach 3 Protective Works Sheets 1 through 5 of 5
  - Letter from U.S. Corps of Engineers dated January 28, 2008
  - Promontory at Magic Ranch Grading & Drainage Plan Sheet 4 of 19
  - NRCS Soil Survey



APPENDIX E

Electronic Digital Files

- DDMSW Existing & Post-Development ZIP files
- Existing & Post-Development HEC-1 Files for both the 6 hour and 24 hour durations
- FlowMaster & CulvertMaster Files
- PDF of Drainage Report

PLATES

PLATE 1	Vicinity Map
PLATE 2	Aerial Map
PLATE 3	FEMA Flood Insurance Rate Map
PLATE 4	Existing Condition Soils Map
PLATE 5	Post-Development Soils Map
PLATE 6	CAP Salt-Gila Aqueduct Map
PLATE 7	Existing Condition Land Use Map
PLATE 8	Post-Development Condition Land Use Map
PLATE 9	Existing Condition HEC-1 Schematic Map
PLATE 10A	Post-Development Condition HEC-1 Schematic Map
PLATE 10B	Post-Development Condition HEC-1 Schematic Map with Promontory Downstream
PLATE 11	Existing Condition Hydraulic Map
PLATE 12A	Post-Development Condition Hydraulic Map
PLATE 12B	Post-Development Condition Hydraulic Map with Promontory Downstream
PLATE 13A	Development Phasing Map
PLATE 13B	Development Phasing Map with Promontory Downstream

<sup>zg</sup>  
Y:\WP\Reports\Residential\144247 AZ Farms Master Drainage Report.docx



## 1.0 EXECUTIVE SUMMARY & INTRODUCTION

### 1.1 Executive Summary

This Master Drainage Report is being revised due to the following:

1. Update to the Arizona Farms' land use plan west of Copper Basin Railroad;
2. Inclusion of Quail Run Lane along the west boundary of the Site.
3. The inclusion of a Post-Development 100-year, 25-year, 10-year, 2-year, 24hr & 6hr hydrology analysis that considers the Site's outflow condition for the west portion of Arizona Farms to be located at the historical Heritage Road outfall location, approximately ¼ mile east of the intersection of Quail Run Lane and Heritage Road.

The following are the revisions to this report:

#### Appendix B - Post-Development Condition Data & Hydrology:

- Proposed Tc & Clark Variables - Updated
- Routing Data - Updated
- Post-Development Condition HEC-1 Output 100-yr, 25-yr, 10-yr & 2-yr, 6hr and 24hr storm events with the historical outflow location along Heritage Road (without Promontory) - New
- Post-Development Condition HEC-1 Output 100-yr, 25-yr, 10-yr & 2-yr, 6hr and 24hr storm events with Promontory downstream of Heritage Road - Updated
- Pre vs Post-Development Flow Summary -Updated
- Post-Development Required Retention Volume & Drywell Calculations - Updated

#### Appendix C – Hydraulics:

- Post-Development Condition Channel Hydraulic Outputs -Updated
- Culvert Hydraulic Calculations - Updated

#### Appendix D – Supporting Documentation

- Promontory at Magic Ranch Grading & Drainage Plan Sheet 4 of 19 - New

#### Appendix E – Electronic Digital Files:

- DDMSW 2-Post-Development ZIP files for with/without Promontory – New
- 2-Post-Development HEC-1 files for with/without Promontory – New
- FlowMaster & CulvertMaster Files – Updated
- PDF of Drainage Report – Revised

Plates:

- Plate 5 – Post-Development Soils Map - Updated
- Plate 8 – Post-Development Condition Land Use Map - Updated
- Plate 10A – Post-Development Condition HEC-1 Schematic Map - with the outfall at the historical location along Heritage Road - New
- Plate 10B – Post-Development Condition HEC-1 Schematic Map - with Promontory at Magic Ranch downstream of Heritage Road - Updated
- Plate 12A – Post-Development Condition Hydraulic Map - with the outfall at the historical location along Heritage Road - New
- Plate 12B – Post-Development Condition Hydraulic Map - with Promontory at Magic Ranch downstream of Heritage Road - Updated
- Plate 13A – Development Phasing Map - Updated
- Plate 13B – Development Phasing Map with Promontory Downstream - New

## 1.2 Introduction

Arizona Farms is a proposed mixed use (residential, commercial, and open space) development located in Pinal County, Arizona. The Arizona Farms development (herein referred to as the “Site”) consists of approximately 1153 acres and is located north of Heritage Road, south of Arizona Farms Road, west of Felix Road, and east of the Quail Run Lane alignment. The property is located within Section 1, Township 4 South, Range 8 East, and Section 6, Township 4 South, Range 9 East, of the Gila and Salt River Meridian (refer to Plate 1 – *Vicinity Map*).

This Master Drainage Report addresses both the pre- and post-development Site conditions and provides a conceptual master drainage plan for the proposed development. The report describes the off-site and on-site drainage, and establishes preliminary minimum parameters for the design of drainage improvements. As such, this report presents the results of the conceptual drainage design for the post-development. The purpose of the proposed drainage facilities within the Site is to provide a minimum 100-year flood protection for the project infrastructure and the phasing of the parcels that satisfies the drainage standards and regulations of Pinal County, while ensuring that the downstream and upstream drainage conditions are not adversely impacted and/or altered by the development of this project. The results of the study will be used as a guideline for final design of the project infrastructure and phased parcel improvements. To the best of

our knowledge, the report has been prepared in accordance with Wood, Patel & Associates, Inc.'s (Wood/Patel's) understanding of Pinal County's drainage design standards and regulation requirements.

The Site is planned to include both residential and commercial parcels, open space, and potentially an elementary school. This report addresses both the off-site and on-site hydrology and hydraulics entering and leaving the Site. In addition, it considers an on-site drainage condition for storm water retention of the 100-year, 2-hour runoff volume and a pre- vs. post-peak flow analysis of the 100-year, 25-year, 10-year and 2-year storm frequencies and the 6-hour and 24-hour rainfall duration events. The results substantiate the post-development peak flows leaving the Site do not exceed pre-developed peak flows and that the downstream properties experience similar or reduced flows for each storm event.

## 2.0 DESCRIPTION OF STUDY AREA

### 2.1 Existing Site Conditions

The Site lies within the Pinal County Area Drainage Master Plan (ADMP) Gila River North Watershed. The majority of the Site drains from the northeast to the southwest at an approximate 0.35 percent slope. Elevations range from 1,540 in the northeast, to 1,510 feet in the southwest. In the late 1930's these two sections of land were graded for agricultural production and the land use presently is agricultural. The agricultural fields within these two sections are typically graded into 1/16<sup>th</sup> or 1/8<sup>th</sup> sections and are bordered by irrigation delivery or tailwater ditches. Wash remnants from historic on-site natural drainage channels are not recognizable since the Site has been regraded for agriculture. To the west and south the Site is fronted by abandoned agricultural fields and undeveloped desert, respectively. There is an existing subdivision to the southeast called Crestfield Manor. The remainder of the Site is bound to the north and east by agricultural fields. The Copper Basin Railroad (formerly Southern Pacific Railroad) bisects the property diagonally and acts as a drainage divide; with approximately 389 acres west and 763 acres east of the railroad.

### 2.2 Watershed Soils

Based on the NRCS Eastern Maricopa, Northern Pinal, Eastern Pinal and Southern Gila, and Pinal Western Part Counties Area Arizona Soils Survey (included within Appendix D – *Supporting Documentation*), the off-site watersheds and Site are primarily made up of a two (2) soil types. The first is classified as a clay loam soil (Soils Co and 9) and is hydrologic Soil Group C. The Contine series consists of very deep well drained soils formed in alluvium from mixed sources. Contine soils are on fan terraces and basin floors, hydrologic Soil Group C is classified as soils having very slow infiltration rates when thoroughly wetted (refer to Plate 4 – *Existing Condition Soils Map* and Plate 5 – *Post-Development Soils Map*). The second soil type is classified as a loam soil (Soils My, 24, 28, 31) and is also a hydrologic soil group C, except soil 31 which is a hydrologic Soil Group B. Hydrologic Soil Group B is classified as soils having moderate infiltration rates when thoroughly wetted and consisting chiefly of moderately deep to deep, moderately well to well-drained soils with moderately fine to moderately coarse textures.

### 2.3 Rainfall Seasons

In general, there are two (2) separate rainfall seasons. The first occurs during the winter months from November to March when the area is subjected to occasional storms from the Pacific Ocean. While this is classified as a rainfall season, there can be periods of a month or more in this or any other season when practically no precipitation occurs. The second rainfall season occurs during July and August when Arizona is subjected to widespread thunderstorm activity where moisture supply originates both in the Gulf of Mexico and along Mexico's west coast. These thunderstorms are extremely variable in intensity and location.

### 2.4 Flood Insurance Rate Map (FIRM)

The FEMA Flood Insurance Rate Maps (FIRM) for Pinal County, Arizona and Incorporated Areas, Map Number 04021C0875E, dated December 4, 2007, indicates the Site is within Zone "X".

Zone "X" is defined by FEMA as follows:

*"Areas determined to be outside the 0.2% annual chance floodplain."*

The location of the Site relative to the FIRM panel is illustrated on Plate 3 – *FEMA Flood Insurance Rate Map*.

### 2.5 Major Drainage Courses

There are no major washes with an anticipated 100-year peak flow equal to or greater than 500 cfs that traverses, or originates from, the Site. Significant water courses that traverse through the Site have been identified as washes with a 100-year flow greater than 200 cfs. Only one significant wash has been identified that enters the northwest corner of the property from two (2) 10-foot by 5-foot concrete box culverts and travels along the western property boundary (Quail Run Lane alignment) until it turns east along the Heritage Road alignment before exiting south approximately ¼ mile from the southwest corner of the property. The 100-year floodplain for this significant wash has been delineated for the existing and post-development condition. In the existing condition, one other significant wash exists downstream of the Site when the 100-year peak flow leaves along Heritage Road, immediately east of Copper Basin Railroad. At this location, flows combine from the north and east and leave the Site with a peak discharge that exceeds 200 cfs. The Site is all agricultural fields that have been graded west, south, and

southwest and has north-south and east-west field roads with access to irrigation delivery ditches.

**2.6 Section 404 Jurisdictional Washes**

Based on the letter received from the U.S Army Corps of Engineers, there are no washes subject to jurisdiction of Section 404 requirements on-site. This letter can be found in Appendix D – *Supporting Documentation*.

### 3.0 EXISTING DRAINAGE CONDITIONS

#### 3.1 Off-Site Watershed Impacts

It was determined that there are five (5) locations that off-site drainage enters the Site. Off-site runoff entering the Site originates from the northeast. As can be seen on Plate 9 – *Existing Condition HEC-1 Schematic Map*, in the upper watersheds, east of the Magma Flood Retarding Structure (FRS), off-site watersheds generally have steep to moderately-steep topography with well-defined natural washes. The Magma Flood Retarding Structure (FRS), which was constructed in the early 1960’s, effectively eliminated approximately 78 square miles of contributing watershed from impacting the Arizona Farms property. However, because the Dam was originally built as a Class B Agricultural Dam, significant improvements were necessary to bring the Dam in compliance with the design safety requirements associated with protecting increased populations and improvements. Throughout the subsequent 50 years, funds have been acquired from various sources and repairs to the Dam that would bring it up to code were supposed to be completed in 2015 (see Appendix D – *Supporting Documentation for the Letter from the Magma Flood Control District dated March 4, 2014*). After review of the Magma Flood Control District (AZMFCD) board meeting minutes and further discussion with Mr. Kent Pace, General Manager of the AZMFCD, the Dam repairs were completed in March of 2016. The AZMFCD has completed the necessary documentation and submitted to the Arizona Department of Water Resources (ADWR) where it is anticipated that the Magma Dam FRS “unsafe” classification will be changed to “safe”.

There was a period of time that downstream of the Magma FRS, the watershed had moderately steep slopes with fairly well defined washes. In the early- to mid-1980’s the Central Arizona Project Aqueduct (CAP) was constructed west of the Magma FRS and effectively redirected off-site flows from the contributing upstream watersheds between the FRS and the CAP. Construction of the CAP periodically provided aqueduct overchutes to pass upstream flows. As can be seen from Plate 6 – *CAP Salt-Gila Aqueduct Map*, the only overchute (2-42” CMPs) that impacts the Arizona Farms property is located just north of Judd Road.

As detailed within the *Middle Magma Channel Hydrologic & Hydraulic Analyses Technical Report* (2014) prepared by JE Fuller Hydrology & Geomorphology, Inc.,

although the CAP canal was not designed to be a flood control structure, other than the overchute north of Judd Road, the CAP blocks all flow east of the canal from impacting the Site with no locations upstream of the Site with peak flows overtopping the CAP canal. The likelihood of the CAP canal failure is assumed to be negligible.

As detailed within Appendix D – *Supporting Documentation*, the 100-year outflow was determined by the *Salt-Gila Aqueduct Reach 3 Protective Works* to be 60 cfs. The outflow was routed through the Arizona Public Service site and westward along Judd Road to Attaway Road. A split flow occurs at the intersection of Attaway Road and Arizona Farms Road where flow crosses over Arizona Farms Road and enters onto the land south of the roadway. Currently there are two (2) sets of culverts that exist at this intersection; 2-30” CMPs that run south along the west side of Attaway Road and 3-30” CMPs along the north side of Arizona Farms Road that cross west under Attaway Road. A preliminary split flow evaluation was performed at the intersection to determine how much flow continues to the west on the north side of Arizona Farms Road and how much crosses over the roadway and impacts the property located south of Arizona Farms Road and west of the Attaway Road alignment (see Appendix C – *Hydraulics* for the split flow results). It was determined that approximately 82 cfs during the 100-year, 6-hour event crosses onto the land south of Arizona Farms Road. The split flow then enters the off-site property agricultural fields (DA Off-M), combines with the off-site property flow of 25 cfs and continues to the south where a combined flow of 95 cfs enters the Site (which is greater than the 24-hour duration flow).

The second location where flow enters the Site is located immediately downstream of the Felix Road and Arizona Farms Road intersection. Currently there are four (4) 42-inch CMPs that pass the peak 100-year, 6-hour flow under Arizona Farms Road. However, approximately 100-feet downstream there are three (3) 24-inch concrete pipe culverts that can only pass approximately 42 cfs, while the rest weirs over the top of a dirt irrigation access road. A preliminary split flow analysis was performed at this location and it was determined that approximately 55 cfs of the peak Q100 of 208 cfs will weir across Felix Road and enter the roadway swale that currently exists along the west side of Felix Road for approximately ½ mile before it enters the Site. The remainder of the flow will continue south along the roadway swale located along the east side of Felix Road, with approximately 35 cfs entering the irrigation fields east of Felix Road (see Appendix C –

*Hydraulics* for the split flow results).

The third location is at the northeast corner of the Site. The drainage area is called Off-N and consists of approximately 45-acres of agricultural fields that drain onto the Site. The 100-year, 6 hour flow was determined to be 47 cfs (which is greater than the 24-hour duration flow).

The fourth location is at the existing two (2) 10-foot by 5-foot concrete box culverts located immediately upstream of the intersection of the Quail Run Lane alignment and Arizona Farms Road. At the northeast corner of the intersection of the Copper Basin Railroad and Arizona Farms Road, the railroad currently acts as a retarding structure with several existing culverts that drain the water under the railroad prior to the discharge collecting at the existing two (2) 10-foot by 5-foot concrete box culverts. Survey information of the existing ponding area east of the railroad within the agriculture fields was obtained to determine the volume of ponding and specific relevant culvert information in order to perform a routing of the flow through the storage basin. As a result of this storage, the peak 100-year, 24-hour flow was reduced from 518 cfs to 191 cfs. This flow then combines with additional off-site drainage areas and the flow passing through the box culverts was determined to be approximately 316 cfs.

The fifth location that flow enters the property is located at the southwest corner of the Site where off-site flow from the abandoned agricultural fields located west of the Quail Run Lane alignment enters an existing drainage channel. Although beyond the scope of this report, there appears to be a split flow that occurs at this location where significant flow may continue to the south; however, for the purpose of this report, the flow was conservatively considered to completely enter the Site and was determined to be approximately 278 cfs for the 100-year, 6-hour storm event.

As can be seen on Plate 11 – *Existing Condition Hydraulic Map*, the results of the field investigations identified the existing locations along Arizona Farms Road and Felix Road where currently culverts exist. Most of the culverts have existing conditions that are partially filled with sediment. It was assumed within the hydrology/hydraulic analyses that these culverts would be maintained by the appropriate ownerships and were assumed to be fully effective for the results presented within this report.

### 3.2 Adjacent Properties' Existing Drainage Studies & Plans

A number of adjacent properties' existing drainage studies and plans were reviewed that analyzed drainage in the general vicinity of the Site. A short description of each report/plans has been provided below. Please refer to Plate 2 – *Aerial Map* for the location of each of the adjacent properties.

1. Crestfield Manor (4/2004) drainage report prepared by Sunrise Engineering is located immediately south along the southeast boundary of the Site. The report indicated that there were no off-site flows from the Site that impact the subdivision. As a result of the on-site topography, there is minimal flow from some of the agricultural fields that does impact Felix Road and ultimately enters the Crestfield Manor. As a result, this flow in the post-development conditions will be routed to the west in order to prevent any adverse impact to the drainage system of Crestfield Manor.
2. *Wild Horse Estates (5/1999)* drainage report prepared by WLB Group is located south of Crestfield Manor. This report was prepared prior to Crestfield Manor and indicated that there are upstream watershed areas from the Site that did impact the Wild Horse Estates subdivision which was contradictory to the Crestfield Manor drainage report. This supports the results that were determined within the on-site watershed delineations and the fact that in the existing condition some drainage does impact Crestfield Manor from the Site.
3. *Felix Farms (3/2005)* drainage report prepared by Sunrise Engineering was to be located east of Felix Road and immediately north of the intersection of Felix Road and Heritage Road. Although this subdivision was not constructed, the drainage report indicated that there were no off-site flows impacting the subdivision. As a result of the topography that was obtained for the Site and the additional field survey information, it was determined that there is at least off-site flow along the east side of Felix Road within a roadside drainage swale that would impact the Felix Farms subdivision. This information was provided to both Pinal County and the Town of Florence in order to inform the agencies of this situation and that future development would be required to adhere to existing historical flow patterns east of Felix Road. The Town of Florence Director of Community Development Department, Mr. Mark Eckhoff, has acknowledged this and stated that the existing plans for Felix Farms are no longer valid.

4. *Magic Ranch (2/2004) & Magic Ranch Unit 2 (9/2005)* prepared by JMI & Associates, Inc. is located approximately a ½ to ¾ of a mile west of the Site along Surrey Lane and south of Arizona Farms Road. These drainage reports determined that there was an existing natural storage basin occurring southwest of the intersection of the Union Pacific Railroad (that runs west of Surrey Lane) and Arizona Farms Road. The results indicated that there was approximately 220 acre-feet of volume that reduced the peak 100-year flow from 858 cfs to 36 cfs as it passes under the railroad through two (2) 24” CMPs. As previously discussed, this flow was determined to continue southeast and ultimately impact the Site along the southwest corner of the property.
5. *Magma Ranch III Unit 1 – Grading & Drainage Plans (5/2006)* prepared by Premier Engineering Company is located west of Felix Road and north of Judd Road (approximately 2 miles north of the Site). These plans indicate that there is no peak flow from Magma Ranch located east of Felix Road that continues to the west and north of Judd Road.
6. *Magma Ranch Master Drainage Report (July 2004)* was prepared by Premier Engineering Company and is located east of Felix Road and north of Judd Road. The results indicate that there was an existing condition HEC-1 100-year, 6 hour peak flow of 1209 cfs and post-development of 1189 cfs. This flow continues to the south remaining east of the CAP and therefore doesn’t impact the Site.
7. *Magma Ranch Phase 1 thru 8* drainage reports were prepared by Premier Engineering Company. All on-site drainage reports address only the on-site requirements for development. The subdivision phases were included within the *Magma Ranch Master Drainage Report* and appear to adhere to the drainage requirements and therefore do not impact the Site.
8. *Central Arizona Project (CAP) Salt-Gila Division – Arizona Salt-Gila Aqueduct Reach 3 Protective Works* prepared by the United States Department of the Interior Bureau of Reclamation. The drainage information details the CAP Salt-Gila Aqueduct overchute locations and flows discharging from the CAP located to the east of the Site. As shown on Plate 6 – *CAP Salt-Gila Aqueduct Map*, at location 500+00

there is a detention basin that exists east of the CAP with a pipe overchute of two (2) 42" RCPs. The upstream drainage area equaled 0.93 square miles and hydrology indicated that a Q100 (in) of 160 cfs entered the basin and a Q100 (out) of 60 cfs exits the basin. The storage volume was 1559.6 = 0 AF, 1561.6 = 12 AF and 1563.5 = 45 AF. This information was incorporated into the off-site hydrology analysis.

9. *Promontory at Magic Ranch Grading & Drainage Plans* prepared by OTAK Incorporated. The approximate 240-acre property is located immediately southwest of the Site. As can be seen on the Sheet 4 of 19, provided within Appendix D – *Supporting Documentation*, the Promontory property has been designed to accept off-site flow at the northwest corner of their development at the intersection of Heritage Road and Quail Run Lane. As such, the Site's post-development condition outflow location along the west side of the property will correspond with the location of the anticipated off-site inflow location of the Promontory at Magic Ranch.
  
10. *Middle Magma Channel Hydrologic & Hydraulic Analyses Technical Report* (June 2014) prepared by JE Fuller addressed the hydrologic and hydraulic conditions of the Middle Magma Channel (MMC) and evaluate potential alternatives to provide contiguous, safe passage of floodwaters from the Magma FRS to the Gila River. The report results indicate that the runoff generated from the watersheds east of the CAP Canal is routed through the CAP Canal at three locations east of the Site and that there are no locations upstream of the Site where overtopping occurs along the canal. The only location downstream of the CAP Canal where the routed flow impacts the Site is from the overchute located north of Judd Road. The technical report hydrologic methodology is consistent with the hydrology drainage analyses within this report. In addition, the report's assessment of the CAP Salt-Gila Division – Arizona Salt-Gila Aqueduct Reach 3 Protective Works outflows impacting Arizona Farms is consistent with the results determined within this report.

### 3.3 Existing On-site Drainage

The Site is entirely agricultural in use. The existing drainage conditions are controlled by delivery and tailwater ditches bounding the fields as well as berms at field edges and crop stage. Common practice is to use lower runoff coefficients in agricultural areas. Depending on how each field has been disked and graded, irrigation will flow east to west or north to south. However in a significant flooding event such as the 100-year, 6

hour storm, flooding will follow the aggregate topography of the Site; from east to west and southwesterly.

As previously mentioned, a manmade drainage divide exists as a result of the Copper Basin Railroad bisecting the Site. The railroad embankment was analyzed to determine the possibility of failure since this is not a flood control structure. As can be seen within Appendix C – *Hydraulics*, existing ground cross sections were analyzed at several locations along the railroad embankment and the results indicate that the 100-year peak flow is always less than two feet deep. As a result it was concluded that the existing condition railroad embankment is considered stable and failure is not expected. In the post-development condition, any drainage conveyance corridors adjacent to the railroad embankment shall be designed below grade and outside of the Railroad right-of-way rather than against the embankment and therefore no post-development condition failure along the railroad embankment is anticipated.

As can be seen on Plate 9 – *Existing Condition HEC-1 Schematic Map*, there are three locations that flow leaves the Site, all of which occur along the Heritage Road alignment at the southern boundary of the property. The first is at the northwest corner of the intersection of Felix Road and Heritage Road where a small portion of the on-site agricultural fields drain onto Heritage Road. This is a roadway sump location that drained south into Crestfield Manor storage basins. The second location is east of the Copper Basin Railroad where it intersects the Heritage Road alignment. There currently is a stormwater ponding condition that occurs on-site due to the basin outlet condition being controlled by an existing irrigation canal located immediately downstream and south of the Heritage Road alignment. It was determined that due to this irrigation canal; there is currently an approximate 760-foot wide weir flow outlet condition. The third location is west of the Copper Basin Railroad, approximately ¼ mile east of the intersection of the Quail Run Lane and Heritage Road alignments. The existing drainage channel that accepts flow from the two (2) 10'x5' box culverts (located at the intersection of Arizona Farms Road and Quail Run Lane) runs south along the Quail Run Lane alignment where it turns east and continues approximately ¼ of a mile until it enters two (2) 30" HDPE pipes and continues to the south, leaving the Site. These pipes are inadequate to pass the 100-year existing condition flow and subsequently water backs up onto the Site and then sheetflows over an approximate 850-foot wide weir to the south.

### **3.4 Existing Condition Hydrology**

Existing condition hydrology has been modeled utilizing *DDMSW Version 4.8.0*, obtained from the Flood Control District of Maricopa County (FCDMC), and the U.S. Army Corps of Engineers' *HEC-1, Flood Hydrograph Package, Version 4.1*, (June 1998) to determine off-site and on-site peak flows prior to the development of the Site for the 100-year, 25-year, 10-year, and 2-year, 6-hour and 24-hour storm events. It was determined that the 100-year, 6-hour storm duration had a higher peak discharge than the 100-year, 24-hour duration for the flow leaving along Heritage Road east of the railroad and the 100-year, 24-hour duration peak flow was greater than the 100-year, 6-hour duration flow for the discharge leaving along Heritage Road west of the railroad. As a result, both storm durations were considered within the report. Refer to Appendix A – *Existing Condition Data & Hydrology* for the DDMSW and HEC-1 output. Off-site watersheds were delineated using USGS quadrangle maps, the Pinal County Area Drainage Master Plan (ADMP) Gila River North Watershed GIS drainage maps, and site visit field investigations. On-site watersheds were delineated using one (1) foot topographic contour mapping obtained from El Dorado Holdings and supplemental Wood Patel survey information.

The results of the existing condition hydrology and the ponding limits of existing storage basins are shown on Plate 9 - *Existing Condition HEC-1 Schematic Map* and detail the calculated 100-year, 6-hour and 24-hour peak flows entering and leaving the Site.

### **3.5 Existing Condition Hydraulics**

Existing condition wash hydraulics have been modeled utilizing normal depth calculations determined by Bentley FlowMaster (Ver. 8i, 2010). This was performed on the one wash located along Quail Run Lane that exceeded a 100-year peak flow of 200 cfs. Eight (8) cross sections were obtained along the wash and the resulting washes' water surface elevations were used to delineate the 100-year floodplain. The washes' hydraulic results have been included within Appendix C – *Hydraulics* and the results of the 100-year floodplain are shown on Plate 11 – *Existing Condition Hydraulics Map*. As can be seen by the results, the existing drainage channel does not have the capacity to contain the 100-year flow and the discharge exceeds the top of banks, spreading out onto the Site's agriculture fields and onto the land west of the wash.

## 4.0 POST-DEVELOPMENT DRAINAGE CONDITIONS

### 4.1 Drainage Design Criteria

The drainage design criteria of the Pinal County Drainage Manual Volume 1 & Volume 2 (2004), Drainage Ordinance (1998) and Floodplain Management Ordinance (2006) was used to design the drainage system for the Site. In conjunction with these standards and regulations, the ADOT *Highway Drainage Design Manual Hydrology* (2014) was used where appropriate.

Key drainage design criteria are presented below:

- Off-site flows shall enter and discharge from the Site such that historical drainage patterns are maintained. Drainage easements shall be provided over drainage ways that convey flows of 200 cfs or more during the 100-year storm event. The drainage easements shall encompass the 100-year floodplain. These easements shall be dedicated upon final platting of the planning units. All off-site flow passing through the Site shall be placed in permanent public drainage easements. All retention basins collecting runoff from public right-of-ways shall also be put in a drainage easement.
- Each parcel shall have at least one all-weather road access with a maximum flow of 8-inches in depth over the culvert or overflow roadway section during the 25-year peak flow with no adverse backwater effect during the 100-year peak flow event.
- Culverts for collector and arterial streets are to be designed to convey at least the 50-year peak discharge with no flow crossing over the roadway.
- Stormwater conveyance within streets are to be designed with the 10-year runoff carried within the curbs and the 100-year runoff carried within the right-of-way provided that flow depths do not exceed 6-inches above the roadway centerline. Flows that cause these limits to be exceeded shall be picked up by storm drain systems and/or diverted to drainage ways specifically designed for this purpose. Street capacity calculations will be done for main roadways for 4-in and 6-in curbs. Drainage flowing along streets may not encroach more than the width of a lane from either side.
- All inlets and outlets for drainage structures shall be protected from erosion.

- Pipes or roadside channels may be provided if the runoff exceeds the street capacity. A storm drain system may be provided if the 10-year and/or 100-year runoff would inundate the adjacent finished floors. Catch basins, scuppers, etc. will be provided to remove water so as not to exceed maximum depth of 8-inches within the street.
- Typical lot grading for the various lot configurations will provide flow lines around the building pad and from the back yard to the street (unless split lot grading is acceptable to Pinal County) with typical slopes noted in the plans. Typical lot grading diagrams will be provided in the individual parcel grading plans.
- Retention basins shall be designed as multi-purpose facilities where possible. Regional and/or local subdivision retention basins shall be designed with 4:1 side slopes and a maximum of 3-feet of ponding during the 100-year, 2-hour storm. All basins shall be designed with 1-foot of freeboard. Drainage easements shall be provided over all parcel retention basins and these easements shall be dedicated upon final platting of the planning units. Storage basins shall have an emergency spillway to safely direct overflow into a recognized watercourse.
- Future stormwater storage basins shall provide for dissipation of the entire 100-year, 2-hour storage volume within 36-hours following the storm event using infiltration and/or drywells.
- Basin inlets and outlets shall be designed to avoid erosion within the basin, head cutting or deposition near the inlet. Trash racks and access barriers shall be provided for culverts 18-inches or larger.
- Off-site flows shall not be routed through on-site stormwater storage basins but shall be routed through the Site and released at the natural point of outfall.
- Finish floor elevations shall be a minimum of 1-foot above the emergency overflow elevation of any adjacent retention/detention basins and/or the highest adjacent 100-year water surface elevation.
- All channels shall be designed to include adequate freeboard and shall have at a minimum 1-foot in subcritical channels and 2-foot in supercritical channels.

Under the circumstance that drainage policies and/or standards are not addressed within this report, the Pinal County drainage design criteria and standards shall be used during the development of the Site.

#### **4.2 Post-Development On-Site Drainage**

The overall drainage concept is to route off-site flows through the Site to historic discharge locations, resembling existing drainage patterns. Since there are no natural washes through the Site, the development plan will make provisions to collect and convey off-site flow to existing conditions discharge locations. Post-development retention basins provide 100-year, 2-hour stormwater storage for the developed portions of the Site. To substantiate that post-development peak flows leaving the Site do not exceed pre-developed peak flows, a post-development HEC-1 model was developed for the 100-year, 25-year, 10-year, and 2-year 6-hour and 24-hour storm events. The model reflects post-development land use, including storage and resulting attenuation for post-development retention basins.

On-site flows may be conveyed through streets, storm drain systems, drainage swales, roadside ditches, and/or channels to proposed retention basins. Retention basins will be sized for the 100-year, 2-hour storm event. On-site runoff from storm events exceeding the 100-year, 2-hour flow will pass through emergency overflow spillways to safely discharge stormwater to a conveyance channel, street, or other positive drainage away from the basin. Retained runoff will be dissipated from the basins by utilizing stormwater storage infiltration, and/or drywells. The developer will provide Pinal County with certified as-built dimensions of the basins, and the actual volume of storage provided during development of the Site.

In all locations, lowest floor elevations shall be set a minimum of 1-foot above the emergency overflow elevation, or the highest adjacent 100-year water surface elevation, whichever is greater.

#### **4.3 Post-Development Hydrology**

A post-development HEC-1 model was generated by utilizing the post-development land use plan (see Plate 8 – *Post-Development Land Use Map*). The proposed online retention basins were included within the HEC-1 model. Resulting peak flows can be found within *Section 6.0 – Pre- vs. Post-Development Peak Flow Analysis*, and on Plate 10 – *Post-*

*Development Condition HEC-1 Schematic Map*. DDMSW and Post-development HEC-1 output calculations are located within Appendix B – *Post-Development Condition Data and Hydrology*.

#### **4.4 Erosion and Sediment Control**

The development will include on-site retention basins which retain the on-site 100-year, 2-hour runoff volume and ultimately reduce peak flows to pre-development levels prior to leaving the Site. The off-site flows are to be conveyed through the designated drainage corridors, which shall be designed to mimic the existing conditions sediment transport equilibrium slope and therefore sediment aggradation/degradation is not anticipated to be an issue. Scour protection will be provided both at the upstream and downstream ends of culverts and within drainage swales/channels as necessary.

#### **4.5 Post-Development Hydraulics**

##### **4.5.1 Drainage Swale/Channel Hydraulics**

Preliminary grading conditions similar to existing ground slopes were used to route off-site flows entering the Site, and on-site post-development flows to the appropriate historical outfall locations. Post-development drainage swales and channels have been modeled utilizing normal depth calculations determined by Bentley FlowMaster (V8i, 2010). The primary channel locations include Felix Road from the mid-section line south to Heritage Road then west to the Copper Basin Railroad; Heritage Road from Quail Run Lane to approximately a ½ mile east of Quail Run Lane; and Quail Run Lane from Arizona Farms Road to Heritage Road. Hydraulic output is located in Appendix C – *Hydraulics* and the 100-year floodplain limits are anticipated to be contained within the drainage swale/channel corridors (refer to Plate 12 – *Post-Development Condition Hydraulic Map* for drainage swale/channel locations).

Per the Pinal County drainage design requirements any post-development channels that have a 100-year flow of 200cfs or greater (i.e. the future Quail Run Lane channel) shall be designed using a standard step backwater hydraulic model. As development progresses, subsequent Phase 1 and/or Parcel 1 drainage reports will be required to address the drainage

design of any channel conveying a 100-year flow of 200cfs or greater using a standard step backwater hydraulic model.

#### **4.5.2 Culvert Hydraulics**

Culvert sizes to convey flows through the Site were estimated using a culvert hydraulic computer program. The preliminary culverts proposed for the Site's 100-year stormwater management system can be seen on Plate 12 – *Post-Development Hydraulic Map*. The procedures used follow the Federal Highway Administration, Hydraulic Design Series Number 5 Hydraulic Design of Highway Culverts (USDOT, FHWA, HDS-5, 1985). The culverts' headwater elevations were calculated for inlet and outlet control and the higher of the two was designated as the controlling headwater elevation. The culverts' headwater elevation was determined using Bentley's CulvertMaster (Version 3.3) which computes the headwater using the HDS-5 methodology. The corresponding calculations are located within Appendix C - *Hydraulics*.

For arterial/major collector and/or minor collector/local roadways, a combination of a cross road culvert and a drainage dip section may be designed to convey a portion of the larger, less frequent 100-year peak storm flow over the roadway. Under no circumstance shall the over-topping roadway flow exceed a 0.8 feet maximum depth during the 100-year storm event.

Culverts may be corrugated metal pipes (CMP) with a Manning's "n" value of 0.024, cast-in-place pipe (CIPP), or reinforced concrete pipes (RCP) with a Manning's "n" value of 0.013. For significant flows, considerations may be made for reinforced concrete box culverts (per ADOT standards).

#### **4.5.3 Street Conveyance**

Stormwater conveyance within streets are to be designed with the 10-year runoff carried within the curbs and the 100-year runoff carried within the right-of-way provided that flow depths do not exceed 6-inches above the roadway centerline. Flows that cause these limits to be exceeded shall be picked up by storm drain systems and/or diverted to drainage ways specifically designed for this purpose. Street capacity calculations will be done for main roadways for 4-in and 6-in

curbs. Drainage flowing along streets may not encroach more than the width of a lane from either side. A Manning's "n" value of 0.015 will be used for the standard street cross-section. All continuous grade curb openings (scuppers and catch basins) will be designed assuming a 1.25 x Length clogging factor and sump conditions will apply a 2.0 x Length clogging factor.

#### **4.5.4 Storm Drain Design**

Storm drains may be used to enhance the drainage conveyance in critical project locations. More specifically, the storm drains will supplement the drainage conveyance where street conveyance is found inadequate to handle the runoff within the street cross-section.

Storm drains will either be CMP or reinforced concrete pipes (RCP) with a Manning's "n" value of 0.024 or 0.013, respectively. Storm drain systems will be sized to maintain the hydraulic grade line (HGL) at least 6-inches below the gutter line in a 10-year flood. The 100-year HGL cannot be higher than 12-inches lower than the adjacent homes' finished floor elevations. In addition, the 100-year HGL cannot be higher than the elevation of the ground at the edge of the right-of-way or drainage easement.

For hydraulic storm drain design, StormCAD software by Haestad Methods and/or Hydraflow Storm Sewer for AutoCAD Civil 3D may be used to model the proposed storm drain systems. The software utilizes the hydraulic design guidelines and parameters from the Urban Drainage Design Manual, Hydraulic Engineering Circular No. 22 by Federal Highway Administration, November 1996 (3rd Edition Revised 2013).

#### **4.6 Retention Basin Storage**

Pinal County requires that runoff from the 100-year, 2-hour storm event be retained on-site. Basins should be designed with the proposed landscaping scheme in mind. Per the County regulations, all basins will be designed with ponding depths of three (3) feet or less during the 100-year, 2-hour storm with varying side slopes not exceeding the required 4:1 (H:V) slope. Underground stormwater storage may be used in commercial

properties only and shall adhere to the County's regulations and standards if implemented within future commercial development.

As the development of individual parcels occur within the Site, interim retention/detention basins may be utilized to store and/or attenuate the 100-year peak storm runoff from undeveloped areas surrounding the developed parcel(s). Regional retention basins may be considered as an option for this Site to obtain effective peak flow attenuation and multiple land use benefits for the drainage system. Temporary drainage easements shall be required if temporary stormwater storage basins are used outside of the area being platted at the time of parcel development. The easement must be recorded prior to plat approval but may be abandoned with the platting of the future phased parcels.

Within the Site, the 100-year, 2-hour required retention volumes were determined for each on-site post-development parcel drainage area. In order to simulate an on-line retention basin, a diversion card was used in the HEC-1 and the 100-year, 2-hour required retention volume was removed from the inflow hydrograph. The remaining hydrograph runoff was then routed downstream.

As the Site development occurs, on-site storm water will be routed through basins and storage routing will be performed using an updated HEC-1 model. The surface area of a proposed retention basin will be measured at representative elevations within the basin boundary. This information will be directly entered into the HEC-1 model on the SE and SA records. As an alternate, this information can be converted to a volume and entered into the model using the SE and SV records. The data will be utilized by the HEC-1 model for reservoir routing of a specified inflow hydrograph.

All storage basins used for retention to meet the 100-year, 2-hour stormwater storage requirements shall use infiltration, and/or drywells to drain the basins within 36 hours.

Basin locations, layout, and sizes, along with details for inlet and outlet structures will be determined as development occurs within the Site.

Basins shall be designed with emergency overflows. Required retention volumes were calculated using the following equation:

$$V=C*(P/12)*A$$

Where:

*C = Runoff Coefficient*

*P = Precipitation Depth in inches*

*A = Drainage Area in acres*

The final grading and post-development weighted runoff coefficient and drainage area parameters will be determined during parcel development of the Site. The 100-year, 2-hour precipitation depth for use in Pinal County was obtained from NOAA Atlas 14 isopleth precipitation maps. Refer to Appendix B - *Post-Development Condition Data and Hydrology* for detailed retention required calculations.

#### **4.7 First Flush Volume**

AZPDES has established a minimum level of control for new development at which stormwater pollution prevention practices must be put in place. This minimum standard is “First Flush” and consists of retaining or treating the first 0.5 inches of direct runoff from a storm event. Normally this minimum level of control is met by following the Pinal County retention requirements. The required first flush retention volumes are determined using the Rational Method. The Rational Method determines the required storage volume (V) using a point rainfall depth (P), a runoff coefficient (C), and the sub-basin area (A). These parameters are used in the following equation to determine the required volume:

$$V = C \frac{P}{12} A$$

In the first flush event, a C value of 1, is used, with a rainfall depth of 0.50-inches, this generates the required one half (½) inch of runoff.

#### **4.8 Post-Development Drainage Along Heritage Road**

As a result of modeling the post-development on-site drainage system’s retention basins, the peak 100-year flows that exit the Site at the three locations along Heritage Road have been reduced below existing condition peak flows. The three locations are: Heritage Road east of the Copper Basin Railroad (HEC-1 RET4), the post-development 100-year,

6-hour peak flow was determined to be 114 cfs, which has been reduced from the existing condition 100-year peak flow of 232 cfs. The second location at the northwest corner of the intersection of Felix Road has no outflow during any storm event and therefore is in conformance with the Crestfield Manor drainage report.

The third location is west of Copper Basin Railroad and two post-development outflow locations along Heritage Road were analyzed: the first location was the current existing condition outflow located approximately ¼ mile east of the intersection of the Quail Run Lane and Heritage Road alignments. As was previously determine in the existing condition the more frequent storm event flows enter two (2) 30” HDPE pipes and continues to the south, leaving the Site. These pipes are inadequate to pass the 100-year flow and subsequently water backs up onto the Site and then sheetflows over an approximate 850-foot wide weir to the south. In order to re-establish the existing broad weir outflow condition it may be necessary to design an outflow structure that allows for the flow to discharge out of a controlled weir structure so as to mimic the existing drainage outflow conditions. However, this type of outlet condition, although matching the existing condition, does not lend itself to a favorable development condition downstream. As a result, the second outfall location was analyzed which is located at the northeast corner of the intersection of Quail Run Lane and Heritage Road (located at the southwest corner of the Site). As can be seen on Promontory at Magic Ranch Grading and Drainage Plans, Sheet 4 of 19 (received from OTAK on 5/31/2017 and located in Appendix D – Supporting Documentation), accommodations for the 100-year flow within the Quail Run Lane drainage channel has been provided by including a double barrel 12-ft x 4-ft box culvert to pass the discharge underneath Heritage Road. As detailed within the hydrology analyses for these two locations, (HEC-1 CQ2), the post-development 100-year, 24-hour peak flow is 371 cfs down from the existing condition 100-year, 24-hour peak flow of 423 cfs.

#### **4.9 Development Phasing East & West of the Copper Basin Railroad**

Although the exact timing and phasing of the development and the major infrastructure is unknown at this time, the following are recommendations for logical phasing based on either the land east of the railroad or west of the railroad being developed together. As can be seen on Plate 13A – *Development Phasing Map* and Plate 13B – *Development Phasing Map with Promontory Downstream*, when east of the railroad is developed the

property may be developed in three (3) phases. Since the existing agricultural fields drains east to west, Phase 1 could start along the northeast parcels and adjacent to Felix Road and continue south including Parcels X, Y, Z, CC and EE. As a result, this would include the channel drainage infrastructure along Felix Road and Heritage Road. Phase 2 would include the central part of the eastern property and therefore would include a channel along the east side of the Attaway roadway and include Parcels N through W, AA, BB and DD. Phase 3 would be the remainder of the parcels adjacent to the railroad: Parcels A, B and F through M. Phase 3 would also include the channel and retention basin east of and adjacent to the railroad.

West of the railroad can also be developed logically in three phases. Considering that the existing agricultural fields also drain east to west, the first phase may be along Arizona Farms Road and include Parcels A through D and Parcel Q and R. The drainage infrastructure would consist of the Quail Run Lane channel to collect flow from Parcels A, R and Q and drainage swales to convey flow from Parcels B through D to the Heritage Road Channel. Without Promontory to the south, a Phase 1 Weir would also be required in order to re-establish the existing drainage flow conditions downstream of Heritage Road. The second phase could include Parcels E, F, G, N, O and P and would use the drainage swales from Phase 1 and the channel along Heritage Road. Phase 3 would include the remainder of the Parcels, Parcel H through M, and the remaining channel along Heritage Road.

As the development progresses, internal drainage infrastructure will be better understood and updates to this recommended phasing approach that addresses the undeveloped land and drainage will have to be considered within the individual parcel development final drainage reports.

## 5.0 DATA ANALYSIS METHODS

### 5.1 Hydrologic Procedures, Parameter Selection and Assumptions

Off-site watersheds were delineated using USGS quadrangle maps, Pinal County Area Drainage Master Plan (ADMP) Gila River North Watershed GIS drainage maps, and site visit field investigations. On-site watersheds were delineated using one foot topographic contour mapping obtained from El Dorado Holdings and supplemental Wood Patel survey information. Post-development land use planning was used for on-site contributing watersheds. The U.S. Army Corps of Engineers' HEC-1 software was used to develop peak flows at concentration points entering and exiting the Site for both the existing and post-development conditions.

- Rainfall was determined using the NOAA Atlas 14 data. The 100-year, 6-hour precipitation depth utilized in the model was 2.74 inches and the 100-year, 24-hour depth used within the model was 3.84 inches. DDMSW was utilized to perform an aerial reduction of the 100-year precipitation depths.
- Infiltration losses were determined using the Green and Ampt method, soil data obtained by the NRCS Web Soil Survey, and the Maricopa County DDMSW software.
- DTHETA and PSIF values were assigned based on the computed bare ground XKSAT values using the look up tables in the DDMSW software for Maricopa County. Most drainage areas or modeling sub-basins were composed of several subareas containing soils of different textures. Therefore, a composite value for the Green and Ampt parameters that are to be applied to the drainage areas for modeling sub-basins needed to be determined. The procedure for determining the composite value is to average the area-weighted logarithms of the XKSAT values and to select the PSIF and DTHETA values from a graph. The XKSAT value (and naturally occurring rock outcrop percentage) for each map unit has been identified by the National Resources Conservation Service (NRCS). The values for XKSAT are weighted based on the percentage of each unique soil texture present in the map unit. The weighted values take into consideration the horizon depth of the soil textures in regard to the expected depth of infiltration during the design storm duration. The bare ground XKSAT values were then adjusted based on average subbasin vegetation cover.

- DDMSW was used to generate sub-basin hydrographs based on the Clark method. Unit hydrographs to convert rainfall excess into runoff hydrographs were computed using the methods outlined in the ADOT Hydrology Manual. The ADOT Manual recommends the use of the Clark Unit hydrograph which requires two inputs – time of concentration (Tc) and a storage coefficient (R).

The ADOT time of concentration equation for desert/mountain areas is:

$$T_c = 2.4 A^{0.1} L^{0.25} L_{ca}^{0.25} S^{-0.2}$$

Where,

A = drainage area in square miles

L = flow path length in miles

Lca = length along flow path to point opposite the basin centroid in miles

S = flow path slope in feet per mile

Tc = time of concentration in hours

The ADOT time of concentration equation for agricultural areas is:

$$T_c = 7.2 A^{0.1} L^{0.25} L_{ca}^{0.25} S^{-0.2}$$

The ADOT storage coefficient equation is a function of Tc, L, and A:

$$R = 0.37 T_c^{1.11} L^{0.8} A^{-0.57}$$

Where,

Tc = time of concentration in hours

L = flow path length in miles

A = drainage area in square miles

R = storage coefficient in hours

Existing condition and post-development condition land uses were input into DDMSW, as well as watershed characteristics such as high elevation, low elevation, and watercourse length to generate the runoff hydrographs.

- The time of concentrations for the 25-year, 10-year and 2-year storm events were calculated based on the ratios determined between these storm events' time of concentrations by Maricopa County.

- The values of the synthetic dimensionless time-area relations for the Clark Unit Hydrograph were obtained from the Maricopa County urban and natural watersheds time-area relations.
- Runoff hydrographs were routed using the Normal Depth Storage Routing Method.

Resulting existing and post-development peak flows exiting the Site is discussed within Section 6.0 - *Pre- vs. Post-Development Peak Flow Analysis*.

## 5.2 Hydraulic Procedures, Methods, Parameter Selection, and Assumptions

Floodplain delineations, culvert sizing, and other detailed hydraulic calculations were performed at a preliminary post-development level within this drainage report. Where applicable (where runoff volume exceeds available basin storage volume), retention basins outlet weirs were tentatively designed to pass the 100-year peak outflow. Stormwater storage basin drywell calculations can be found within Appendix B & Appendix C for RET 4.

## 5.3 Stormwater Storage Calculation Methods and Assumptions

On-site retention basins will be provided for each parcel and may include surface and/or underground storage facilities (for commercial properties only) and use infiltration, and/or dry wells to evacuate the facilities, as deemed necessary. Required stormwater storage calculations were performed using the Rational Method. The equations used to calculate the required and provided retention volumes are presented below.

$$V_{REQUIRED} = C * \left( \frac{P}{12} \right) * A$$

Where:

- V is the required retention volume in acre-feet
- C is the weighted “C” coefficient
- P is the precipitation in inches for the 100-year, 2-hour rainfall, 2.35-inches for the proposed site.
- A is the drainage area in acres

As parcel development occurs, provided retention basin volumes shall be calculated using the Conic Approximation Method as such:

$$V = \frac{a}{3}(A_{Top} + A_{Bot} + \sqrt{A_{Top}A_{Bot}})$$

*Where:*

*a = distance between the areas*

*A<sub>Top</sub> = Area of the top of basin*

*A<sub>Bot</sub> = Area of the bottom of basin*

The ultimate provided retention volume calculations will be based on the disturbed final graded and post-development areas. The ultimate runoff coefficients utilized will be based on the Pinal County Drainage Manual Volume 2 Table 2-1.

Please see Appendix B –*Post-Development Condition Data and Hydrology* for detailed required retention volume calculations.

## 6.0 PRE VERSUS POST-DEVELOPMENT PEAK FLOW ANALYSIS

Refer to the tables within Appendix B for the comparative peak discharge rates for the pre- versus post-development 6-hour and 24-hour storm duration conditions at the concentration points along the project's southern boundary where flow leaves, or may leave (for the Promontory box culvert location), the Site along Heritage Road. During the 100-year, 6-hour and 24-hour storm events, the modeling results indicate post-development flows leaving the Site are below the pre-development peak flows at the three (3) historical outfall locations and for the post-development Promontory at Magic Ranch box culvert outfall location. Additionally, during the 25-year, 10-year and 2-year, 6-hour and 24-hour storm events, the post-development flows leaving the Site were also at or below the pre-development peak flows at all historical outfall locations and at the post-development Promontory at Magic Ranch box culvert outfall location. The results are summarized in the Pre Versus Post-Development Flow Tables located within Appendix B – *Post-Development Condition Data and Hydrology*.

## 7.0 OPERATION, MAINTENANCE & LIABILITY

The proposed drainage system shall be operated and maintained in accordance with Pinal County Design Standards and Policies. Ongoing maintenance of the designed or recommended drainage system is required to preserve the design integrity and purpose of the drainage system. Failure to provide maintenance can prevent the drainage system from performing to its intended design purpose and can result in reduced performance. Maintenance within the public right-of-way is the responsibility of the governing municipality. However, it is the responsibility of land owner for facilities on private property. Prior to ultimate condition build-out upstream of drainage structures, additional maintenance may be required due to an increase in sedimentation build-up. A regular maintenance program is required to have drainage systems perform to the level of protection or services as presented in this report.

A maintenance program shall at a minimum (but not limited to) include scheduled and unscheduled operations such as:

- Inspections of the drainage system improvements shall be performed and documented on an annual basis;
- Unscheduled additional inspections performed during and after major storm events;
- Removal of debris and excessive sediment build-up within channels and/or culverts/storm drain systems;
- Scheduled mowing, debris removal, graffiti removal and/or rock replacements;
- Repair or replacement of damaged erosion protection and/or channel overbanks;
- Maintenance vehicle access ramps to be provided for all channel segments as necessary;
- Sedimentation staff gauges within stormwater storage basins as necessary;
- Installation of additional erosion control measures as needed.

## 8.0 CONCLUSIONS

Based on the results of the study, the following can be concluded:

- The *Master Drainage Report for Arizona Farms* is prepared in accordance with our understanding of Pinal County drainage requirements and standards.
- Ultimately, a detailed drainage system composed of streets, scuppers, catch basins, storm drains, culverts, open channels, and retention basins will be designed for all parcels within the Site.
- Based on the HEC-1 computer modeling, resulting peak flows for the post-development condition 100-year, 25-year, 10-year and 2-year, 6-hour and 24-hour storm flows exiting the Site do not exceed pre-development condition levels, as summarized within this report.
- As development progresses, on-site retention basins will be designed to store the 100-year, 2-hour storm event for disturbed areas.
- Stormwater storage infiltration, and/or drywells shall evacuate retained runoff from basins within the 36-hour requirement.
- Drainage infrastructure has been designed in accordance with the appropriate criteria defined in this report. For situations not covered in this report, the drainage design criteria of the Pinal County Drainage Manual Volume 1 & Volume 2 (2004), Drainage Ordinance (1998) and Floodplain Management Ordinance (2006) and the ADOT *Highway Drainage Design Manual Hydrology* (2014) requirements shall be used for drainage facility design.
- Additional drainage reports substantiating the conformance to the master drainage system design will be required for each individual parcel. These reports are to address both the on-site drainage for the individual parcel as well as how the upstream and downstream drainage is being handled around the parcel.
- All finished floor elevations are to be designed at least 1-foot above the highest adjacent 100-year water surface elevations.
- The Site must provide all-weather access per the Drainage Ordinance requirements.
- The Site's proposed drainage design is in compliance with the Pinal County Drainage Ordinance (2007) and the Pinal County Drainage Manual (2004). As the development proceeds the Site must continue to be in compliance with the Pinal County Drainage Ordinance (2007) and the Pinal County Drainage Manual (2004).

- The Site shall not cause any adverse impacts or increased drainage problems for adjacent properties upstream and/or downstream.
- Ongoing maintenance is required for the drainage systems in order to assure design performance. Maintenance is the responsibility of ownership.

## 9.0 REFERENCES

1. *Drainage Manual Volume 1 & Volume 2*; Pinal County (2004).
2. *Drainage Ordinance*, Pinal County (1998).
3. *Floodplain Management Ordinance*, Pinal County (2006).
4. *Highway Drainage Design Manual Hydrology*, ADOT (2014).
5. *Drainage Design Manual for Maricopa, County, Arizona, 4<sup>th</sup> Edition, Hydrology*, Flood Control District of Maricopa County, August 15, 2013.
6. *Drainage Design Manual for Maricopa, County, Arizona, Hydraulics*, Flood Control District of Maricopa County, August 15, 2013.
7. *National Flood Insurance Program, Flood Insurance Rate Map, Panel Numbers 04021C0875E* Federal Emergency Management Agency (FEMA), dated December 04, 2007.
8. *HEC-1 Flood Hydrograph Package*, US Army Corps of Engineers, June 1998.
9. *Bentley FlowMaster V8i*, Haestad Methods Solution Center, November 2013.
10. *Bentley CulvertMaster V3.3*, Haestad Methods Solution Center, November 2016.
11. *Highway Drainage Design Manual Volume 2 Hydrology* Second Edition, ADOT, 2014.

**Existing Condition 100-year, 6-hour  
HEC-1 Output**

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 07JUN17 TIME 10:41:04
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Flood Control District of Pinal County
2 ID AZ FARMS EX 100YR6HR - Arizona Farms MDR Existing Condition 100YR, 6HR
3 ID 100 YEAR
4 ID 6 Hour Storm
5 ID Unit Hydrograph: Clark
6 ID Storm: Multiple
7 ID FILE NAME: EX100YR6HR.DAT
8 ID BY: WOOD/PATEL JCD
9 ID 11/03/2016
*DIAGRAM
10 IT 2 1JAN99 0 2000
11 IO 5
12 IN 15
*
13 JD 2.74 0.0001
14 PC 0.000 0.008 0.016 0.025 0.033 0.041 0.050 0.058 0.066 0.074
15 PC 0.087 0.099 0.118 0.138 0.216 0.377 0.834 0.911 0.931 0.950
16 PC 0.962 0.972 0.983 0.991 1.000
17 JD 2.72 0.5000
18 PC 0.000 0.008 0.016 0.025 0.033 0.041 0.050 0.058 0.066 0.074
19 PC 0.087 0.099 0.118 0.138 0.216 0.377 0.834 0.911 0.931 0.950
20 PC 0.962 0.972 0.983 0.991 1.000
21 JD 2.67 2.8
22 PC 0.000 0.009 0.016 0.025 0.034 0.042 0.051 0.059 0.067 0.076
23 PC 0.087 0.100 0.120 0.163 0.252 0.451 0.694 0.837 0.900 0.938
24 PC 0.950 0.963 0.975 0.988 1.000
25 JD 2.53 16.0
26 PC 0.000 0.015 0.020 0.030 0.048 0.063 0.076 0.090 0.105 0.119
27 PC 0.135 0.152 0.175 0.222 0.304 0.472 0.670 0.796 0.868 0.912
28 PC 0.946 0.960 0.973 0.987 1.000
*
29 KK OFF A BASIN
30 BA 0.553
31 LG 0.50 0.00 7.58 0.15 0
32 UC 3.302 1.934
33 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
34 UA 100
*
35 KK DA9 DIVERT
36 DT DTA9 0.0 0.0
37 DI 0.0 66.0 206.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
38 DQ 0.0 9.0 55.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
*
39 KK RAB ROUTE
40 RS 7 FLOW
41 RC 0.016 0.025 0.025 5100 0.0025 0.00
42 RX 0.00 0.00 3.00 15.00 30.00 35.00 39.00 54.00
43 RY 1538.0 1538.00 1537.00 1536.00 1536.00 1537.00 1538.00 1539.00
*
*

```

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
44 KK OFF B BASIN
45 BA 0.584
46 LG 0.50 0.00 4.87 0.46 0
47 UC 4.401 3.738
48 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0
49 UA 100
*

```

```

50      KK      CBAB COMBINE
51      HC          2
      *

52      KK      ON 1  BASIN
53      BA      0.023
54      LG      0.50      0.00      5.05      0.42      3
55      UC      1.045      1.146
56      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
57      UA      100
      *

58      KK      OFF C  BASIN
59      BA      0.481
60      LG      0.50      0.00      7.58      0.15      0
61      UC      3.874      3.202
62      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
63      UA      100
      *

64      KK      RCF  ROUTE
65      RS          6      FLOW
66      RC      0.016      0.025      0.025      2290      0.0022      0.00
67      RX      0.00      0.00      11.00      15.00      42.00      54.00      65.00      69.00
68      RY      1536.0      1536.00      1535.00      1534.00      1534.00      1535.00      1535.00      1536.00
      *
      *

69      KK      OFF D  BASIN
70      KO
71      BA      0.887
72      LG      0.35      0.34      7.00      0.10      0
73      UC      2.221      1.995
74      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
75      UA      100
      *

76      KK      DD STORAGE
77      KO
78      RS          1      STOR
79      SV          12.00      45.00
80      SQ          0.00      70.00
81      SE      1559.6      1561.60      1563.60
      *
      *

```

1

HEC-1 INPUT

PAGE 3

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

82      KK      RED  ROUTE
83      RS          4      FLOW
84      RC      0.025      0.025      0.025      2210      0.0027      0.00
85      RX      0.00      0.00      0.00      6.00      10.00      16.00      16.00      16.00
86      RY      1557.0      1557.00      1557.00      1554.00      1554.00      1557.00      1557.00      1557.00
      *
      *

87      KK      OFF E  BASIN
88      BA      0.124
89      LG      0.35      0.36      5.05      0.23      0
90      UC      0.659      0.432
91      UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
92      UA      100
      *

93      KK      CBDE COMBINE
94      *          1          2
      HC          2
      *

95      KK      REF  ROUTE
96      *          40          2
      RS          169      FLOW
97      RC      0.025      0.016      0.025      10410      0.0019      0.00
98      RX      0.00      2.00      35.00      49.00      63.00      80.00      88.00      90.00
99      RY      1542.0      1540.00      1540.00      1540.28      1540.28      1540.00      1540.00      1542.00
      *
      *

100     KK      OFF F  BASIN
101     BA      1.187
102     LG      0.50      0.00      8.36      0.12      0
103     UC      5.749      4.831
104     UA      0          3.0          5.0          8.0          12.0          20.0          43.0          75.0          90.0          96.0
105     UA      100
      *

106     KK      CBEF COMBINE
107     HC          2
      *

108     KK      CPF COMBINE
109     HC          2
      *

110     KK      DF  DIVERT
111     DT      DTF      0.0          0.0
112     DI      0.0      120.0      328.0          0.0          0.0          0.0          0.0          0.0          0.0          0.0
113     DQ      0.0          0.0          79.0          0.0          0.0          0.0          0.0          0.0          0.0          0.0
      *
      *

```

1

HEC-1 INPUT

PAGE 4

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```



180 KK R67 ROUTE  
 181 KO  
 182 RS 16 FLOW  
 183 RC 0.050 0.035 0.050 1500 0.0010 0.00  
 184 RX 0.00 3.00 1261.00 1267.00 1273.00 1278.00 1311.00 1410.00  
 185 RY 1511.0 1510.00 1510.00 1508.00 1508.00 1510.00 1510.00 1511.00  
 \*  
 \*

1

HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

186 KK ON 7 BASIN  
 187 BA 0.193  
 188 LG 0.50 0.01 5.71 0.31 0  
 189 UC 3.014 2.840  
 190 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0  
 191 UA 100  
 \*

192 KK CB67 COMBINE  
 193 HC 2  
 \*

194 KK R78 ROUTE  
 195 KO  
 196 RS 11 FLOW  
 197 RC 0.050 0.035 0.050 1350 0.0015 0.00  
 198 RX 0.00 2.00 230.00 1296.00 1305.00 1307.00 1310.00 1315.00  
 199 RY 1510.0 1509.00 1508.00 1509.00 1507.00 1507.00 1509.00 1510.00  
 \*

200 KK MR BASIN  
 201 KM MAGIC RANCH HYDROGRAPH FROM HEC-HMS DRAINAGE REPORT OUTPUT  
 202 BA 1.369  
 203 QI 0 0 0 0 0 0 0 0 0 0  
 204 QI 0 0 0 0 0 0 0 0 0 0  
 205 QI 0 0 0 0 0 0 0 0 0 0  
 206 QI 0 0 0 0 0 0 0 0 0 0  
 207 QI 0 0 0 0 0 0 0 0 0 0  
 208 QI 0 20 22 24 27 30 33 34 35 36  
 209 QI 36 36 36 36 36 36 36 36 36 36  
 210 QI 36 36 36 36 36 36 36 36 36 36  
 211 QI 36 36 36 36 36 36 36 36 36 36  
 212 QI 36 36 36 36 36 36 36 36 36 36  
 213 QI 36 36 36 36 36 36 36 36 36 36  
 214 QI 36 36 36 36 36 36 36 36 36 36  
 215 QI 36 36 36 36 36 36 36 36 36 36  
 216 QI 36 36 36 36 36 36 36 36 36 36  
 217 QI 36 36 36 36 36 36 36 36 36 36  
 218 QI 36 36 36 36 36 36 36 36 36 36  
 219 QI 36 36 36 36 36 36 36 36 36 36  
 220 QI 36 36 36 36 36 36 36 36 36 36  
 221 QI 36 36 36 36 36 36 36 36 36 36  
 222 QI 36 36 36 36 36 36 36 36 36 36  
 223 QI 36 36 36 36 36 36 36 36 36 36  
 224 QI 36 36 36 36 36 36 36 36 36 36  
 225 QI 36 36 36 36 36 36 36 36 36 36  
 226 QI 36 36 36 36 36 36 36 36 36 36  
 227 QI 36 36 36 36 36 36 36 36 36 36  
 228 QI 36 36 36 36 36 36 36 36 36 36  
 229 QI 36 36 36 36 36 36 36 36 36 36  
 230 QI 36 36 36 36 36 36 36 36 36 36  
 231 QI 36 36 36 36 36 36 36 36 36 36  
 232 QI 36 36 36 36 36 36 36 36 36 36  
 233 QI 36 36 36 36 36 36 36 36 36 36  
 \*

1

HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

234 QI 36 36 36 36 36 36 36 36 36 36  
 235 QI 36 36 36 36 36 36 36 36 36 36  
 236 QI 36 36 36 36 36 36 36 36 36 36  
 237 QI 36 36 36 36 36 36 36 36 36 36  
 238 QI 36 36 36 36 36 36 36 36 36 36  
 239 QI 36 36 36 36 36 36 36 36 36 36  
 240 QI 36 36 36 36 36 36 36 36 36 36  
 241 QI 36 36 36 36 36 36 36 36 36 36  
 242 QI 36 36 36 36 36 36 36 36 36 36  
 243 QI 36 36 36 36 36 36 36 36 36 36  
 \*

244 KK RMR ROUTE  
 245 KO  
 246 RS 71 FLOW  
 247 RC 0.050 0.050 0.050 7240 0.0014 0.00  
 248 RX 0.00 0.00 0.00 6.00 106.00 112.00 112.00 112.00  
 249 RY 1510.0 1510.00 1510.00 1509.00 1509.00 1510.00 1510.00 1510.00  
 \*  
 \*

250 KK OFF K BASIN  
 251 BA 0.505  
 252 LG 0.30 0.23 6.16 0.17 5  
 253 UC 1.543 1.047  
 254 UA 0 3.0 5.0 8.0 12.0 20.0 43.0 75.0 90.0 96.0  
 255 UA 100  
 \*

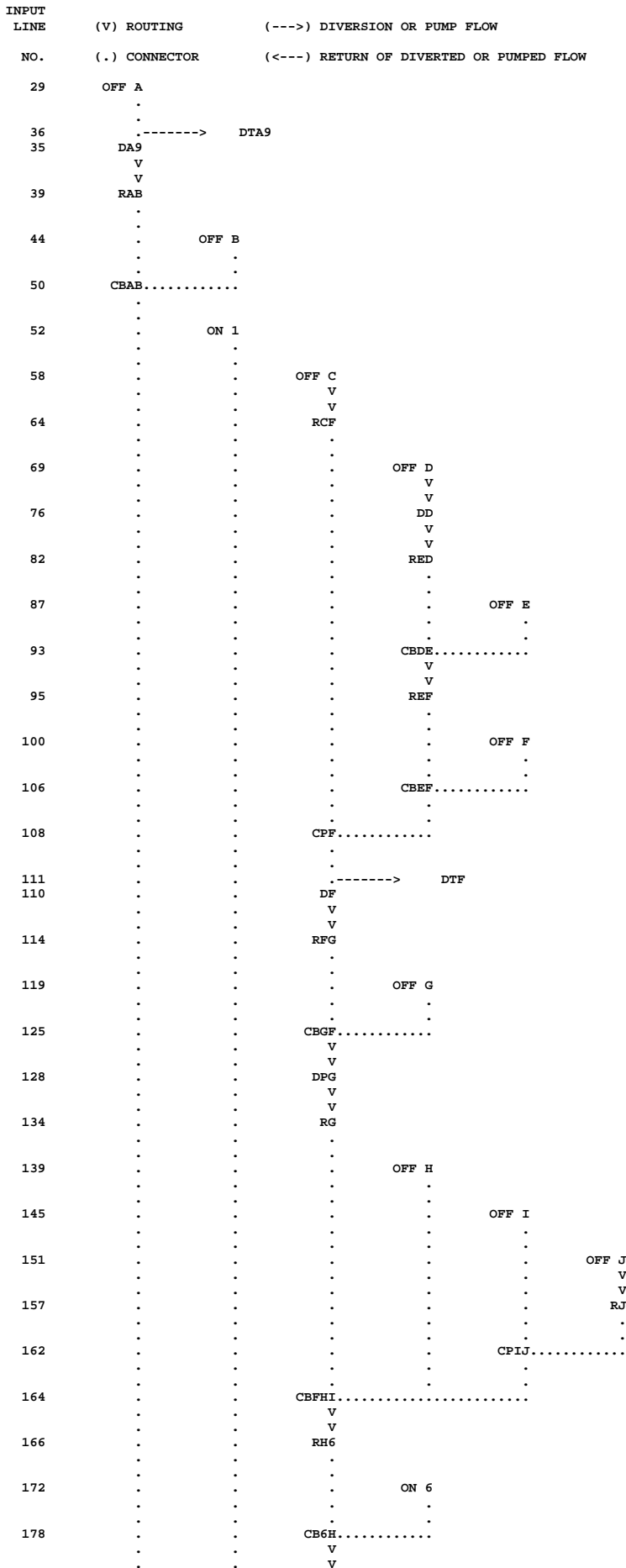
256 KK CB7K COMBINE  
 257 HC 3  
 \*

258 KK OFF L BASIN





SCHEMATIC DIAGRAM OF STREAM NETWORK



```

180      .      .      R67
      .      .      .
186      .      .      .      ON 7
      .      .      .      .
192      .      .      CB67.....
      .      .      V
      .      .      V
194      .      .      R78
      .      .      .
200      .      .      .      MR
      .      .      .      V
      .      .      .      V
244      .      .      .      RMR
      .      .      .      .
250      .      .      .      .      OFF K
      .      .      .      .      .
256      .      .      .      CB7K.....
      .      .      .      .
258      .      .      .      .      OFF L
      .      .      .      .      V
      .      .      .      .      V
264      .      .      .      .      RL8
      .      .      .      .      .
269      .      .      .      .      .      ON 8
      .      .      .      .      .
275      .      .      .      .      CB8L.....
      .      .      .      .
277      .      .      .      .      CP8.....
      .      .      .      .      V
      .      .      .      .      V
279      .      .      .      .      DET8
      .      .      .      .
286      .      .      .      .      .      <----- DTF
285      .      .      .      .      DF
      .      .      .      .      V
      .      .      .      .      V
287      .      .      .      .      RF
      .      .      .      .      .
292      .      .      .      .      .      OFF M
      .      .      .      .      .
298      .      .      .      .      .      CFPM.....
      .      .      .      .      V
      .      .      .      .      V
300      .      .      .      .      RFM
      .      .      .      .      .
305      .      .      .      .      .      ON 3
      .      .      .      .      .
311      .      .      .      .      .      CFM3.....
      .      .      .      .      V
      .      .      .      .      V
313      .      .      .      .      D23
      .      .      .      .      V
319      .      .      .      .      R24
      .      .      .      .
325      .      .      .      .      .      <----- DTA9
324      .      .      .      .      DA9
      .      .      .      .      V
      .      .      .      .      V
326      .      .      .      .      RA4
      .      .      .      .      .
331      .      .      .      .      .      .      OFF N
      .      .      .      .      .      V
      .      .      .      .      .      V
337      .      .      .      .      .      .      RN
      .      .      .      .      .      .
342      .      .      .      .      .      .      CP4N.....
      .      .      .      .      .      V
      .      .      .      .      .      V
344      .      .      .      .      .      .      RA4N
      .      .      .      .      .      .
349      .      .      .      .      .      .      ON 4
      .      .      .      .      .      .
355      .      .      .      .      .      .      CP24.....
      .      .      .      .      .
357      .      .      .      .      .      .      ON 5
      .      .      .      .      .      .
363      .      .      .      .      .      .      CB45.....
      .      .      .      .      .      V
      .      .      .      .      .      V
365      .      .      .      .      .      .      RET4

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998                       *
*   VERSION 4.1                     *
* RUN DATE 07JUN17 TIME 10:41:04 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
*   609 SECOND STREET          *
*   DAVIS, CALIFORNIA 95616    *
*   (916) 756-1104            *
*
*****

```

```

Flood Control District of Pinal County
AZ FARMS EX 100YR6HR - Arizona Farms MDR Existing Condition 100YR, 6HR
100 YEAR
6 Hour Storm
Unit Hydrograph: Clark
Storm: Multiple
FILE NAME: EX100YR6HR.DAT
BY: WOOD/PATEL JCD
11/03/2016

```

```

11 IO      OUTPUT CONTROL VARIABLES
          IPRT      5  PRINT CONTROL
          IPLOT     0  PLOT CONTROL
          QSCAL     0. HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN      2  MINUTES IN COMPUTATION INTERVAL
          IDATE     1JAN99 STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        2000 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    3JAN99 ENDING DATE
          NDTIME    1838 ENDING TIME
          ICENT     19  CENTURY MARK

          COMPUTATION INTERVAL .03 HOURS
          TOTAL TIME BASE     66.63 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-Feet
SURFACE AREA      ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

```

13 JD      INDEX STORM NO. 1
          STRM      2.74 PRECIPITATION DEPTH
          TRDA      .00 TRANSPOSITION DRAINAGE AREA

```

```

14 PI      PRECIPITATION PATTERN
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .01 .01 .01 .01 .01 .02 .02 .02 .02 .02
          .02 .02 .04 .06 .06 .06 .06 .06 .06 .06
          .01 .01 .01 .01 .01 .01 .01 .01 .01 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

```

```

17 JD      INDEX STORM NO. 2
          STRM      2.72 PRECIPITATION DEPTH
          TRDA      .50 TRANSPOSITION DRAINAGE AREA

```

```

18 PI      PRECIPITATION PATTERN
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .01 .01 .01 .01 .01 .02 .02 .02 .02 .02
          .02 .02 .04 .06 .06 .06 .06 .06 .06 .06
          .01 .01 .01 .01 .01 .01 .01 .01 .01 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

```

```

21 JD      INDEX STORM NO. 3
          STRM      2.67 PRECIPITATION DEPTH
          TRDA      2.80 TRANSPOSITION DRAINAGE AREA

```

```

22 PI      PRECIPITATION PATTERN
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
          .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

```

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

25 JD INDEX STORM NO. 4  
 STRM 2.53 PRECIPITATION DEPTH  
 TRDA 16.00 TRANSPOSITION DRAINAGE AREA

26 PI PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.02	.02	.02	.02	.02
.02	.02	.02	.03	.03	.03	.03	.03	.03	.03	.03
.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 69 KK \* OFF D \* BASIN  
 \* \*  
 \*\*\*\*\*

70 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 76 KK \* DD \* STORAGE  
 \* \*  
 \*\*\*\*\*

77 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 125 KK \* CBGF \* COMBINE  
 \* \*  
 \*\*\*\*\*

126 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 128 KK \* DPG \* STORAGE  
 \* \*  
 \*\*\*\*\*

129 KO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

166 KK \* RH6 \* ROUTE

167 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

180 KK \* R67 \* ROUTE

181 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

194 KK \* R78 \* ROUTE

195 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

244 KK \* RMR \* ROUTE

245 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

279 KK \* DET8 \* STORAGE

280 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

313 KK \* D23 \* STORAGE

314 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPL0T 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

\*\*\* \*\*

365 KK \* RET4 \* STORAGE

\*\*\*\*\*

366 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

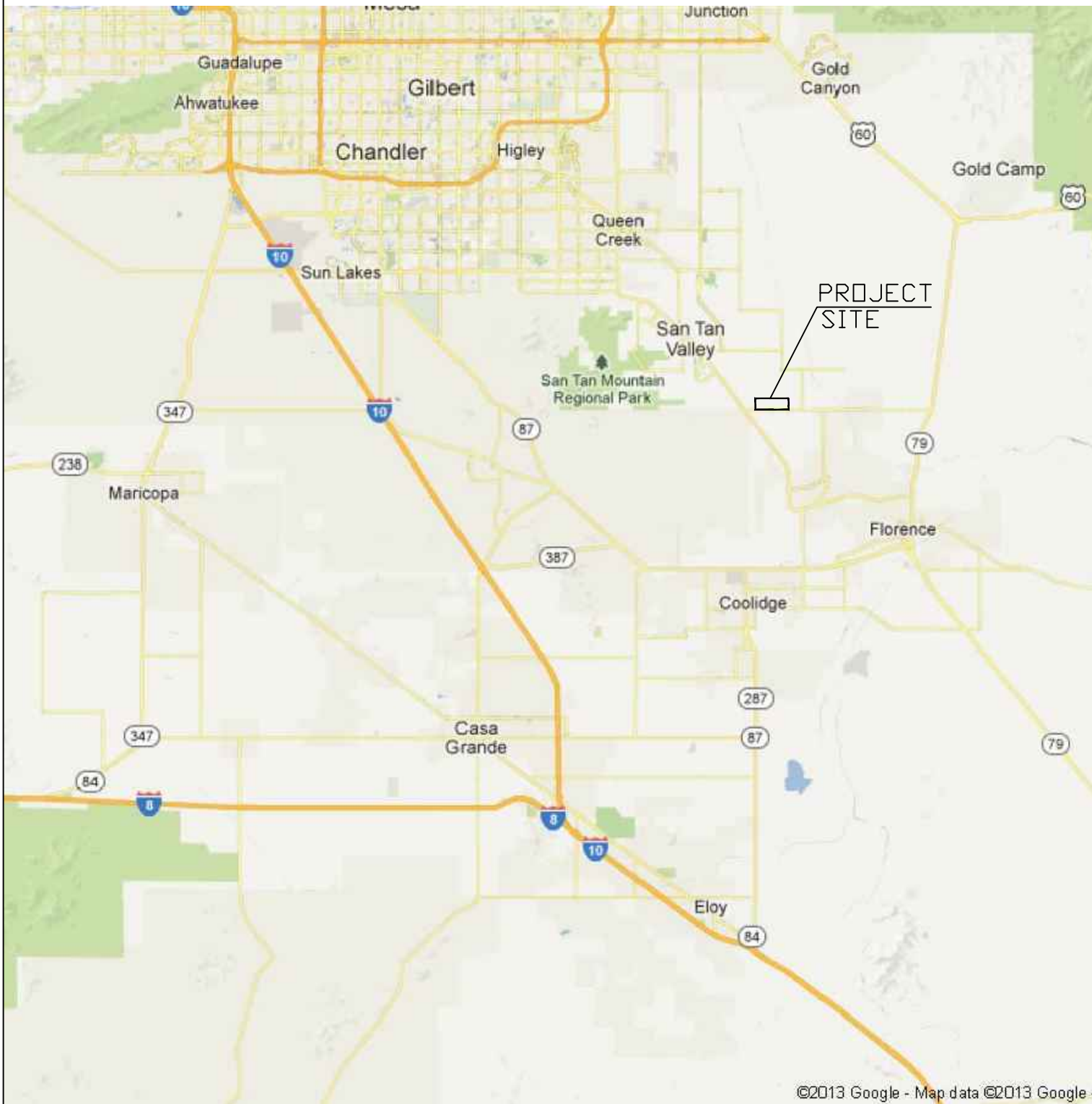
RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	OFF A	208.	6.53	101.	27.	10.	.55		
DIVERSION TO	DTA9	56.	6.53	22.	6.	2.	.55		
HYDROGRAPH AT	DA9	152.	6.53	79.	22.	8.	.55		
ROUTED TO	RAB	151.	6.77	78.	22.	8.	.55		
HYDROGRAPH AT	OFF B	108.	7.47	72.	21.	8.	.58		
2 COMBINED AT	CBAB	238.	7.10	144.	41.	15.	1.14		
HYDROGRAPH AT	ON 1	15.	4.80	4.	1.	0.	.02		
HYDROGRAPH AT	OFF C	123.	7.03	76.	22.	8.	.48		
ROUTED TO	RCF	123.	7.23	76.	22.	8.	.48		
HYDROGRAPH AT	OFF D	265.	5.77	119.	32.	12.	.89		
ROUTED TO	DD	63.	8.87	56.	25.	9.	.89		
ROUTED TO	RED	63.	9.00	56.	25.	9.	.89		
HYDROGRAPH AT	OFF E	124.	4.43	16.	4.	1.	.12		
2 COMBINED AT	CBDE	108.	4.43	56.	29.	11.	1.01		
ROUTED TO	REF	72.	5.73	55.	28.	10.	1.01		
HYDROGRAPH AT	OFF F	203.	8.63	153.	44.	16.	1.19		
2 COMBINED AT	CBEF	250.	8.93	196.	69.	25.	2.20		
2 COMBINED AT	CPF	335.	8.50	258.	89.	33.	2.68		
DIVERSION TO	DTF	82.	8.50	53.	14.	5.	2.68		
HYDROGRAPH AT	DF	253.	8.50	206.	75.	28.	2.68		
ROUTED TO	RFG	253.	8.80	206.	75.	28.	2.68		
HYDROGRAPH AT	OFF G	284.	9.43	220.	62.	22.	1.90		
2 COMBINED AT	CBGF	510.	9.30	409.	132.	48.	4.57		
ROUTED TO	DPG	188.	13.90	178.	123.	48.	4.57		
ROUTED TO	RG	188.	14.00	178.	123.	48.	4.57		
HYDROGRAPH AT	OFF H	11.	6.53	8.	3.	1.	.06		
HYDROGRAPH AT	OFF I	82.	7.07	53.	16.	6.	.31		
HYDROGRAPH AT	OFF J	230.	6.67	115.	31.	11.	.68		
ROUTED TO	RJ	230.	6.70	115.	31.	11.	.68		
2 COMBINED AT	CPIJ	301.	6.80	165.	46.	17.	.99		
3 COMBINED AT	CBFHI	311.	7.03	253.	163.	64.	5.63		
ROUTED TO	RH6	308.	7.83	251.	163.	64.	5.63		

+	HYDROGRAPH AT	ON 6	83.	6.07	38.	10.	4.	.22
+	2 COMBINED AT	CB6H	343.	7.77	265.	171.	67.	5.85
+	ROUTED TO	R67	340.	8.30	264.	171.	67.	5.85
+	HYDROGRAPH AT	ON 7	49.	6.37	28.	8.	3.	.19
+	2 COMBINED AT	CB67	362.	8.30	276.	176.	69.	6.04
+	ROUTED TO	R78	360.	8.67	275.	176.	69.	6.04
+	HYDROGRAPH AT	MR	36.	14.77	36.	36.	29.	1.37
+	ROUTED TO	RMR	36.	17.17	36.	36.	27.	1.37
+	HYDROGRAPH AT	OFF K	278.	5.13	79.	20.	7.	.50
+	3 COMBINED AT	CB7K	364.	8.67	275.	204.	101.	7.91
+	HYDROGRAPH AT	OFF L	89.	4.17	7.	2.	1.	.05
+	ROUTED TO	RL8	78.	4.30	7.	2.	1.	.05
+	HYDROGRAPH AT	ON 8	76.	5.90	33.	9.	3.	.23
+	2 COMBINED AT	CB8L	83.	4.30	40.	11.	4.	.28
+	2 COMBINED AT	CP8	374.	8.67	280.	209.	103.	8.19
+	ROUTED TO	DET8	364.	8.90	280.	205.	102.	8.19
+	HYDROGRAPH AT	DF	82.	8.50	53.	14.	5.	2.68
+	ROUTED TO	RF	81.	9.17	52.	14.	5.	2.68
+	HYDROGRAPH AT	OFF M	25.	5.37	9.	2.	1.	.07
+	2 COMBINED AT	CPFM	95.	8.93	61.	19.	7.	.07
+	ROUTED TO	RFM	94.	9.17	61.	19.	7.	.07
+	HYDROGRAPH AT	ON 3	35.	5.67	16.	4.	2.	.10
+	2 COMBINED AT	CPM3	101.	9.10	64.	23.	8.	.16
+	ROUTED TO	D23	52.	11.97	42.	15.	6.	.16
+	ROUTED TO	R24	52.	12.30	42.	15.	6.	.16
+	HYDROGRAPH AT	DA9	56.	6.53	22.	6.	2.	.55
+	ROUTED TO	RA4	55.	7.20	22.	6.	2.	.55
+	HYDROGRAPH AT	OFF N	47.	5.00	12.	3.	1.	.07
+	ROUTED TO	RN	45.	5.53	12.	3.	1.	.07
+	2 COMBINED AT	CP4N	65.	7.07	34.	9.	3.	.07
+	ROUTED TO	RA4N	65.	7.50	34.	9.	3.	.07
+	HYDROGRAPH AT	ON 4	141.	7.97	98.	29.	10.	.85
+	3 COMBINED AT	CP24	196.	7.83	137.	50.	18.	1.08
+	HYDROGRAPH AT	ON 5	52.	6.70	32.	10.	3.	.24
+	2 COMBINED AT	CB45	232.	7.77	162.	58.	21.	1.32

+           ROUTED TO           RET4       232.   7.87       161.       56.       20.       1.32

\*\*\* NORMAL END OF HEC-1 \*\*\*

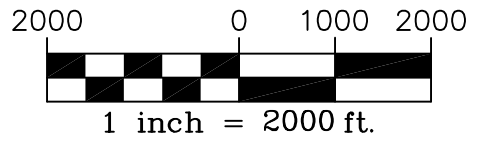
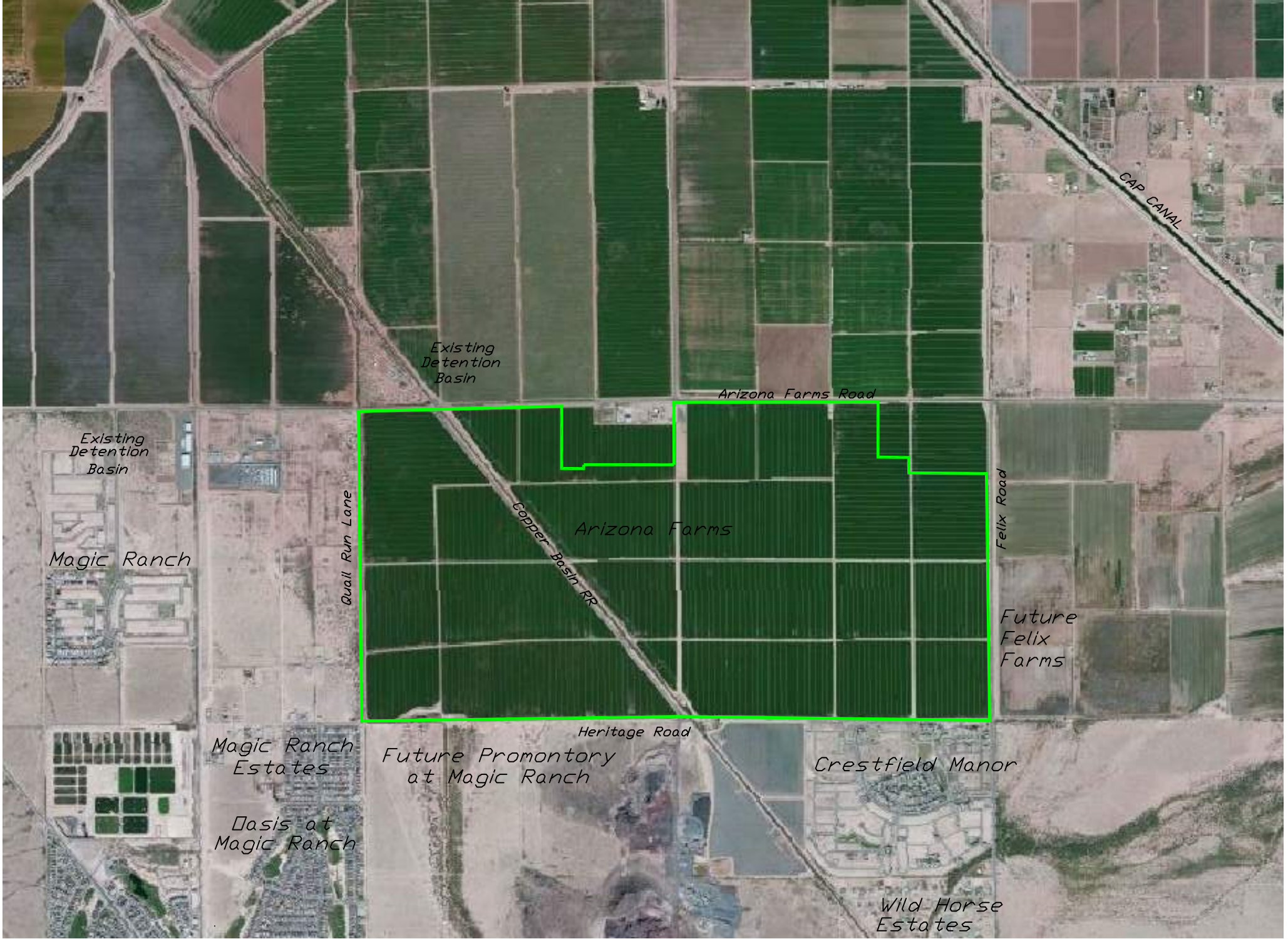


**PLATE 1  
VICINITY MAP**

**ARIZONA FARMS  
PINAL COUNTY, AZ**

**WOOD/PATEL**  
CIVIL ENGINEERS  
HYDROLOGISTS  
LAND SURVEYORS  
CONSTRUCTION MANAGERS  
2051 W. Northern Ave.  
Phoenix, AZ 85021  
(602) 335-8500  
www.woodpatel.com

N:\2014\44247 AZ Farms\Project Support\Reports\Drainage\DR Update\Final County\Exhibits\AZ Farms Plate 2 Aerial Map.dwg



**WOOD/PATEL**

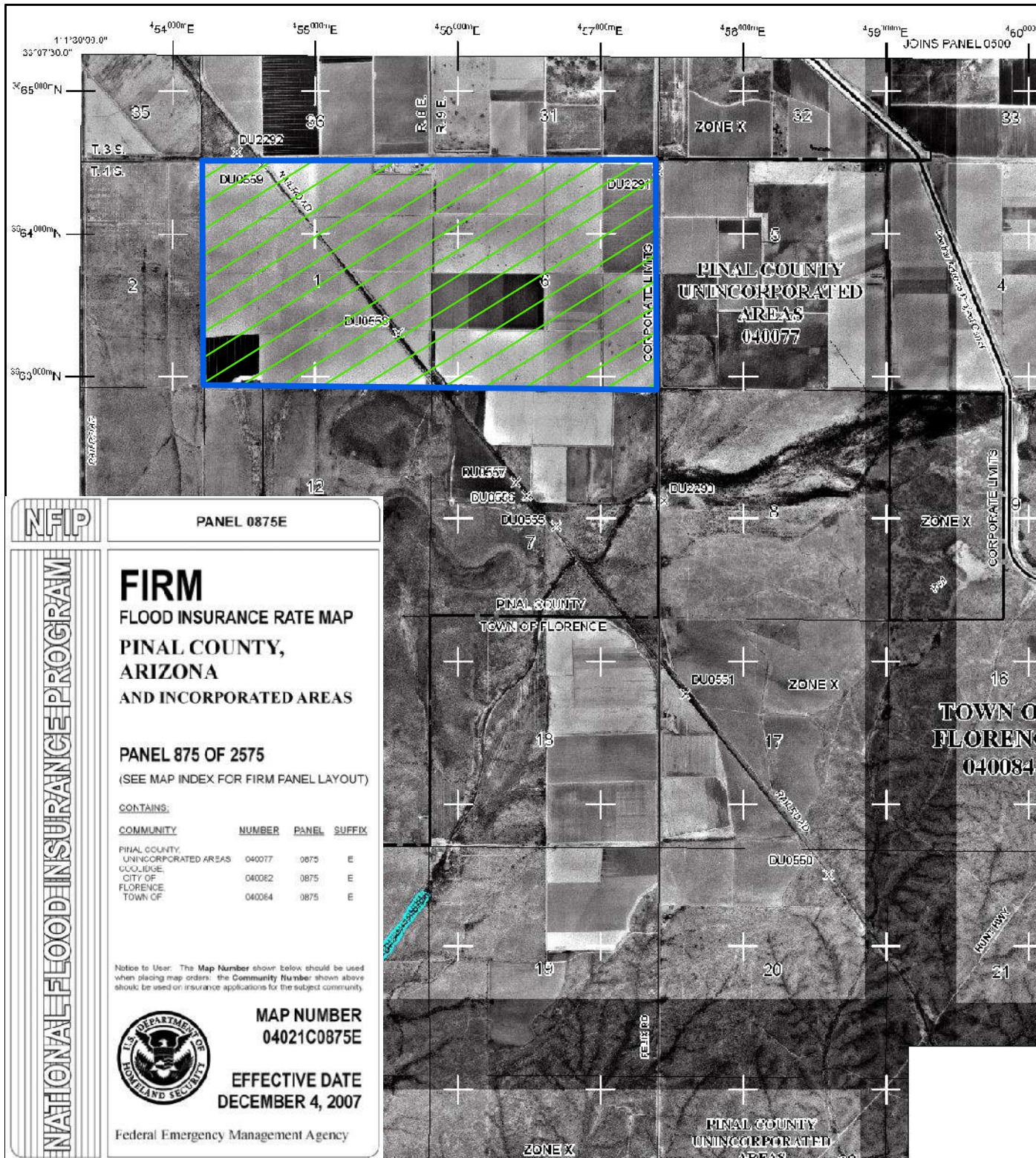
CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS

2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA • GOODYEAR • TUCSON

**ARIZONA FARMS**

**AERIAL MAP  
PLATE 2**

DATE 07/28/2016	SCALE 1" = 2000'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY



### LEGEND

**SPECIAL FLOOD HAZARD AREAS SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**  
 The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently destroyed. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE V** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE**  
 The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

- OTHER FLOOD AREAS**
- ZONE X** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.
- OTHER AREAS**
- ZONE X** Areas determined to be outside the 0.2% annual chance floodplain.
- ZONE D** Areas in which flood hazards are undetermined, but possible.
- COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**
- OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- 1% annual chance floodplain boundary
- 0.2% annual chance floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Area Zones, and boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths, or flood velocities
- Base Flood Elevation line and value: elevation in feet\*
- Base Flood Elevation value where uniform within zone; elevation in feet\*

- \* Referenced to the National Geodetic Vertical Datum of 1929
- A — A — Cross section line
- 2 — 2 — Transsect line
- 112° 07' 08", 33° 25' 41" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83), Western Hemisphere.
- 1000-meter Universal Transverse Mercator grid tick values zone 12
- 875000 FT 5000-foot grid tick values; Arizona State Plane coordinate system, central zone (FIPSZONE 2175) NAD83 (Transverse Mercator)
- X DV2313 Bench mark (see explanation in Notes to Users section of this FIRM panel)
- M1.5 River Mile

1 INCH = 2000 FEET



NFP

PANEL 0875E

# FIRM

## FLOOD INSURANCE RATE MAP

### PINAL COUNTY, ARIZONA

#### AND INCORPORATED AREAS

PANEL 875 OF 2575  
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
PINAL COUNTY, UNINCORPORATED AREAS	040077	0875	E
CITY OF FLORENCE	040062	0875	E
TOWN OF FLORENCE	040064	0875	E

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.



MAP NUMBER  
**04021C0875E**

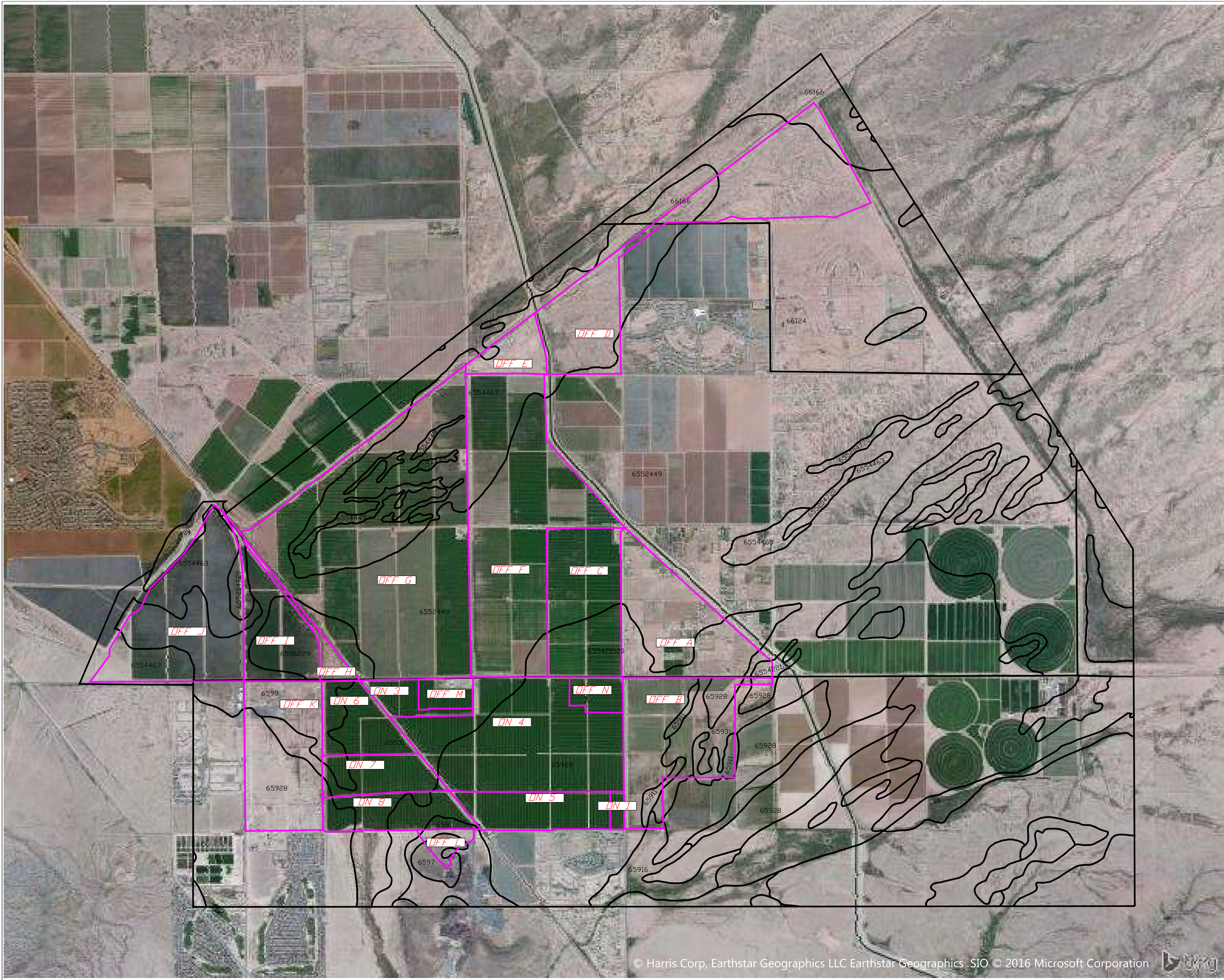
EFFECTIVE DATE  
**DECEMBER 4, 2007**

Federal Emergency Management Agency

ARIZONA FARMS

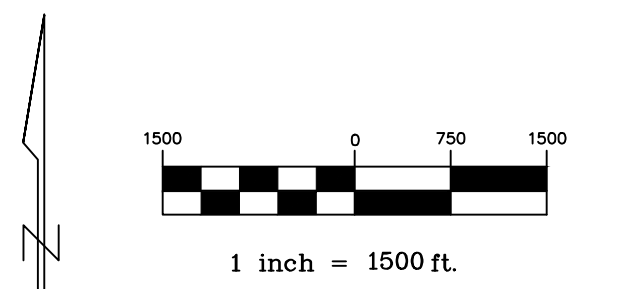
PLATE 3  
 FEMA FIRM MAP

**WOOD/PATEL**  
 MISSION: CLIENT SERVICE™



**LEGEND**

- SOIL BOUNDARY
- SOIL ID



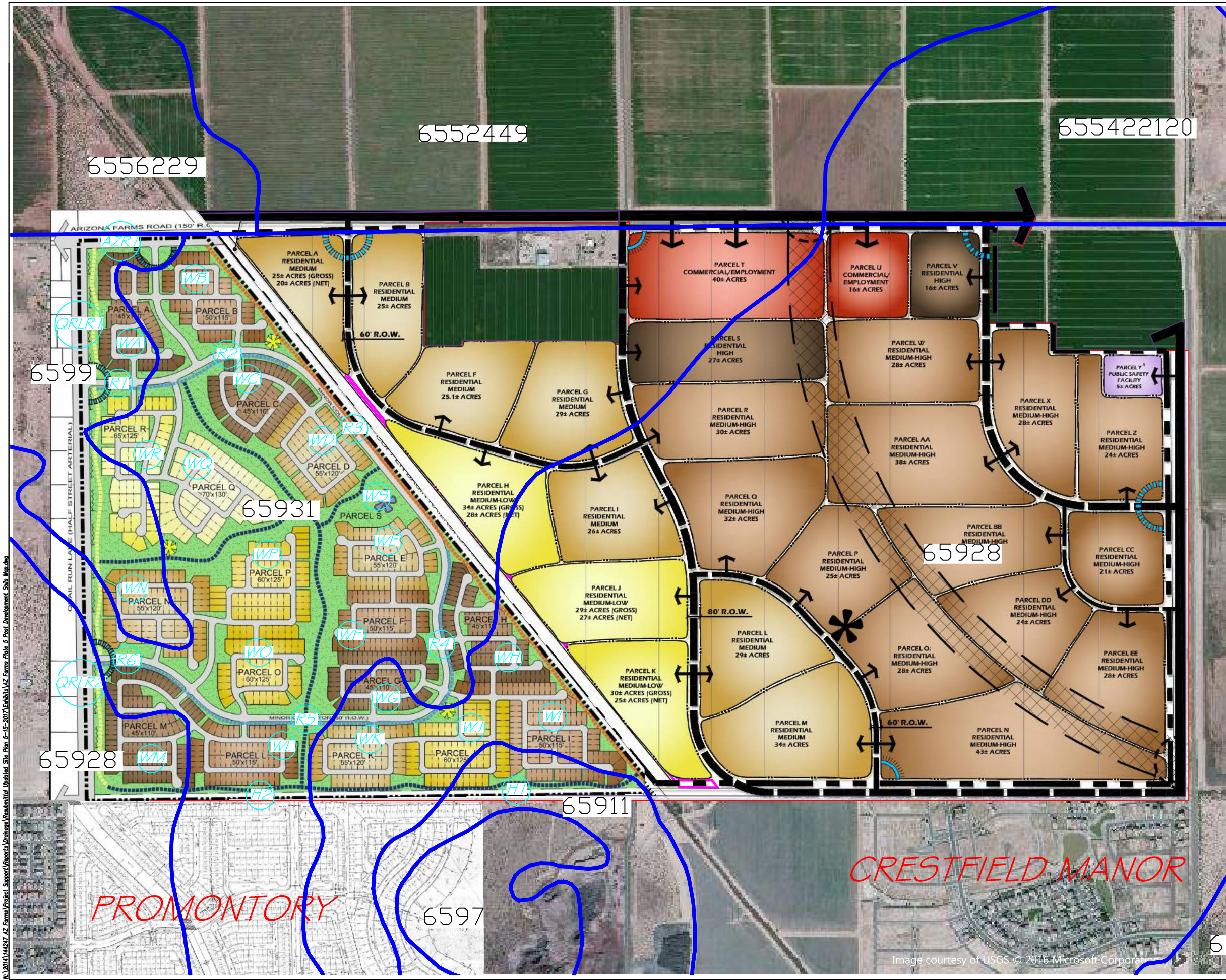
**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS

2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com




PHOENIX • MESA • TUCSON

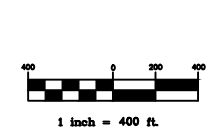
ARIZONA FARMS EXISTING  
 CONDITIONS SOILS MAP  
 PLATE 4

DATE 11/14/2016	SCALE 1" = 1500'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 4



**LEGEND**

-  SOIL BOUNDARY
-  65931 SOIL ID
-  SUB-BASIN



**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA • TUCSON

**ARIZONA FARMS POST DEVELOPMENT SOILS MAP PLATE 5**

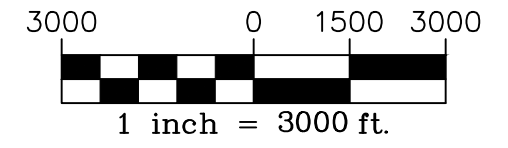
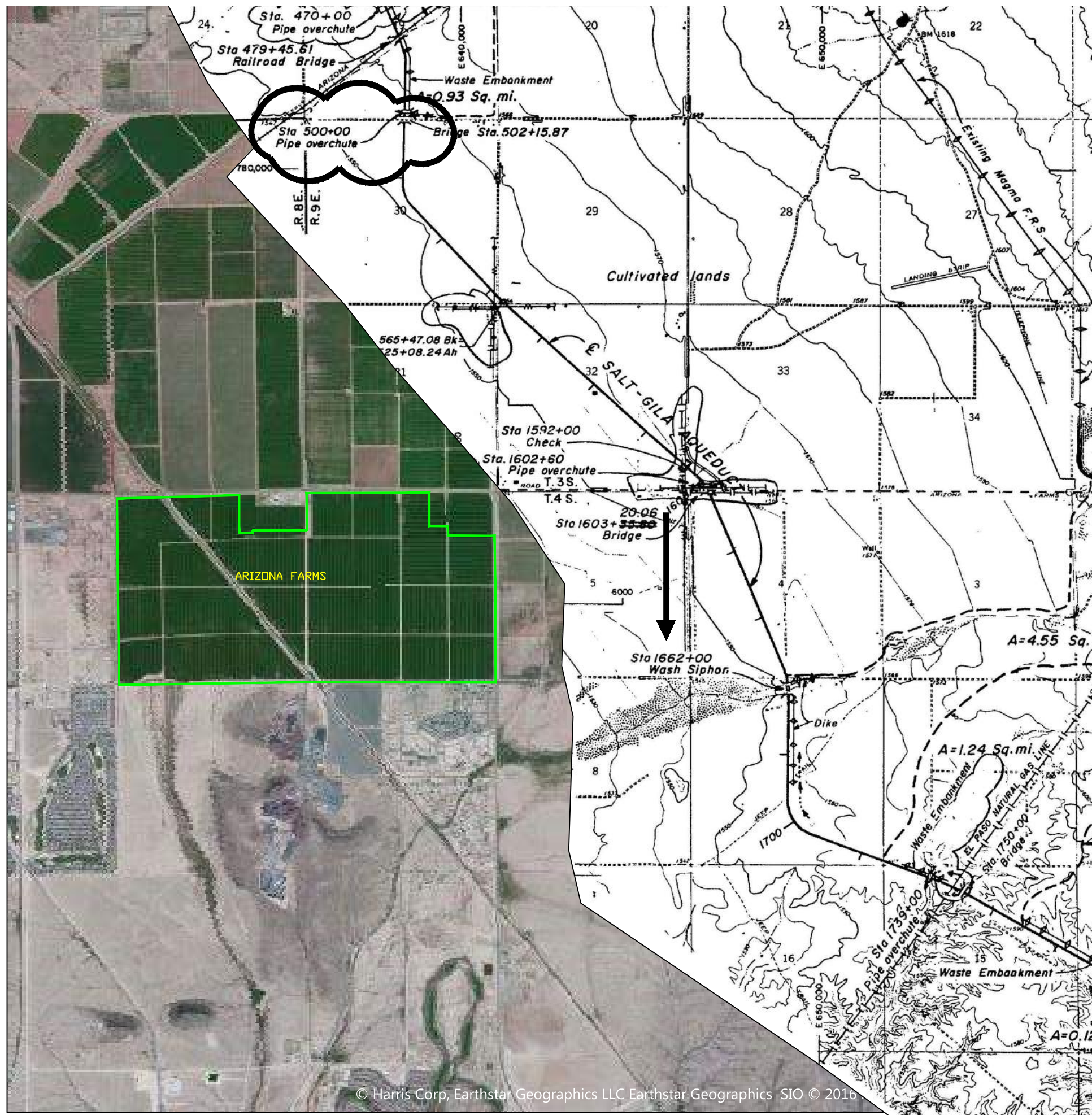
DATE 06/07/2017	SCALE 1" = 400'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 5

N:\2014\144247\_AZ\_Farms\Project\_Support\Reports\Drainage\Revised\Arizona Farms Post-Development Soils Map.dwg  
 11/20/14 14:42:47 AZ\_Farms\Project\_Support\Reports\Drainage\Revised\Arizona Farms Post-Development Soils Map.dwg

*CRESTFIELD MANOR*

*PROMONTORY*

Image courtesy of USGS © 2016 Microsoft Corporation



**EXPLANATION**

	Aqueduct		Primary highway
	Dike		Secondary highway
	Bridge		Light-duty road
	Overchute		Unimproved road
	Culvert		Jeep trail
	Drainage cut		Railroad
	Wash Siphon		Power line
	Check		Pipeline
			Telephone line

**NOTES**

Base map is a composite of Advance sheet U.S. Geological Survey 7.5 minute Quadrangle Sheets, Desert Well, Superstition Mts. S.W., Sacaton N.E., Mogma, Florence, Florence S.E. All of Pinal County, Arizona.

Arizona State plane coordinate system, central zone.

PROTECTIVE WORKS					
STATION	SIZE	PEAK Q in (cfs)	STORAGE CAPACITY (ac ft)	PEAK Q out (cfs)	DESIGN STORM
161+82.90	4-72" PIPE OVERCHUTE	17,000	8,424	1,113	OUTLET QUEEN CK. F.R.S
470+00	36" PIPE OVERCHUTE			17	
500+00	2-42" PIPE OVERCHUTE	160	15	60	
602+50	42" PIPE OVERCHUTE				TAIL WATER DRAINAGE
1662+00	WASH SIPHON	684	19	644	100yr 6hr GENERAL STORM
1884+30	54" PIPE OVERCHUTE	138		138	3hr THUNDER STORM
1887+06	54" PIPE OVERCHUTE	103		103	" "
915+45	2-66" PIPE CULVERT	492		286	100yr 6hr THUNDER STORM
948+60	54" PIPE CULVERT	242		151	" "
970+40	2-72" PIPE CULVERT	1032		562	3hr THUNDER STORM
986+00	48" PIPE CULVERT	117		117	" "
991+00	48" PIPE CULVERT	131		125	" "
1009+00	36" PIPE CULVERT	67		67	" "
1012+00	66" PIPE CULVERT	213		213	" "
1036+00	30" PIPE CULVERT	632		480	" "
1052+35	42" PIPE CULVERT	95		83	" "
1059+50	42" PIPE CULVERT	90		90	" "

**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS

2051 W. Northern Ave.  
 Phoenix, AZ 85021

(602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA

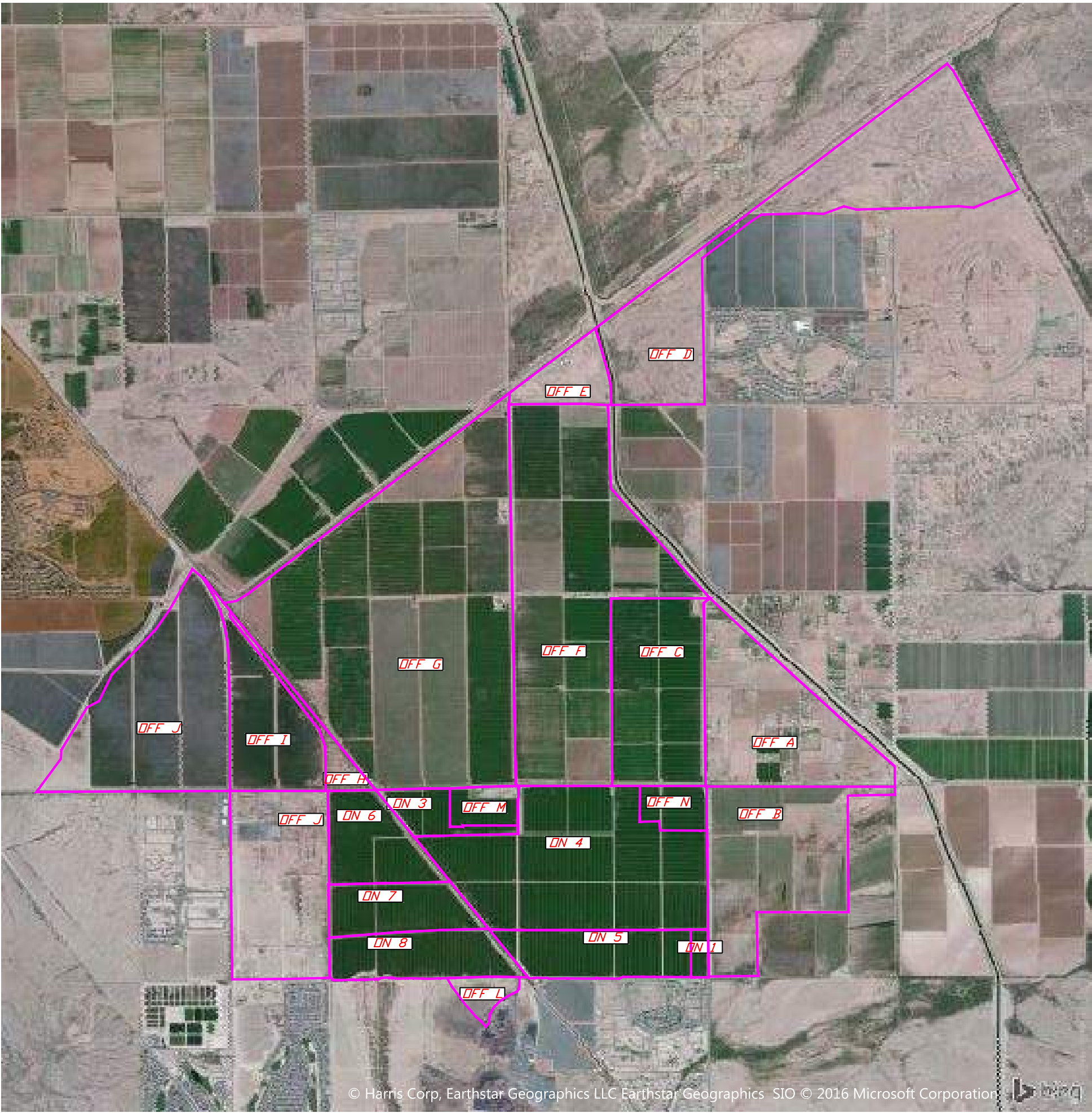
**ARIZONA FARMS**

**SALT-GILA AQUEDUCT REACH 3 MAP PLATE 6**

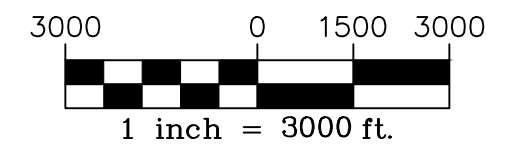
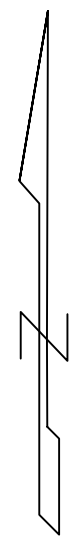
DATE	SCALE	SHEET
01/28/2016	1" = 3000'	1 OF 1
JOB NO.	DESIGN JCD	CHECK MY
144247	DRAWN JCD	

N:\2014\144247\_AZ Farms\Project\_Support\Reports\Drainage Exhibits\AZ Farms Plate 6 CAP Soil-Gila Aqueduct Map.dwg

N:\2018\144247\_AZ\_Farms\Project\_Support\Drainage\_MDR\_Update\Final\_Counts\Resubmittal\_MDR\_11-3-2016\MLB\_Files\_10-20-2016\Exhibits\AZ\_Farms\_Plate\_7\_Existing\_Conditions\_Landuse\_Map\_2.dwg



© Harris Corp, Earthstar Geographics LLC Earthstar Geographics SIO © 2016 Microsoft Corporation



**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA

<b>ARIZONA FARMS</b>		
<b>ARIZONA FARMS EXISTING CONDITIONS LANDUSE PLATE 7</b>		
DATE 11/14/2016	SCALE 1" = 3000'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY

N: 2014\144247 AZ Farms\Project\_Support\Reports\Drainage\Resubmittal\_Updated\_Site\_Plan\_5-15-2017\Exhibits\AZ Farms Plate 8 Post Development Land Use Map\_144247.dwg

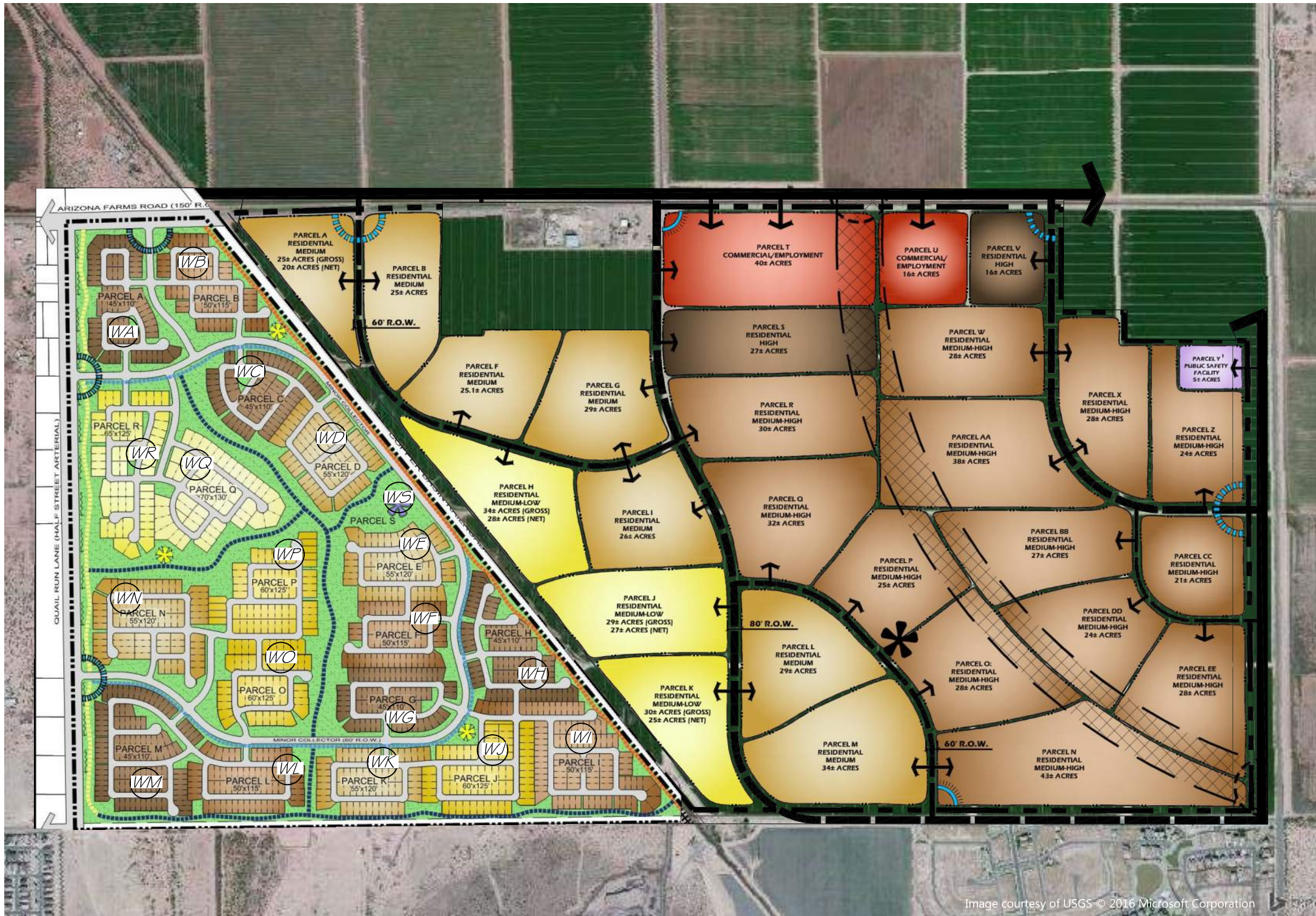


Image courtesy of USGS © 2016 Microsoft Corporation

**LEGEND OF SYMBOLS:**

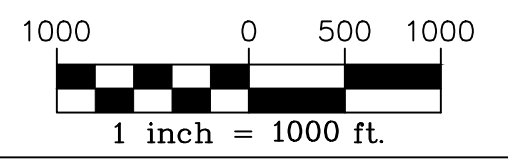
- Property Boundary
- Planning Parcel Boundary
- Copper Basin Railroad
- Conceptual North-South Freeway Corridor
- Existing Drainage Channel
- Vehicular Access
- Primary Community Entry
- Community Entry
- Potential Secondary Elementary School Site

**WEST PLAN SUMMARY TABLE:**

Land Use	
	Single-Family Residential
	Single-Family Residential
	Community Park Site
	Elementary School Site

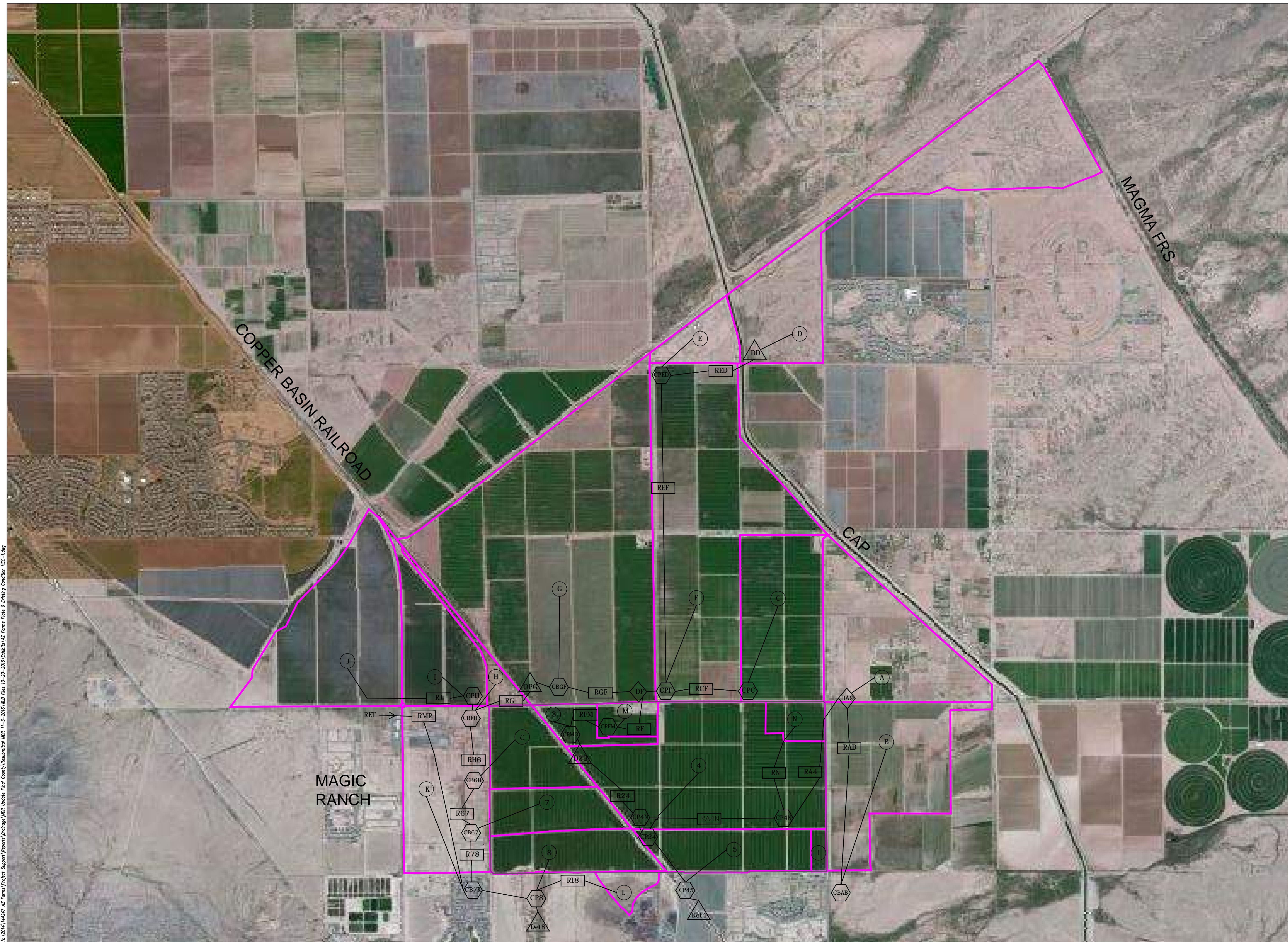
**EAST PLAN SUMMARY TABLE:**

Land Use	
	Single-Family Residential
	Single-Family Residential
	Single-Family Residential
	Multi-Family Residential
	Public Safety Facility
	Commercial/Employment

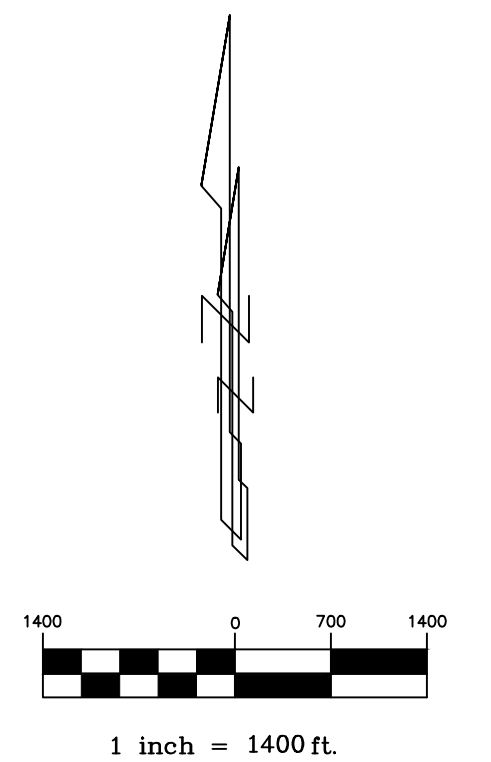


**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA

<b>ARIZONA FARMS</b>		
<b>PROPOSED LAND USE MAP PLATE 8</b>		
01/28/2016	1" = 1000'	1 1
144247	DESIGN JCD	CHECK MY
	DRAWN JCD	



- LEGEND**
- A HEC-1 SUB BASIN
  - RAB HEC-1 ROUTING PATH
  - CPG1 HEC-1 COMBINATION POINT
  - DPG HEC-1 STORAGE
  - DF HEC-1 DIVERSION
  - DRAINAGE AREAS



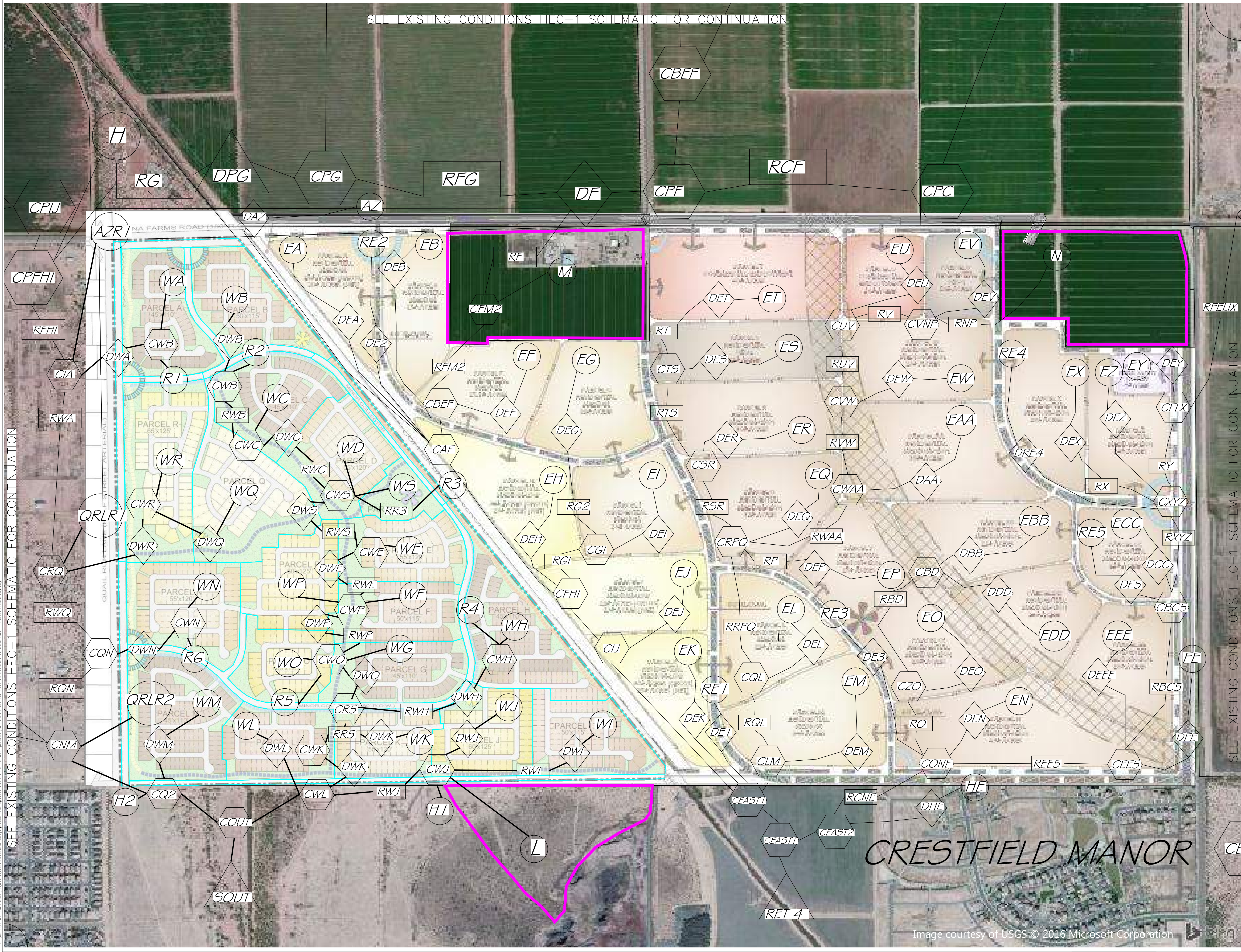
**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA

PLATE 9 ARIZONA FARMS  
 EXISTING CONDITION  
 HEC-1 SCHEMATIC MAP




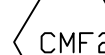

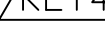

DATE 11/03/2016	SCALE 1" = 1400'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 9

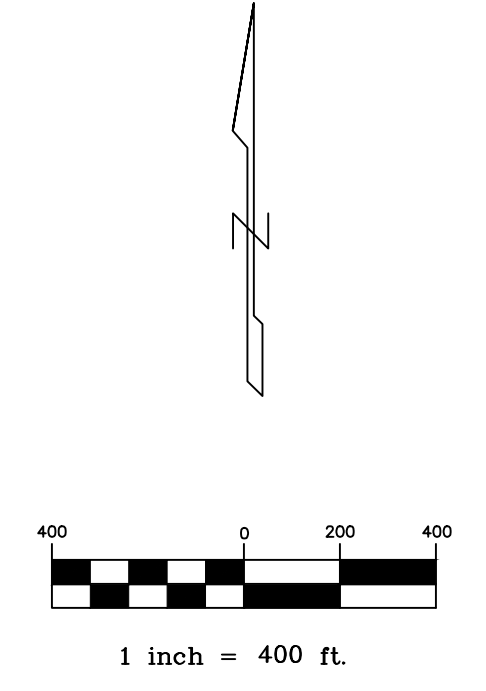
W:\2014\144247 AZ Farms\Project\_Support\Reports\Drainage\Map\_11-3-2016\WB\_Plate\_10-20-2016\Subarea AZ Farms\_Plate\_9 Existing Condition HEC-1.dwg

SEE EXISTING CONDITIONS HEC-1 SCHEMATIC FOR CONTINUATION



**LEGEND**

-  OFFSITE DRAINAGE AREAS
-  HEC-1 SUB BASIN
-  HEC-1 ROUTING PATH
-  HEC-1 COMBINATION POINT
-  HEC-1 RETENTION/DETENTION
-  HEC-1 DIVERSION
-  ONSITE DRAINAGE AREAS



**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA • TUCSON

**PLATE 10A**  
 POST-DEVELOPMENT CONDITION  
 HEC-1 SCHEMATIC MAP

DATE 07/26/2016	SCALE 1" = 400'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE B

**CRESTFIELD MANOR**

Image courtesy of USGS © 2016 Microsoft Corporation

SEE EXISTING CONDITIONS HEC-1 SCHEMATIC FOR CONTINUATION

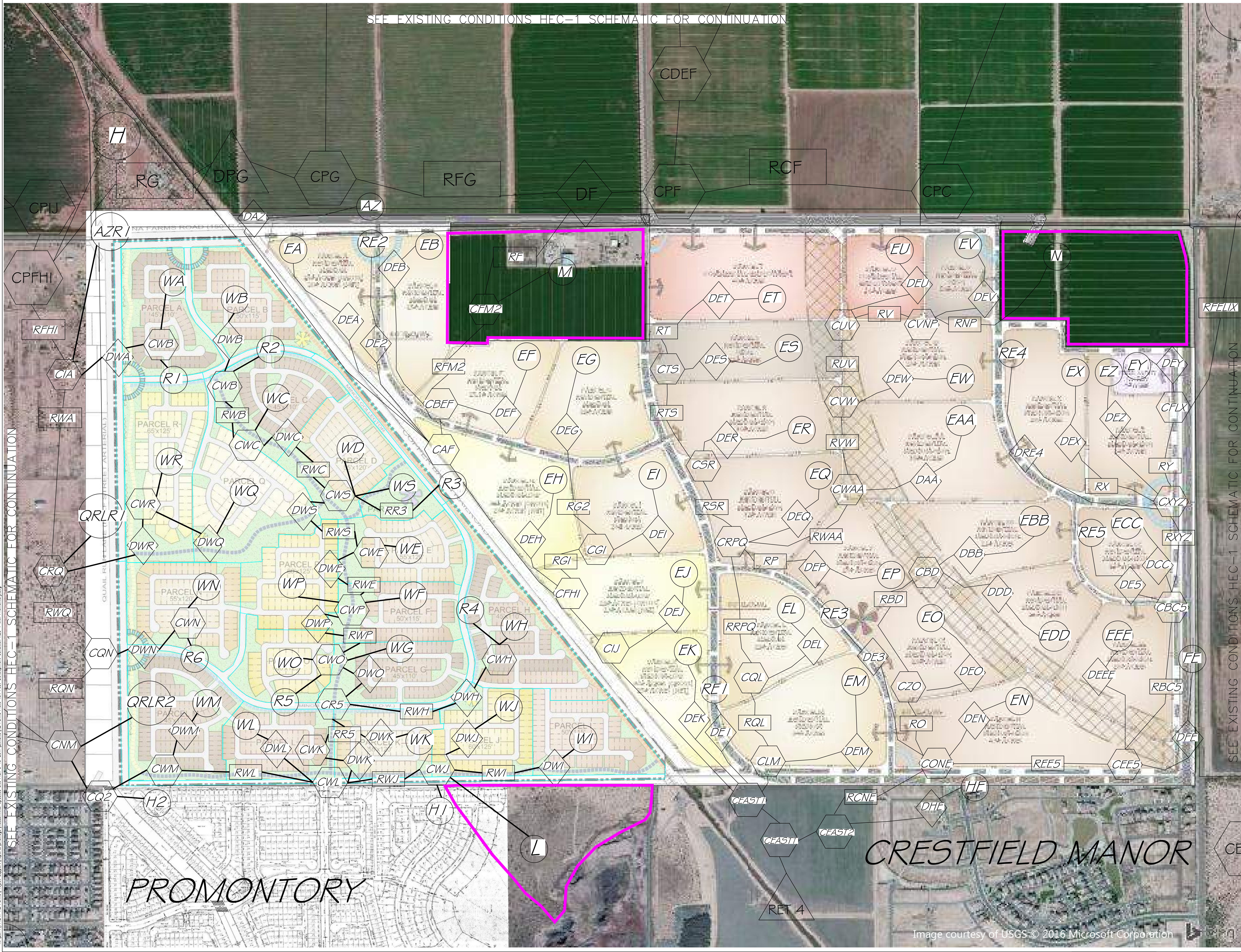
SEE EXISTING CONDITIONS HEC-1 SCHEMATIC FOR CONTINUATION

N:\2014\144247 AZ Farms Project Support\Reports\Drawings\Submitted\Updated Site Plan 5-15-2017\Crestfield AZ Farms Plate 10A Post-Development Condition HEC-1 without Promontory.dwg

SEE EXISTING CONDITIONS HEC-1 SCHEMATIC FOR CONTINUATION

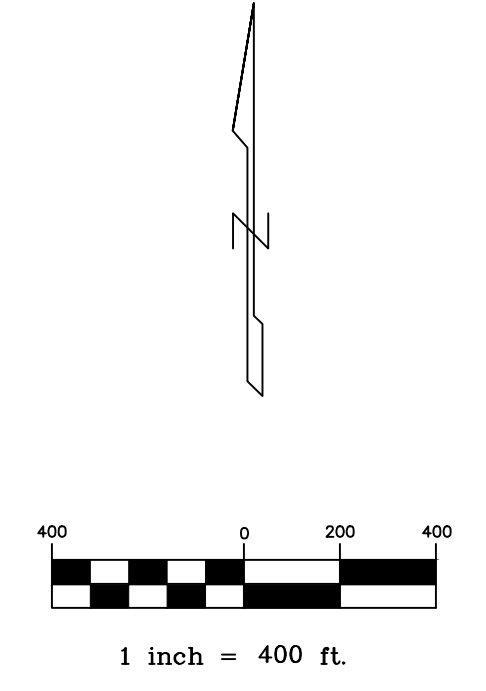
SEE EXISTING CONDITIONS HEC-1 SCHEMATIC FOR CONTINUATION

SEE EXISTING CONDITIONS HEC-1 SCHEMATIC FOR CONTINUATION



**LEGEND**

- OFFSITE DRAINAGE AREAS
- HEC-1 SUB BASIN
- HEC-1 ROUTING PATH
- HEC-1 COMBINATION POINT
- HEC-1 RETENTION/DETENTION
- HEC-1 DIVERSION
- ONSITE DRAINAGE AREAS



PROMONTORY

CRESTFIELD MANOR

**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA • TUCSON

PLATE 10B  
 POST-DEVELOPMENT CONDITION  
 HEC-1 SCHEMATIC MAP  
 WITH PROMONTORY DOWNSTREAM

DATE 07/26/2016	SCALE 1" = 400'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE B

Image courtesy of USGS © 2016 Microsoft Corporation

M:\2014\144247\_AZ\_Farms\Project\_Support\Reports\Drawings\Submitted\Updated\_Site\_Plan\_5-15-2017\Crestfield AZ Farms Plate 10B Post-Development Condition HEC-1 with Promontory.dwg



**LEGEND**

- Q<sub>100</sub>=182 cfs 100-YR 6-HR PEAK WASH FLOW
- EXISTING 100 YR FLOODPLAIN
- EXISTING 100 YR PONDING LIMITS
- PROJECT BOUNDARY

**WOOD/PATEL**

CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave.  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA • TUCSON

**PLATE 11 ARIZONA FARMS  
 EXISTING CONDITION  
 HYDRAULICS DRAINAGE MAP**

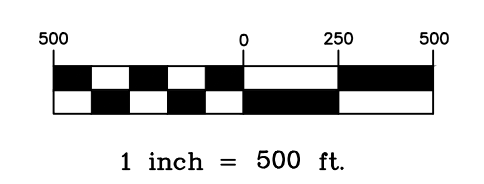
DATE 11/03/2016	SCALE 1" = 500'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 11

Image courtesy of USGS © 2016 Microsoft Corporation



**LEGEND**

- Q100=206cfs 100-YR, 6-HR PEAK DISCHARGE
- PROPOSED CULVERTS
- PROPOSED CHANNEL ID
- ▭ STORAGE



**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS

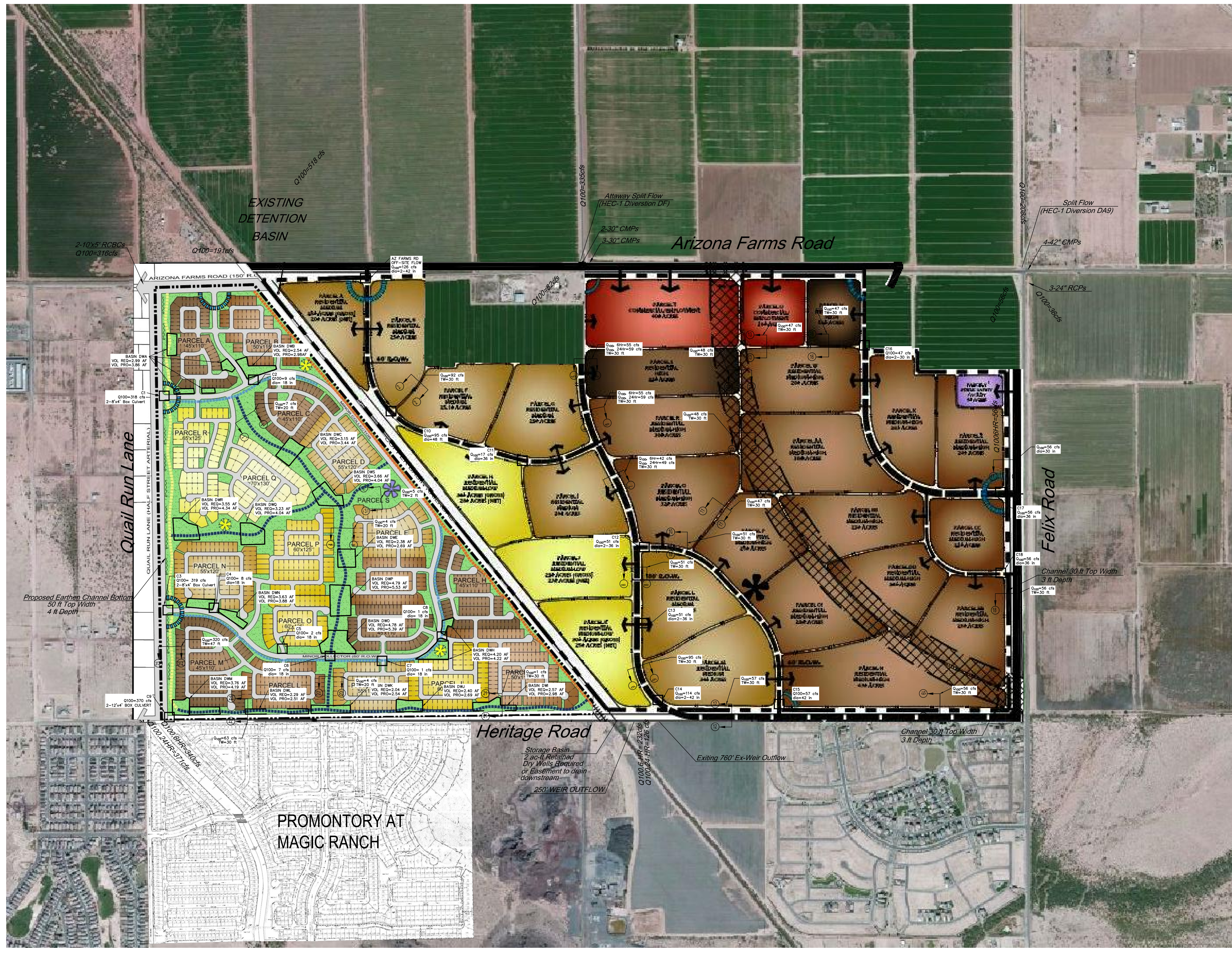
2051 W. Northern Ave  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com

PHOENIX • MESA • TUCSON

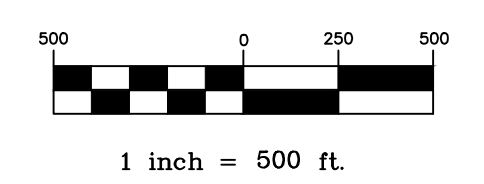
---

PLATE 12A  
 PROPOSED CONDITION  
 HYDRAULICS DRAINAGE MAP

DATE 11/08/2016	SCALE 1" = 500'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 12



- LEGEND**
- Q100=206cfs 100-YR, 6-HR PEAK DISCHARGE
  - PROPOSED CULVERTS
  - ① PROPOSED CHANNEL ID
  - ▭ STORAGE



**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS

2051 W. Northern Ave  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com

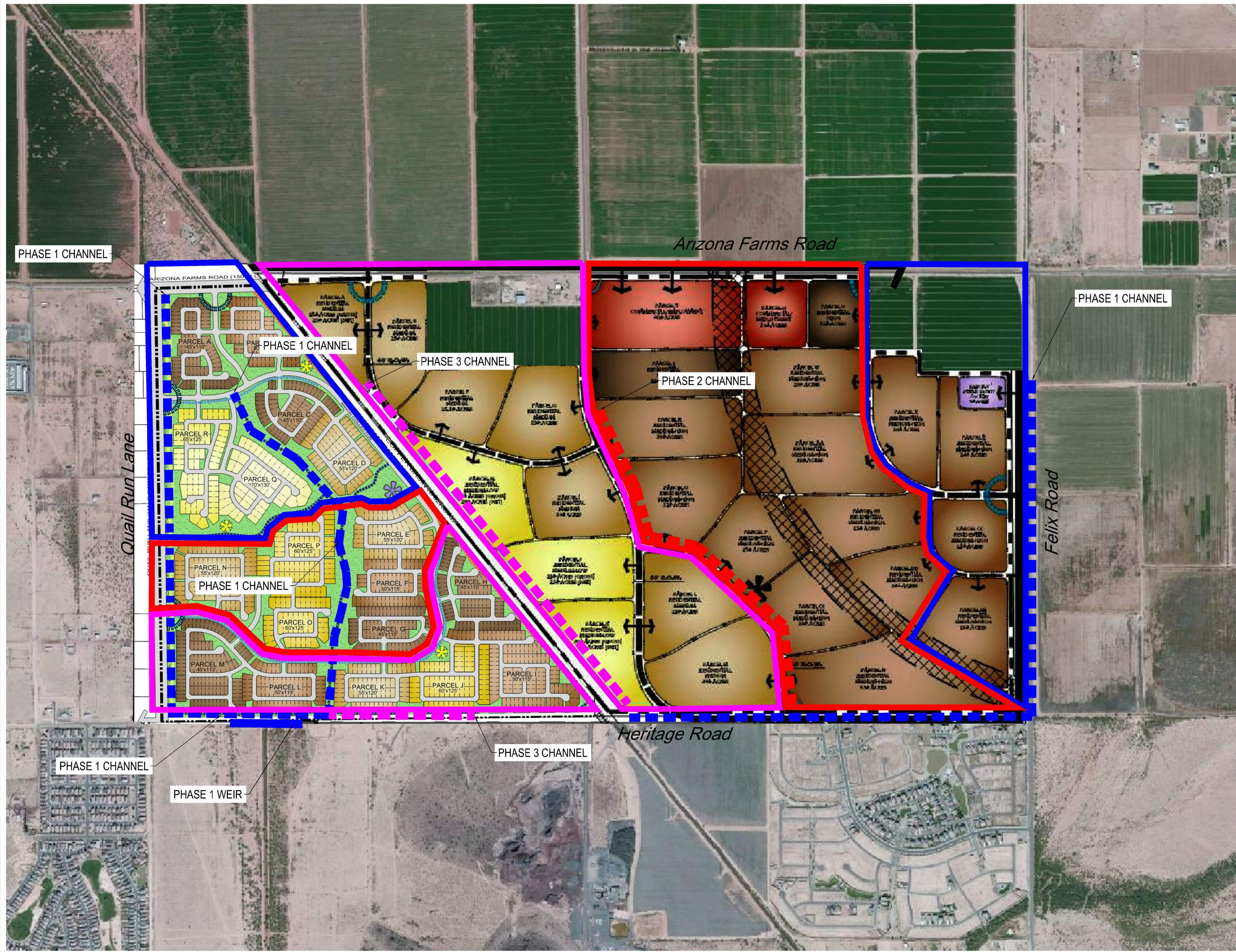
PHOENIX • MESA • TUCSON

---

PLATE 12B  
 PROPOSED CONDITION  
 HYDRAULICS DRAINAGE MAP  
 WITH PROMONTORY DOWNSTREAM

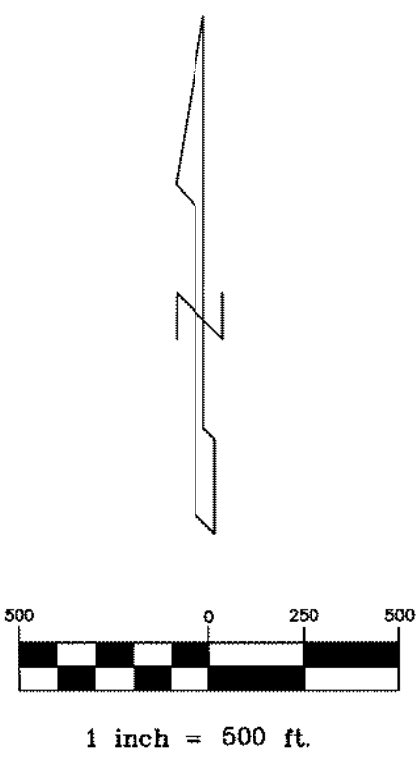
DATE 06/06/2017	SCALE 1" = 500'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 12

© 2017 Wood/Patel, Inc. All Rights Reserved. This drawing is the property of Wood/Patel, Inc. and is not to be reproduced, stored in a retrieval system, or transmitted in any form or by any means, electronic, mechanical, photocopying, recording, or by any information storage and retrieval system, without the prior written permission of Wood/Patel, Inc.



**LEGEND**

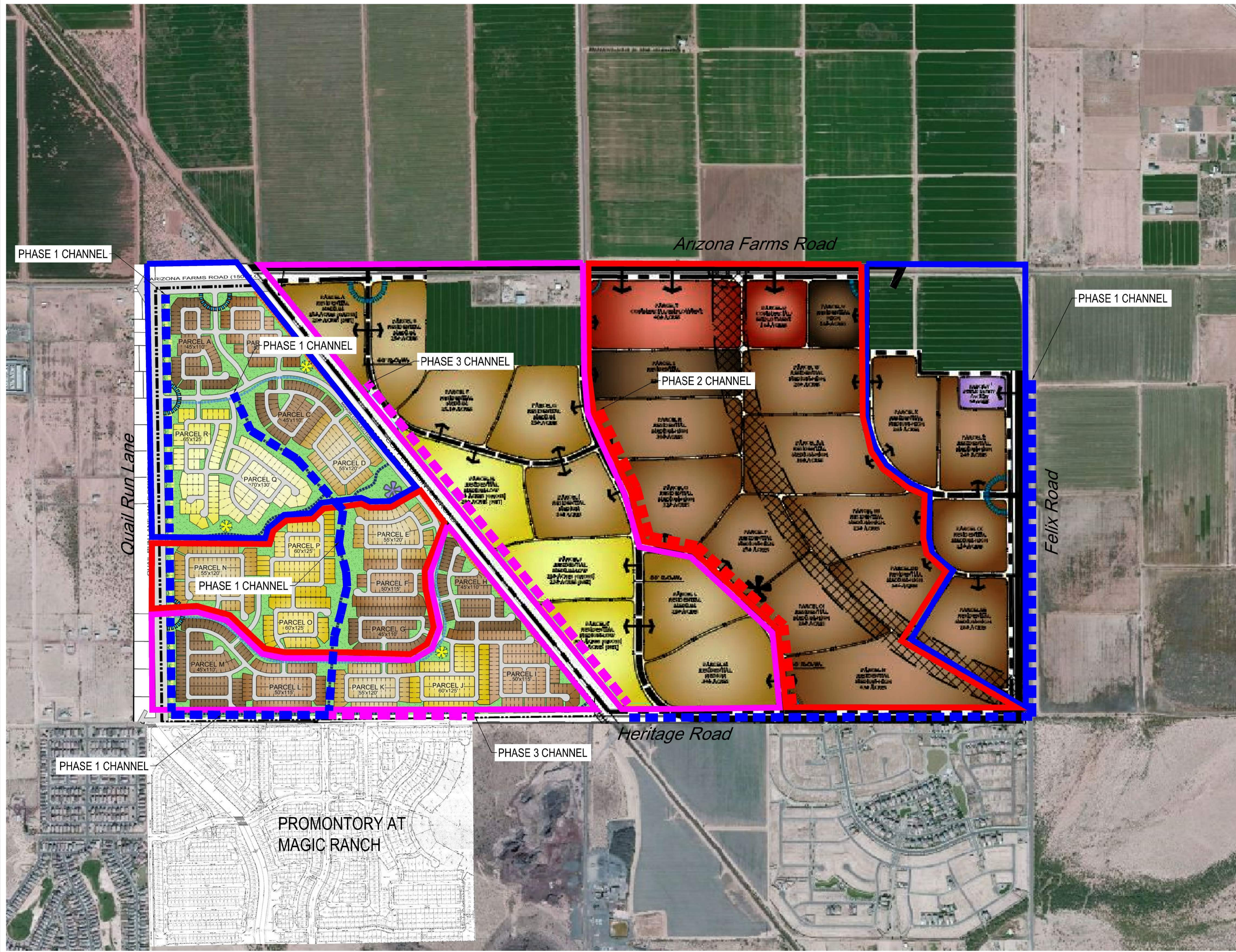
- PHASE 1 DEVELOPMENT
- PHASE 2 DEVELOPMENT
- PHASE 3 DEVELOPMENT
- PHASE 1 CHANNEL
- PHASE 2 CHANNEL
- PHASE 3 CHANNEL



**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA • TUCSON

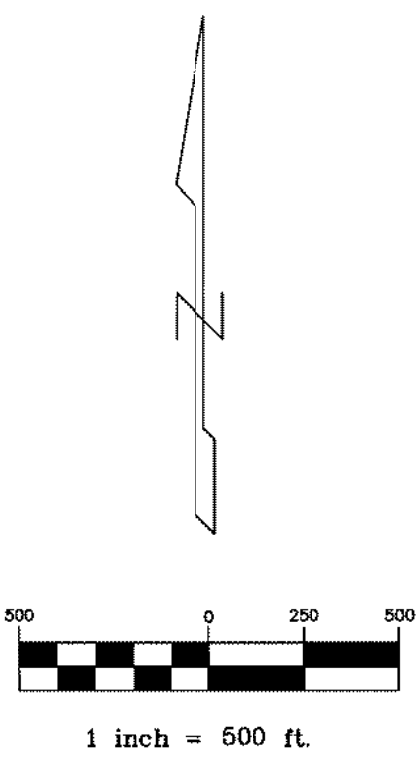
**PLATE 13A AZ FARMS  
 DEVELOPMENT PHASING MAP**

DATE 06/07/2017	SCALE 1" = 600'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 12



**LEGEND**

- PHASE 1 DEVELOPMENT
- PHASE 2 DEVELOPMENT
- PHASE 3 DEVELOPMENT
- - - PHASE 1 CHANNEL
- - - PHASE 2 CHANNEL
- - - PHASE 3 CHANNEL



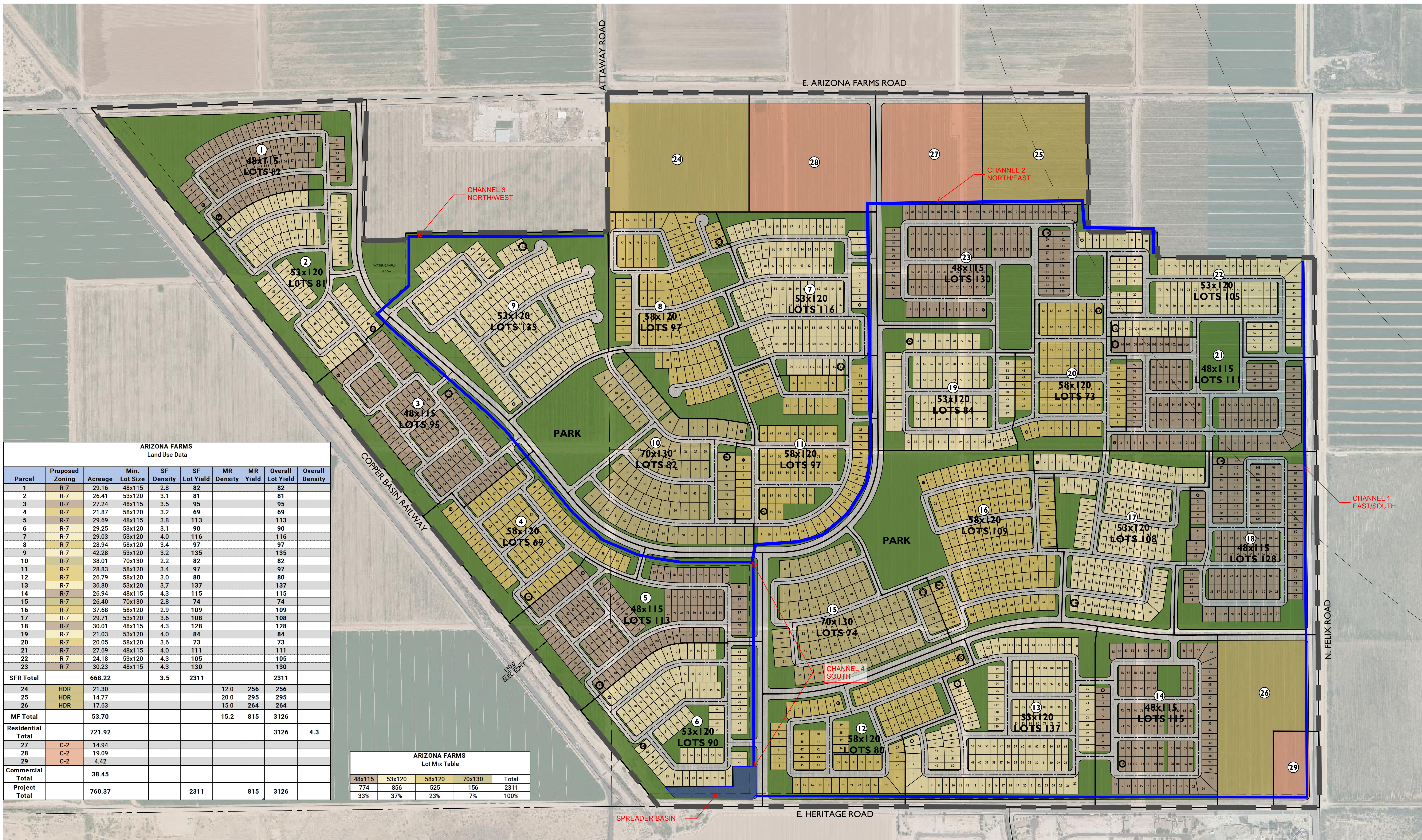
**WOOD/PATEL**  
 CIVIL ENGINEERS  
 HYDROLOGISTS  
 LAND SURVEYORS  
 CONSTRUCTION MANAGERS  
 2051 W. Northern Ave  
 Phoenix, AZ 85021  
 (602) 335-8500  
 www.woodpatel.com  
 PHOENIX • MESA • TUCSON

**PLATE 13B AZ FARMS  
 DEVELOPMENT PHASING MAP  
 WITH PROMONTORY DOWNSTREAM**

DATE 06/06/2017	SCALE 1" = 500'	SHEET 1 OF 1
JOB NO. 144247	DESIGN JCD DRAWN JCD	CHECK MY FILE PLATE 12

## **Appendix D.2**

### **HEC-I Schematic Map**

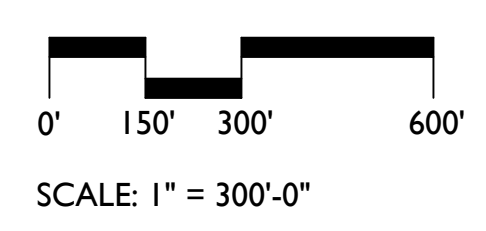
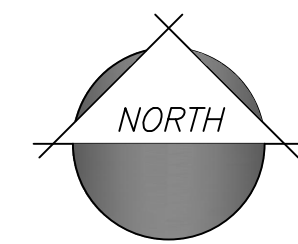


ARIZONA FARMS  
Land Use Data

Parcel	Proposed Zoning	Acreage	Min. Lot Size	SF Density	SF Lot Yield	MR Density	MR Yield	Overall Lot Yield	Overall Density
1	R-7	29.16	48x115	2.8	82			82	
2	R-7	26.41	53x120	3.1	81			81	
3	R-7	27.24	48x115	3.5	95			95	
4	R-7	21.87	58x120	3.2	69			69	
5	R-7	29.69	48x115	3.8	113			113	
6	R-7	29.25	53x120	3.1	90			90	
7	R-7	29.03	53x120	4.0	116			116	
8	R-7	28.94	58x120	3.4	97			97	
9	R-7	42.28	53x120	3.2	135			135	
10	R-7	38.01	70x130	2.2	82			82	
11	R-7	28.83	58x120	3.4	97			97	
12	R-7	26.79	58x120	3.0	80			80	
13	R-7	36.80	53x120	3.7	137			137	
14	R-7	26.94	48x115	4.3	115			115	
15	R-7	26.40	70x130	2.8	74			74	
16	R-7	37.68	58x120	2.9	109			109	
17	R-7	29.71	53x120	3.6	108			108	
18	R-7	30.01	48x115	4.3	128			128	
19	R-7	21.03	53x120	4.0	84			84	
20	R-7	20.05	58x120	3.6	73			73	
21	R-7	27.69	48x115	4.0	111			111	
22	R-7	24.18	53x120	4.3	105			105	
23	R-7	30.23	48x115	4.3	130			130	
<b>SFR Total</b>		<b>668.22</b>		<b>3.5</b>	<b>2311</b>			<b>2311</b>	
24	HDR	21.30				12.0	256		256
25	HDR	14.77				20.0	295		295
26	HDR	17.63				15.0	264		264
<b>MF Total</b>		<b>53.70</b>				<b>15.2</b>	<b>815</b>		<b>3126</b>
<b>Residential Total</b>		<b>721.92</b>						<b>3126</b>	<b>4.3</b>
27	C-2	14.94							
28	C-2	19.09							
29	C-2	4.42							
<b>Commercial Total</b>		<b>38.45</b>							
<b>Project Total</b>		<b>760.37</b>			<b>2311</b>		<b>815</b>	<b>3126</b>	

ARIZONA FARMS  
Lot Mix Table

48x115	53x120	58x120	70x130	Total
774	856	525	156	2311
33%	37%	23%	7%	100%



## **Appendix D.3 Hydroflow Outputs**

# Channel Report

## 21-0389 AZ Farms - Off Drn Channel - East/South

### Trapezoidal

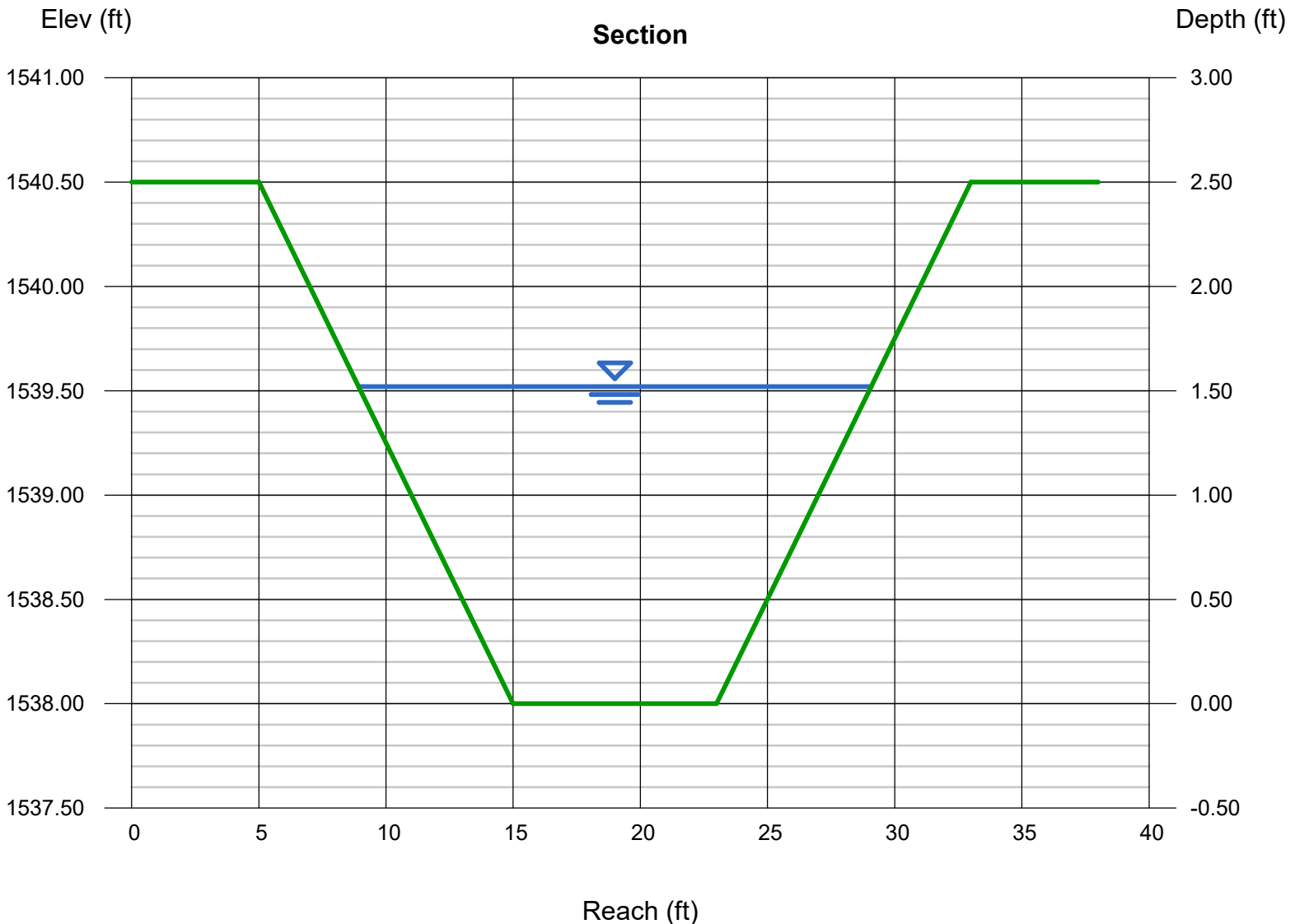
Bottom Width (ft) = 8.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.50  
Invert Elev (ft) = 1538.00  
Slope (%) = 0.25  
N-Value = 0.025

### Highlighted

Depth (ft) = 1.52  
Q (cfs) = 65.00  
Area (sqft) = 21.40  
Velocity (ft/s) = 3.04  
Wetted Perim (ft) = 20.53  
Crit Depth, Yc (ft) = 1.06  
Top Width (ft) = 20.16  
EGL (ft) = 1.66

### Calculations

Compute by: Known Q  
Known Q (cfs) = 65.00



# Channel Report

## 21-0389 AZ Farms - Off Drn Channel - North/East

### Trapezoidal

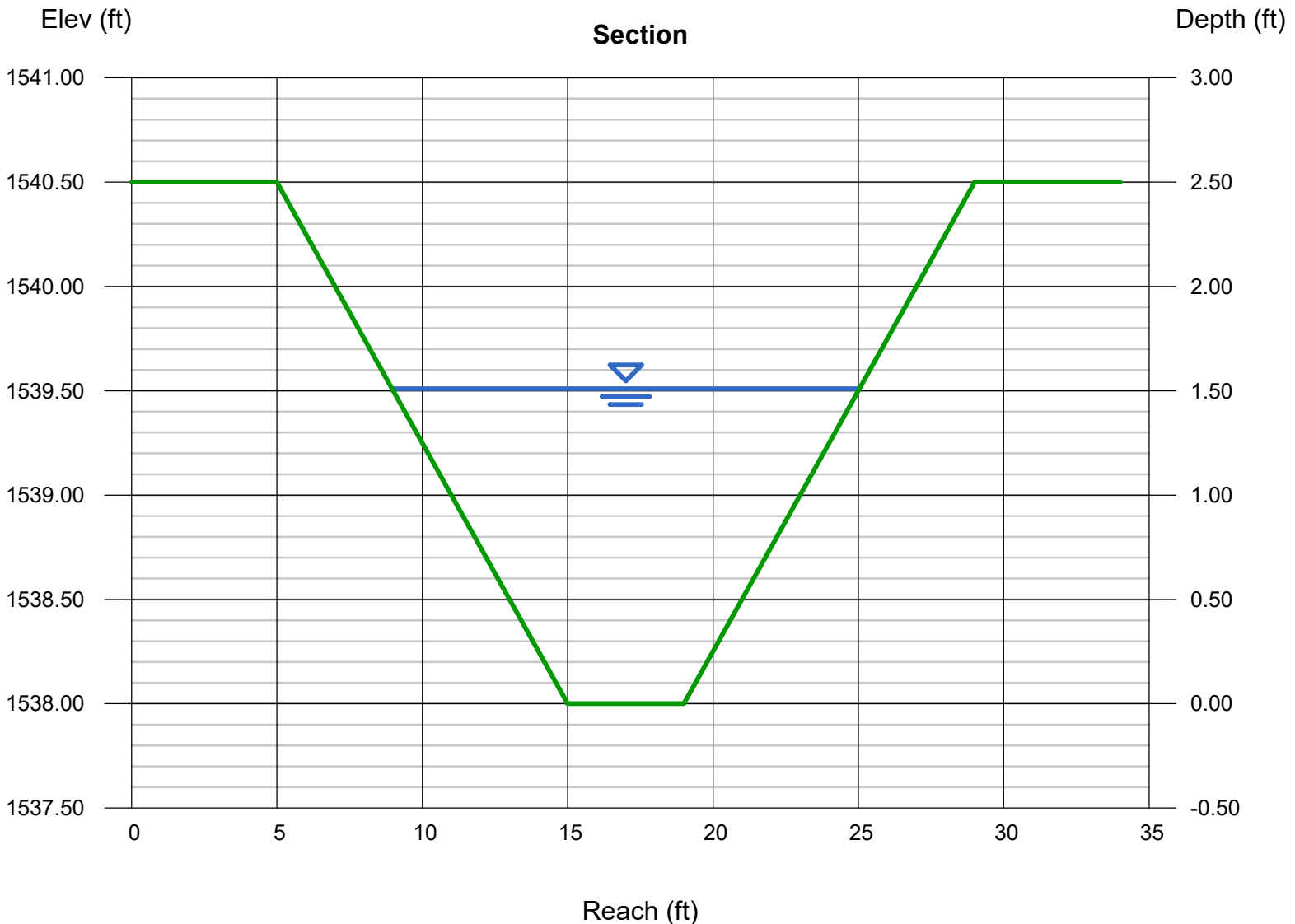
Bottom Width (ft) = 4.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 2.50  
Invert Elev (ft) = 1538.00  
Slope (%) = 0.31  
N-Value = 0.025

### Highlighted

Depth (ft) = 1.51  
Q (cfs) = 47.00  
Area (sqft) = 15.16  
Velocity (ft/s) = 3.10  
Wetted Perim (ft) = 16.45  
Crit Depth, Yc (ft) = 1.14  
Top Width (ft) = 16.08  
EGL (ft) = 1.66

### Calculations

Compute by: Known Q  
Known Q (cfs) = 47.00



# Channel Report

## 21-0389 AZ Farms - Off Drn Channel - North/West

### Trapezoidal

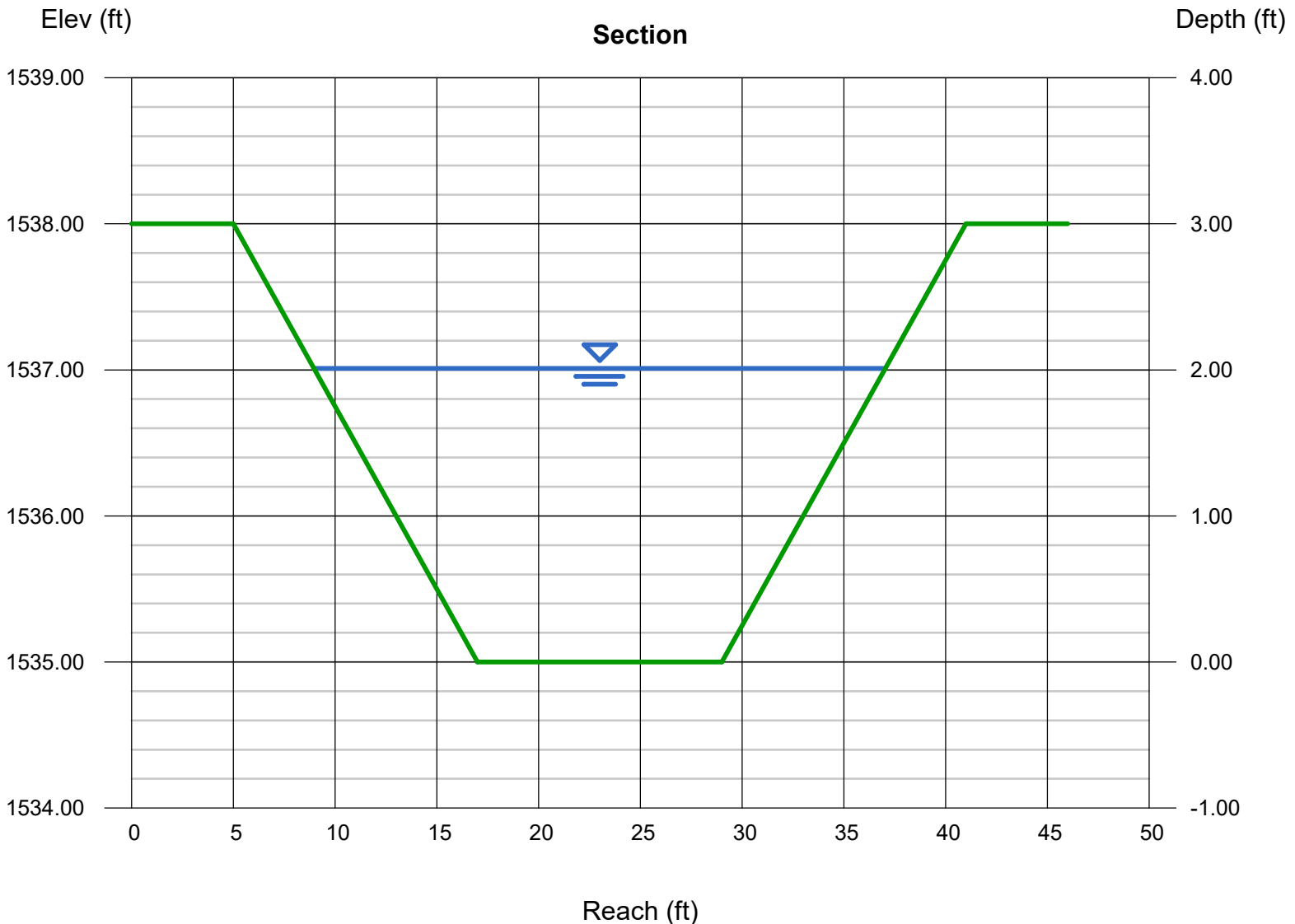
Bottom Width (ft) = 12.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 3.00  
Invert Elev (ft) = 1535.00  
Slope (%) = 0.10  
N-Value = 0.025

### Highlighted

Depth (ft) = 2.01  
Q (cfs) = 95.00  
Area (sqft) = 40.28  
Velocity (ft/s) = 2.36  
Wetted Perim (ft) = 28.57  
Crit Depth, Yc (ft) = 1.10  
Top Width (ft) = 28.08  
EGL (ft) = 2.10

### Calculations

Compute by: Known Q  
Known Q (cfs) = 95.00



# Channel Report

## 21-0389 AZ Farms - Off Drn Channel - North/West

### Trapezoidal

Bottom Width (ft) = 20.00  
Side Slopes (z:1) = 4.00, 4.00  
Total Depth (ft) = 3.00  
Invert Elev (ft) = 1525.00  
Slope (%) = 0.10  
N-Value = 0.025

### Highlighted

Depth (ft) = 2.02  
Q (cfs) = 142.00  
Area (sqft) = 56.72  
Velocity (ft/s) = 2.50  
Wetted Perim (ft) = 36.66  
Crit Depth, Yc (ft) = 1.08  
Top Width (ft) = 36.16  
EGL (ft) = 2.12

### Calculations

Compute by: Known Q  
Known Q (cfs) = 142.00

